

## Springfield Freeway Study Final Report

I-44 and US 60/State Highway 360
\#2017-10-40066
\#2017-11-40351
\#2017-10-40067
Springfield, MO
July 9, 2018


## Contents

Executive Summary ..... 1
Introduction ..... 1
Existing/No-Build Conditions ..... 3
Operational Assessment ..... 3
2017 Existing Conditions (No-Build) Operational Analysis ..... 7
2040 No-Build Operational Analysis ..... 11
Safety Assessment ..... 20
Roadway Assessment ..... 27
Bridge Assessment. ..... 31
Project Development ..... 34
Evaluation Process ..... 34
Cost Estimates ..... 36
Prioritization ..... 39
Assessing Benefits over Time ..... 39
Travel-Time Benefits ..... 40
Travel Time Savings ..... 40
Value of Travel Time Savings (VTTS) ..... 40
Safety Benefits ..... 44
Other Benefits ..... 45
Benefit / Cost (B/C) Ratio vs. Net Benefit ..... 46

## Appendices

Appendix A - No-Build Mainline and Ramp Volume Diagrams (2017 and 2040)
Appendix B - 2018 No-Build Operational Analysis
Appendix C - 2040 No-Build Operational Analysis
Appendix D - Roadway Analysis Tables
Appendix E - Bridge Analysis Tables
Appendix F - Project Exhibits
Appendix G - Detailed Cost Estimates
Appendix H - Crash Modification Factors
Appendix I - Mid-Project Preliminary Prioritization Results

## Executive Summary

This report summarizes the analysis leading to the long-term prioritization of improvements along Interstate 44 and US Highway 60 in and near the city of Springfield, MO. The study team examined existing conditions related to traffic flow, safety, roadway design, and bridge ratings. The team also developed traffic flow analysis for the year 2040 to identify future capacity needs. Based on these investigations, this report presents a series of recommended projects, including such items as ramp terminal intersection improvements, interchange reconfigurations, grade separations, auxiliary lanes, acceleration/deceleration lane improvements, and a braided ramp. For each project, the study team developed conceptual drawings and cost estimates.

The study team developed monetized estimates of the traffic operational and safety benefits expected to result from each individual project. Prioritization was based on the comparison of these monetized benefits with the estimated costs over a 2018-2040 time horizon. As Table E1 shows, the projects were ranked two different ways: using a Benefit/Cost (B/C) Ratio, and a Net Benefit estimate (monetized benefits minus costs). As the table indicates, the resulting rankings are not very dissimilar when comparing major projects. The top four large (>\$9M) projects are the same "bundle" in both lists, and really represent two projects: (1) US-60 / Route 125 grade separation, and (2) a braided ramp improvement on US-60 in the area from Glenstone Avenue to US-65. Projects 60E-5 and 60E-6, the remaining two projects, both obtain nearly all their traffic delay benefits from the US-60 / Route 125 grade separation, and thus should ultimately be prioritized much lower on the list. The fifth large project is conversion of US-60 to a freeway from Highland Springs Road to Route J / NN.

These rankings and costs can be used by MoDOT at a programming level in formulating the Statewide Transportation Improvement Program (STIP). Projects below a B/C ratio of 0.8 are not at a stage of need where inclusion in the STIP is recommended.

## Table E-1: Recommended Project Prioritization


*Projects 60E-5 and 60E-6 obtain nearly all their traffic delay benefits from project 60E-1, and so are not considered high priority.
**Typically, projects with a Benefit-Cost ( $B / C$ ) Ratio of 1.0 or greater are reasonable to construct during the planning horizon (2040). Due to the fact that a small number of benefits are not accounted for in the study methodology, two projects with $B / C$ ratios $>0.8$ are also reasonable to consider.

## Introduction

MoDOT's Southwest District, in cooperation with the Ozarks Transportation Organization (OTO), has undertaken a study to identify and prioritize highway projects along three corridors in the Springfield area. The three corridors are described below and shown in Figure 1.

- US 60/360 from l-44 to US 65 (referred to as the US 60 West corridor in this document)
- US 60 from US 65 to FR 247 (referred to as the US 60 East corridor in this document)
- I-44 from US 60/360 to Hwy 125

Figure 1: Study Corridors


MoDOT's mission is to provide a world-class transportation system that is safe, innovative, reliable and dedicated to a prosperous Missouri. MoDOT has three key values that represent the fundamental principles and philosophy of the agency: "Safety", "Service", and "Stability".

- This study prioritized "Safety" through developing projects that would have a tangible safety benefit through anticipated reduction in crashes.
- This report is in keeping with MoDOT's "Service" value in that it identifies transportation solutions of great value and prioritizes the solutions such that resources are used wisely.
- The "Stability" value is a key theme throughout this report as the analysis identifies projects needed to keep roads and bridges in good condition, maintain the existing transportation infrastructure in a reliable and convenient condition, and provide a safe and efficient transportation system that will support and advance economic development.

In assisting MoDOT to fulfill its mission to MoDOT customers, this report provides the following tangible results:

1. Keep Customers and Ourselves Safe - This study identified locations with high crash rates and projects were developed to reduce these crashes and ultimately improve safety.
2. Keep Roads and Bridges in Good Condition - This study evaluated the existing condition of the bridges and roadways along the study corridors and identified locations that were below "good" condition or not meeting current standards. These locations with deficiencies were considered when identifying projects based on poor LOS and high crash rates.
3. Providing Outstanding Customer Service - MoDOT customers expect great and timely projects to be delivered. This report provides an in-depth analysis that results in the development of great and needed projects, which are prioritized to meet the needs of the corridors through the study horizon.
4. Deliver Transportation Solutions of Great Value - The projects developed in this report provide solutions that target improvements to safety and efficiency, without recommending unnecessary, costly improvements.
5. Operate a Reliable and Convenient Transportation System - A "reliable" transportation system must be one that is in at least "good" condition. The projects recommended in this report consider the condition of the roadway and bridges in an effort to ensure their condition remain or are improved to good or better. A "convenient" transportation system must be easy to use and provide quick, direct access for all users. Project developed in this study made efficiency a priority while balancing the need for access based on land use.
6. Use Resources Wisely - This study was conducted in an effort to ensure that the study corridors were evaluated properly and projects prioritized to get the best value for the dollar through the study horizon year. This ensures that funding is used when and where it is actually needed.
7. Advance Economic Development - Safe and efficient transportation systems have been proven to assist in providing economic and social opportunities and benefits. The prioritized list of projects in this report provides a pathway to improving and keeping the MoDOT transportation system in a safe and efficient condition, which will ultimately support economic development.

## Existing/No-Build Conditions

In order to understand the existing conditions and needs along the three corridors, assessments were performed on current traffic operations, projected future no-build traffic operations, safety performance, roadway conditions, and bridge conditions.

## Operational Assessment

Traffic count data was obtained from MoDOT and supplemented with additional counts conducted by the consultant team where needed. Older counts were extrapolated and balanced along the corridors to establish a common existing baseline year. See Figures 2-4 for existing (2017) volumes.

Figure 2: 2017 Volumes, US 60 West Corridor


Figure 3: 2017 Volumes, US 60 East Corridor


Figure 4: 2017 Volumes, I-44 Corridor


## 2017 Existing Conditions (No-Build) Operational Analysis

The baseline volumes were analyzed with the current roadway and intersection configurations to determine the current levels of service for the study corridors. Intersection analyses were performed using Synchro, and mainline analyses were performed using FREEVAL. Synchro is a traffic engineering software used to determine macro level LOS, delays, and other operational measures of effectiveness for arterials and intersections. FREEVAL (FREeway EVALuation) is a software designed to faithfully implement the Highway Capacity Manual $6{ }^{\text {th }}$ Edition (HCM) operational analysis computations for undersaturated and oversaturated directional freeway facilities, which incorporate basic freeway segments, weaving segments, and merge and diverge segments. Of particular note, FREEVAL utilizes a Truck to Passenger Car Equivalent (ET) of 2.0 , meeting the recommendations of the $\mathrm{HCM} 6{ }^{\text {th }}$ Edition. Locations currently experiencing conditions of LOS D or worse are identified below and were used as indicators of future congestion, or near-congestion, and areas of higher delay, in order to develop a robust list of potential improvement projects for screening, evaluation and prioritization.

The only study corridor currently experiencing segments operating at LOS D or worse is the US 60 West Corridor, specifically in the eastbound direction. All segments along the US 60 East and I-44 Corridors currently operate at LOS C or better. Eight segments on US 60 West operate at LOS D or worse during the PM peak. These segments are primarily located between the National Avenue interchange and the US-65 interchange. There are no segments that operate at LOS D or worse during the AM peak. The results for all segments operating at LOS D or worse are shown in Table 1. For the full existing segment analysis results see Appendix B.

Table 1: Existing Segments Experiencing LOS D or Worse

|  |  | PM Peak Hour |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  | Density <br> Description <br> (veh/mi/In) | V/C |
| US 60 West Corridor - Eastbound | Type | LOS |  |  |
| Between National Ave Off-Ramp and National Ave On-Ramp | Basic | F | 51.0 | 0.61 |
| National Ave On-Ramp | Merge | E | 71.3 | 0.88 |
| Between National Ave On-Ramp and Republic Rd Off-Ramp | Basic | F | 119.1 | 0.59 |
| Republic Off-Ramp | Diverge | E | 84.4 | 0.88 |
| Between Republic Off-Ramp and BUS-65 On-Ramp | Basic | F | 101.2 | 0.75 |
| BUS-65 On-Ramp | Merge | E | 68.8 | 0.96 |
| Republic On-Ramp | Merge | D | 32.9 | 1.05 |
| US-65 Off-Ramp | Diverge | D | 31.6 | 1.05 |

*LOS = Level of Service | V/C = volume-to-capacity ratio
At the intersection level, several locations currently experience LOS D or worse within each of the three study corridors, as shown in Table 2. As noted in the table, for unsignalized intersections, the LOS and delay for the worst movement is shown. Along the US 60 East corridor, a number of intersections reportedly operate at LOS D or worse; however, it should be noted that the delay at those intersections applies to side street movements with fairly low volumes, not to the heavier volumes along the US 60 mainline. Full intersection results are available in Appendix B.

Table 2: Existing Intersections Experiencing LOS D or Worse

|  |  | AM |  | PM |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Syn_ID | Intersection | LOS | Delay (s/veh) | LOS | Delay (s/veh) |
| US 60 West Corridor |  |  |  |  |  |
| 118* | US 60 WB Ramps \& Hwy MM |  |  | D | 25.3 |
| 115* | US 60 EB Ramps \& Hwy MM | F | 52 | E | 43 |
| 93 | US 60 EB Ramps \& Kansas Expwy |  |  | F | 109.2 |
| 31 | Campbell Ave \& Republic Rd | E | 61.8 | E | 58.7 |
| $62^{*}$ | US 60 \& National Ave EB On-Ramp |  |  | F | 197.1 |
| 46 | US 60 WB Ramps \& Glenstone Ave | D | 41.5 | E | 64.7 |
| US 60 East Corridor** |  |  |  |  |  |
| 5/6* | US 60 \& Highland Springs Blvd | E | 38.5 | F | 573.3 |
| 8/9* | US 60 \& Farm Rd 189 | F | 231.5 | F | 120.2 |
| 12/13* | US 60 \& Farm Rd 193 | F | 102.1 | F | 77.3 |
| $60^{*}$ | US 60 WB Ramps \& Route NN/J | D | 34.1 |  |  |
| 16/17* | US 60 \& Farm Rd 205 | D | 33.9 | E | 47 |
| 20/21* | US 60 \& Farm Rd 213 | E | 38 | D | 30.9 |
| 24/25* | US 60 \& Farm Rd 219 | F | 52.1 | D | 30.9 |
| 29/30* | US 60 \& Farm Rd 223 | F | 78.4 |  |  |
| 33/34* | US 60 \& Farm Rd 229 | E | 46.8 |  |  |
| 36/37 | US 60 \& Hwy 125 | F | 1750.5 | F | 502 |
| 40/41* | US 60 \& Farm Rd 241 |  |  | D | 32.7 |
| I-44 Corridor |  |  |  |  |  |
| 117* | I-44 WB Ramps \& Hwy MM |  |  | F | 75.4 |
| 101 | I-44 WB Ramps \& Chestnut Expwy | D | 36.8 |  |  |
| 62 | I-44 WB Ramps \& Route 13 |  |  | D | 45.8 |
| 40 | I-44 WB Ramps \& Glenstone Ave |  |  | D | 38.9 |
| 8* | I-44 WB Ramps \& Hwy 125 | E | 38 |  |  |

LOS = Level of Service
*At unsignalized intersections, LOS and Delay for the worst movement is shown.
${ }^{* *}$ In the Synchro files, at-grade intersections were coded as two separate intersections (a north and south couplet); however, for the purposes of this table, each couplet is shown on one line and the worst results among the two intersections are shown for each peak.

Figures 5 and 6 illustrate the existing LOS along each corridor and at each of the study intersections for both the AM and PM peak hours.

Figure 5: 2017 No-Build Mainline \& Intersection Levels of Service - AM Peak Hour


Figure 6: 2017 No-Build Mainline \& Intersection Levels of Service - PM Peak Hour


## 2040 No-Build Operational Analysis

Using the OTO Travel Demand Model, growth rates were developed to adjust the baseline volumes to the projected 2040 horizon analysis year. Daily travel demand model outputs were obtained for the OTO's base year of 2012 and the near-term horizon year of 2030. An annual growth rate for each study segment (mainline and ramp) was calculated based on those endpoints, and adjusted within reasonable tolerances to maintain a balanced network. In general, mainline growth rates were assumed to have more accuracy than the ramp rates and were therefore more likely to be held constant (or have a slight adjustment) during the balancing process. The growth rates were then applied to the new 2017 baseline volumes to project to the forecasted 2040 volumes. Growth rates ranged from $0.1 \%$ to $4.75 \%$ at various locations along the study corridors. Figures 7-9 display these projected 2040 volumes.

The methodology used above is common for future year projections in a planning study. It is acknowledged that the travel demand model growth rates should periodically be reviewed and updated to accurately reflect changes in the community and surrounding communities. These changes will allow planners to react more quickly to the changing needs of the transportation system and prioritize projects accurately. Project needs and priorities provided in this report should be subject to change as model updates are made and changes in growth rates and locations become known.

Figure 7: 2040 Volumes, US 60 West Corridor


Figure 8: 2040 Volumes, US 60 East Corridor


Figure 9: 2040 Volumes, l-44 Corridor


The 2040 no-build analysis used the same tools as the existing conditions analysis to determine how well the mainline and intersections along the corridor can be expected to operate under the future no-build conditions.

During the AM peak hour, several basic segments along eastbound US 60 are expected to continue to operate at LOS D or worse. In addition, several westbound US 60 segments are expected to operate at LOS D or worse by 2040. The PM peak hour is projected to experience wider-ranging congestion than the AM peak, with 13 segments along the US 60 West Corridor experiencing LOS D or worse. During the PM peak, there are also a number of segments along I-44 in both directions that are projected to operate at LOS D. All of the segments projected to operate at LOS D or worse are shown in Table 3 below. Full corridor results are provided in Appendix C.

Note that the 2040 No-Build scenario includes auxiliary lanes on US-60 from National Avenue to Glenstone Avenue. This project is currently under construction by MoDOT. Even with this project in place, spillback issues related to the Glenstone Avenue and US-65 interchanges are forecasted to cause eastbound congestion issues.

In the 2040 No-Build intersection analysis, signal timings were optimized in the Synchro files, assuming that by 2040 adjustments would be made to ensure that the signals are operating at their fullest potential. For this reason, a small number of intersections that were shown to be experiencing LOS D or worse in 2018 are projected to operate at LOS C or better in 2040. Those intersections are excluded from Table 4. However, there are several other additional intersections that are expected to degrade to LOS D or worse with the projected 2040 volumes. Table 4 lists all of these intersections; Appendix C contains the full analysis results for all intersections.

Figures 10 and 11 also display the full LOS results for both segments and intersections for the 2040 no-build conditions.

Table 3: 2040 Segments Experiencing LOS D or Worse

|  |  | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Description | Type | LOS | Density (veh/mi/ln) | D/C | LOS | Density (veh/mi/ln) | D/C |
| US 60 West Corridor - Eastbound |  |  |  |  |  |  |  |
| MO-13 On-Ramp | Merge |  |  |  | D | 32.8 | 0.84 |
| Between MO-13 On-Ramp and S Campbell Off-Ramp | Basic |  |  |  | F | 56.0 | 0.56 |
| S Campbell Off-Ramp | Diverge |  |  |  | E | 53.2 | 0.84 |
| Between S Campbell Off-Ramp and On-Ramp | Basic |  |  |  | E | 40.5 | 0.61 |
| Between S Campbell On-Ramp and S National Off-Ramp | Weave | D | 30.2 | 0.83 | F | 97.9 | 0.72 |
| Between National Ave Off-Ramp and On-Ramp | Basic |  |  |  | F | 119.1 | 0.67 |
| National Ave On-Ramp | Merge |  |  |  | E | 87.4 | 1.03 |
| Between National Ave On-Ramp and Republic Rd Off-Ramp | Basic |  |  |  | F | 124.4 | 0.68 |
| Republic Off-Ramp | Diverge |  |  |  | E | 89.5 | 1.03 |
| Between Republic Off-Ramp and BUS-65 On-Ramp | Basic |  |  |  | F | 107.6 | 0.86 |
| BUS-65 On-Ramp | Merge |  |  |  | E | 70.4 | 1.12 |
| Republic Rd On-Ramp | Merge |  |  |  | D | 30.8 | 1.22 |
| US-65 Off-Ramp | Diverge |  |  |  | D | 29.2 | 1.22 |
| US 60 West Corridor - Westbound |  |  |  |  |  |  |  |
| US-65 NB On-Ramp | Merge | D | 28.2 | 0.71 |  |  |  |
| Between S Glenstone Off-Ramp and On-Ramp | Basic | D | 27.7 | 0.76 |  |  |  |
| S Glenstone On-Ramp | Merge | D | 28.7 | 0.86 |  |  |  |
| I-44 Corridor - Eastbound |  |  |  |  |  |  |  |
| MO-13 On-Ramp | Merge |  |  |  | D | 29.1 | 0.73 |
| Between MO-13 On-Ramp and Glenstone Off-Ramp | Basic |  |  |  | D | 26.4 | 0.73 |
| Glenstone Off-Ramp | Diverge |  |  |  | D | 28.5 | 0.73 |
| Glenstone On-Ramp | Merge |  |  |  | D | 29.9 | 0.73 |
| Between Glenstone On-Ramp and US-65 SB Off-Ramp | Basic |  |  |  | D | 26.3 | 0.73 |
| US-65 SB Off-Ramp | Diverge |  |  |  | D | 29.0 | 0.73 |
| US-65 NB On-Ramp | Merge |  |  |  | D | 28.2 | 0.71 |
| I-44 Corridor - Westbound |  |  |  |  |  |  |  |
| Between US-65 On-Ramp and Glenstone Off-Ramp | Basic |  |  |  | D | 26.0 | 0.72 |
| Glenstone Off-Ramp | Diverge |  |  |  | D | 32.6 | 0.72 |
| Glenstone On-Ramp | Merge |  |  |  | D | 31.3 | 0.79 |
| Between Glenstone On-Ramp and MO-13 Off-Ramp | Basic |  |  |  | D | 29.3 | 0.79 |
| MO-13 Off-Ramp | Diverge |  |  |  | D | 30.5 | 0.79 |
| MO-13 On-Ramp | Merge |  |  |  | D | 28.7 | 0.70 |
| West Bypass Off-Ramp | Diverge |  |  |  | D | 28.3 | 0.70 |

LOS = Level of Service | D/C = demand-to-capacity ratio

Table 4: 2040 Intersections Experiencing LOS D or Worse

*At unsignalized intersections, LOS and Delay for the worst movement is shown.
** In the Synchro files, at-grade intersections were coded as two separate intersections (a north and south couplet); however, for the purposes of this table, each couplet is shown on one line and the worst results among the two intersections are shown for each peak.

Figure 10: 2040 No-Build Mainline \& Intersection Levels of Service - AM Peak Hour


Figure 11: 2040 No-Build Mainline \& Intersection Levels of Service - PM Peak Hour


## Safety Assessment

Crash data was obtained for the five-year period from 2012 through 2016 for each of the study corridors. Mainline crash totals for each corridor are displayed in Table 5 below. Distributions of those crashes along each corridor are shown in Figure 12.

Table 5: Total Mainline Crashes (2012-2016)

|  | $\mathbf{2 0 1 2}$ | $\mathbf{2 0 1 3}$ | $\mathbf{2 0 1 4}$ | $\mathbf{2 0 1 5}$ | $\mathbf{2 0 1 6}$ | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| US 60 West | 120 | 112 | 92 | 79 | 70 | $\mathbf{4 7 3}$ |
| Eastbound | 115 | 76 | 59 | 73 | 58 | $\mathbf{3 8 1}$ |
| Westbound |  |  |  |  |  |  |
| US 60 East | 27 | 18 | 24 | 34 | 33 | $\mathbf{1 3 6}$ |
| Eastbound | 29 | 22 | 22 | 32 | 43 | 148 |
| Westbound | 97 | 98 | 87 | 70 | 85 | 437 |
| I-44 | 104 | 98 | 110 | 98 | 92 | 502 |
| Eastbound | 492 | 424 | 394 | 386 | 381 | $\mathbf{2 , 0 7 7}$ |
| Westbound |  |  |  |  |  |  |
| Grand Total |  |  |  |  |  |  |

Figure 12: Crash Distribution


Corridor crash rates along I-44 and US 60 were developed. Those rates were then compared to the statewide average rate for similar freeways during the same time period. The resulting Safety Ratio indicates whether the study corridors are better ( $<1.0$ ) or worse ( $>1.0$ ) than the statewide average. Segments shown in yellow, orange, and red on Figure 13 have been found to exceed the statewide average. These are also shown in Table 6 below.

Table 6: Segments with a Safety Ratio > 1.0

|  | Segment Begin | Segment End | Average Crash Rate <br> (crashes per 100 MVM*) | Safety Ratio |
| :--- | :---: | :---: | :---: | :---: |
| US 60 West |  |  |  | 158.78 |
| EB | Kansas Expy | Campbell Ave | 1.78 |  |
| EB | Campbell Ave | National Ave | 95.11 | 1.04 |
| EB | National Ave | Glenstone Ave | 99.82 | 1.11 |
| EB | Glenstone Ave | US 65 | 121.52 | 1.79 |
| WB | End of Corridor | US 65 | 128.35 | 1.40 |
| WB | Glenstone Ave | National Ave | 131.20 | 1.49 |
| US 60 East |  |  |  |  |
| EB | Start of Corridor | Farm Rd 189 | 198.60 | 2.18 |
| EB | Hwy J/NN | Farm Rd 205 | 105.10 | 1.18 |
| WB | Farm Rd 241 | Rte. 125 | 94.28 | 1.03 |
| WB | Farm Rd 213 | Farm Rd 205 | 93.16 | 1.04 |
| WB | Hwy J/NN | Farm Rd 189 | 91.47 | 1.02 |
| WB | Farm Rd 189 | Start of Corridor | 102.10 | 1.12 |
| I-44 |  |  |  |  |
| EB | Rte. 266 | West Bypass | 116.52 | 1.28 |
| WB | End of Corridor | Rte. 125 | 98.60 | 1.09 |
| WB | Glenstone Ave | Kansas Expwy | 91.83 | 1.04 |
| WB | Rte. 266 | Hwy B/MM | 111.57 | 1.24 |
| WB | Hwy B/MM | US 60 | 109.86 | 1.24 |
| * |  |  |  |  |

* $M V M=$ million vehicle-miles

Intersections along each of the corridors were also evaluated for safety. A total of 936 crashes occurred at intersections during the five-year analysis period. Intersection crashes per study corridor and by year are shown in Table 7.

Table 7: Crash Totals at Study Intersections, by Study Corridor

|  | $\mathbf{2 0 1 2}$ | $\mathbf{2 0 1 3}$ | $\mathbf{2 0 1 4}$ | $\mathbf{2 0 1 5}$ | $\mathbf{2 0 1 6}$ | Total |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| US 60 West | 88 | 64 | 58 | 50 | 86 | $\mathbf{3 4 6}$ |
| US 60 East | 55 | 36 | 45 | 54 | 58 | $\mathbf{2 4 8}$ |
| l-44 | 80 | 86 | 47 | 66 | 63 | $\mathbf{3 4 2}$ |
| Total | $\mathbf{2 2 3}$ | $\mathbf{1 8 6}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 0}$ | $\mathbf{2 0 7}$ | $\mathbf{9 3 6}$ |

A five-year crash rate was calculated using the number of crashes within each intersection's area of influence and the number of entering vehicles (count data from 2016). Locations with a calculated value of 1.0 or greater are shown as orange and red in Figure 13, and are listed in Table 8.

Table 8: Intersections with Crash Rate > 1.0

| Location | Total Crashes | Crash Rate <br> (per MEV*) |
| :--- | :---: | :---: |
| US 60 East | 76 | 1.32 |
| $\quad$ US 60 \& Hwy 125 |  |  |
| I-44 | 27 | 1.17 |
| I-44 EB Ramps \& Chestnut Expwy | 58 | 1.71 |
| I-44 WB Ramps \& West Bypass | 43 | 1.23 |
| I-44 EB Ramps \& West Bypass | 62 | 1.59 |
| I-44 WB Ramps \& Kansas Expwy | 47 | 1.24 |
| I-44 EB Ramps \& Kansas Expwy | 38 | 1.11 |
| I-44 WB Ramps \& Glenstone Ave |  |  |

Figure 13: Corridor and Intersection Safety Ratio


Crash severity was assessed along each corridor. Table 9 summarizes the total crashes for each corridor by severity. During the five-year analysis period, a total of 11 fatal crashes were recorded along the l-44 corridor, of which 8 occurred along the mainline and 3 occurred at intersections. Along the US 60 West corridor, an additional 5 fatal crashes were recorded, all on the mainline. There were no fatalities recorded along the US 60 East corridor. Figure 14 displays the locations of all reported fatal crashes.

## Table 9: Crash Severity

| Corridor | Fatal | Disabling Injury | Minor Injury | Property Damage Only | Total |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Mainline Crashes |  |  |  |  |  |
| US 60 West | 5 (1\%) | 19 (2\%) | 255 (30\%) | 575 (67\%) | 854 |
| US 60 East | 0 (0\%) | 20 (7\%) | 65 (23\%) | 199 (70\%) | 284 |
| I-44 | 8 (1\%) | 24 (3\%) | 195 (21\%) | 712 (75\%) | 939 |
| All Corridors | 13 (1\%) | 63 (3\%) | 515 (25\%) | 1,486 (71\%) | 2,077 |
| Intersection Crashes |  |  |  |  |  |
| US 60 West | 0 (0\%) | 5 (2\%) | 115 (33\%) | 226 (65\%) | 346 |
| US 60 East | 0 (0\%) | 15 (6\%) | 61 (25\%) | 172 (69\%) | 248 |
| I-44 | $3(1 \%)$ | 9 (3\%) | 87 (25\%) | 243 (71\%) | 342 |
| All Corridors | 3 (0\%) | 29 (3\%) | 263 (28\%) | 641 (69\%) | 936 |

Figure 14: Fatal Crashes (2012-2016)


Crash types and contributing circumstances were obtained for crashes that occurred along the study corridor mainlines and analyzed for trends. See the graphs in Figure 15 for crash type/contributing circumstance information by severity for all three study corridors.

Along the US 60 West Corridor, the predominant crash type experienced over the five-year crash analysis period was rear-end crashes. In the eastbound direction, rear-end crashes made up 59\% of crashes, while in the westbound direction $53 \%$ were rear-end crashes. The likely cause of rear end crashes on a facility such as this, where there are no at-grade intersections, is due to unexpected traffic slow-downs due to congestion or road curvature. Other common crash types/contributing circumstances include out-of-control crashes (15\% eastbound, 19\% westbound) and passing crashes ( $13 \%$ eastbound, $14 \%$ westbound). These types of crashes are not uncommon for freeway-type facilities.

Along the US 60 East Corridor, the predominant crash type is the rear-end crash (49\% eastbound, $61 \%$ westbound). The difference between this corridor and the US-60 West corridor is that most of the intersections are at-grade. Therefore, many of the rear-end crashes may be attributable to vehicles slowing down to make turns. The next most common crash type is angle crashes ( $22 \%$ eastbound, $12 \%$ westbound), which would also be attributable to the presence of at-grade intersections.

Along the I-44 Corridor, the most common crash type is out-of-control crashes ( $31 \%$ eastbound, $32 \%$ westbound) followed closely by rear end crashes ( $29 \%$ eastbound, $32 \%$ westbound). Like the US 60 West Corridor, the I-44 corridor is an access-controlled facility, and rear-end crashes are likely attributable to traffic slowdowns. Out-of-control crashes can be caused by a number of things but could include driver over-correction due to roadway curvature. Uncontrollable circumstances such as poor weather conditions and speeding can also contribute to these types of crashes.

Figure 15: Crash Type/Contributing Circumstance


## Roadway Assessment

To perform the roadway assessment of the three study corridors, existing pavement maintenance plans and as-built drawings were provided by MoDOT. In addition, a site visit was conducted along each corridor and aerial photography was used to help supplement the analysis. The analysis primarily assessed horizontal alignments and superelevations, vertical alignments, ramp geometrics, acceleration/deceleration lengths, clear zone obstructions, and stopping sight distances.

The mainline horizontal curvature was assessed as to whether its operational speed matched its design speed. In a number of locations this was found to not be the case, as shown highlighted in solid orange and red on Figure 16. This is particularly true along the US 60 West Corridor, which has several horizontal curves. There are six locations where the operational speed is more than 15 mph slower than the design speed, and another eight locations where the operational speed is 5 to 10 mph slower than the design speed. The US 60 East Corridor, which in comparison to the west corridor is very straight, does not have any horizontal curves that operate at speeds slower than design speeds. The l-44 Corridor has just a few problem locations: two curves that operate more than 15 mph below design speed, and one curve that operates $5-10 \mathrm{mph}$ below design speed.

Mainline vertical curvature was also assessed as to whether its operational speed matched its design speed. Curves where the operational speed was found to be below the design speed are shown as dashed orange and red on Figure 16. Both the US 60 West Corridor and the I-44 Corridor are fairly flat and each have only one vertical curve segment that operates below design speed. The majority of the westbound lanes of the US 60 East Corridor, however, operate at speeds below the design speed due to the vertical curvature.

The operational speed at each interchange ramp was also assessed versus the design speeds. At almost every interchange along all three corridors, there is at least one ramp that operates below design speeds. These are shown with orange and red dots on Figure 16.

The acceleration and deceleration lengths for each interchange ramp were analyzed and compared to Tables 10-3 and 10-5 in the 2011 AASHTO Green Book to determine if the lengths match or exceed requirements. At most of the interchanges along the three corridors, there is at least one ramp with acceleration or deceleration lengths less than what is required. Many are more than 200 feet shorter than what is required. Deficient lengths are shown with orange and red bars on Figure 17.

Each corridor was assessed for clear zone obstructions. The required size of the clear zone is generally determined by the traffic volumes and speeds along the roadway. For the three study corridors, the assumed clear zone was 34 feet. As shown in Figure 17, a number of obstructions were observed along each of the corridors. On the I-44 Corridor, the obstructions appear to be clustered around the MO Hwy 13/Kansas Expressway and Glenstone Avenue interchanges. Along the US 60 Corridors, the infractions are more spread out. Obstructions in the clear zone can include overhead signage, other fixed objects, steep embankment and/or cut slopes, and high fills, but in the case of this study primarily included tall rock outcroppings.

Intersection sight distances were analyzed along the US 60 East Corridor. Sight triangles, areas that should be free of obstructions that block a driver's view of potentially conflicting vehicles, were determined for the appropriate speeds and volumes along the corridor. There are currently four locations where the intersection sight distances do not meet criteria, due to obstructions within the required sight triangles or due to the vertical curvature of the roadway. The problem locations along US 60 are at its intersections with Highland Springs Boulevard, Farm Road 193, Farm Road 213, and Farm Road 223, as shown in Figure 17. The US 60 West and I-44 Corridors do not have any at-grade intersections, and intersections at ramp terminals were not included in this analysis.

Items such as drainage, signing, lighting, guardrai//guard cable, and barrier were reviewed with respect to how they might need to be installed and/or upgraded to the latest standard with a proposed improvement project in the immediate vicinity. There is a drainage issue on the US 60 East Corridor near Farm Road 213 that would require a grade raise of the westbound lanes should a proposed freeway section be implemented. There are also several ongoing guardrail projects along the US 60 West Corridor that involve upgrading existing guardrail to the current Midwest Guardrail System standard.

Figure 16: Horizontal and Vertical Geometry


Figure 17: Roadway Safety and Operational Issues


## Bridge Assessment

Existing bridge inspection reports were obtained from MoDOT and reviewed for each bridge along the three study corridors. Items considered in the overall bridge rating include the bridge deck (the surface on which vehicles travel), the superstructure (which transfers the load of the deck and the bridge traffic to the substructure), and the substructure (which provides support for the entire bridge). Table 10 provides the bridge rating scale and a description for each category as provided by FHWA.

Table 10: Bridge Condition Rating Categories

| Rating | Condition <br> Category |  |
| :---: | :--- | :--- |
| 9 | Excellent | Description |
| 8 | Very Good | No problems noted. |
| 7 | Good | Some minor problems. |
| 6 | Satisfactory | Structural elements show some minor deterioration. |
| 5 | Fair | All primary structural elements are sound but may have minor section loss, cracking, spalling, or scour. |
| 4 | Poor | Advanced section loss, deterioration, spalling, or scour. |
| 3 | Serious | Loss of section, deterioration, spalling, or scour have seriously affected primary structural components. Local failures <br> are possible. Fatigue cracks in steel or shear cracks in concrete may be present. |
| 2 | Critical | Advanced deterioration of primary structural elements. Fatigue cracks in steel or shear cracks in concrete may be <br> present or scour may have removed substructure support. Unless closely monitored, it may be necessary to close the <br> bridge until corrective action is taken. |
| 1 | Imminent <br> Failure | Major deterioration or section loss present in critical structural components, or obvious loss present in critical <br> structural components, or obvious vertical or horizontal movement affecting structural stability. Bridge is closed to <br> traffic, but corrective action may be sufficient to put the bridge back in light service. |

Source: FHWA

None of the bridges along any of the three study corridors has a Poor or worse rating on the FHWA scale. There are two bridges that currently have a Fair rating and both are along the l-44 Corridor. One is the Farm Road 127 overpass, and the other is the US 65 southbound bridge over I-44. Along I-44 there are also four bridges with a Satisfactory rating. All remaining I-44 bridges are rated Good or better. Along the US 60 West Corridor three bridges have a Satisfactory rating, while the remaining have a Good or better rating. The US 60 East Corridor bridges are rated Good or better. Figure 18 shows the overall condition rating for all of the existing bridges.

In addition to the overall bridge ratings, individual ratings for each bridge deck, superstructure, and substructure were observed to determine whether there were specific deficiencies in one of those elements that may need to be addressed. Figures 19-21 show these individual ratings. As with the overall rating, there are no individual elements that currently have a Poor or worse rating.

Figure 18: Overall Condition of Existing Bridges


Figure 19: Existing Bridge Deck Ratings


Figure 20: Existing Bridge Superstructure Ratings


Figure 21: Existing Bridge Substructure Ratings


## Project Development

## Evaluation Process

Utilizing the outputs of the existing and future no-build conditions analysis, a list of projects was developed. In particular, the operational assessment provided levels-of-service (LOS) that were used to identify capacity deficiencies. In regards to freeway capacity, the HCM methodology was used (through FREEVAL) to determine locations with capacity deficiencies. Freeway LOS is based on density, in terms of passenger cars per mile per lane (which is subsequently related to speed and flow). For LOS D or better, the flow rate (or capacity) of a freeway lane at 65 MPH is approximately 2,000 pcphpl. HCM indicates that auxiliary lane capacity can be as low as half of a freeway lane's capacity for segments shorter than 3,000 feet, but only slightly reduced from 2,000 pcphpl for longer segments. In segments with two mixed-flow lanes and one auxiliary lane, capacities can range from 5,000 pcphpl up to nearly 6,000 pcphpl before the freeway segment reaches LOS E. Segment length and the volume of merging and diverging movements affect the capacity of an auxiliary lane. Freeway segments and intersections experiencing LOS D or worse in 2017 or 2040 were considered for improvements. In addition, the historical crash data analysis provided crash rates, which were used to identify locations with safety concerns. Freeway segments and intersections with a crash rate greater than 1.0 were considered for improvements. At these locations, crash types were further evaluated for patterns and deficiencies that were correctable through geometric design and traffic control measures.

Roadway and bridge deficiencies were considered when identifying projects based on poor LOS and high crash rates. Projects were not developed on the basis of roadway and bridge deficiencies alone, but the correction of such deficiencies was included in projects as appropriate.

Other identified operational deficiencies - primarily excessive queue lengths at ramp terminal intersections - were also considered for improvements. Excessive queue lengths on freeway off-ramps contribute to an increased frequency of crashes and a reduction in safety on the ramp and freeway. These identified locations were not experiencing a poor LOS or high crash rate; however, the traffic volumes, lane loading, and queue lengths were determined to justify the need for improvements.

Table 11 lists the 20 projects that were identified through this process. Brief descriptions of each project, as well as the identified capacity and/or crash issues, are also provided. Appendix F contains detailed exhibits for each project.

It should be noted that the scopes of each project identified in this report should include, during the actual project development phase, consideration for items to accommodate additional future growth beyond the 2040 horizon - as reasonable - such as right-of-way acquisition/preservation for future lane or roadway additions.

One issue discussed and considered by the study team, for both the I-44 and US-60 West corridors, was adding auxiliary lanes vs. widening to provide three basic through lanes in each direction. The study team found the following:

- Based on the operational analysis, much of the perceived congestion along both corridors is due in large part to heavy merging, diverging, and weaving volumes or existing capacity issues at ramp terminal locations, such as the eastbound left-turn or westbound right-turn at US-60 and National Avenue.
- One indicator of the need for additional basic through capacity need is the traffic volumes between the off-ramps and on-ramps of a given interchange, because they are free of any movements related to that interchange. Along the busiest part of the US-60 West corridor, such volumes range from approximately $2,500 \mathrm{vph}$ to $4,200 \mathrm{vph}$. The capacity of a single lane at freeway speeds is approximately $2,400 \mathrm{vph}$. Although the projected volumes are nearing this capacity by 2040, they are still below the threshold (with the exception of the Glenstone Avenue interchange, for which the study team developed an operational solution). Through volumes on I-44 are lower and thus also fall below the threshold.
- Capacity analyses performed for this study indicate that auxiliary lanes and capacity/storage enhancements at ramp junctions are expected to adequately accommodate traffic through projected 2040 conditions.
- While six basic through lanes (three per direction) would provide significant capacity improvements through the corridors, it would come at a higher cost than installing auxiliary lanes - which, as described above, provide similar benefits. Since I-44 and US-60 have relatively wide median sections, the most economical place to widen for a new basic through lane would be to the inside. Widening to the inside would also maintain more of the recent auxiliary lane investments, and any new auxiliary lanes would not be "throwaway" projects when the time came for widening to six basic lanes. Therefore, installing auxiliary lanes is a very logical first step to enhancing capacity along the corridors. Auxiliary lanes address the needs through at least 2040 based on the analysis of this report. As described earlier in the section on "2020 No-Build Analysis", future periodic reviews of the travel demand model are needed to update growth rates and continue to guide prioritization of regional needs. Widening to six basic lanes will likely ultimately be needed, just not within the time horizon of this study.

Once identified, the geometric modifications associated with each project were then coded into Synchro and/or FREEVAL, as applicable, and analyzed for both the baseline (2018) and future forecasted (2040) volume scenarios. The results of these "Build" analyses were then compared to the No-Build results for the same years. This process helped to prioritize the projects, as described in more detail in the Prioritization section of this document.

## Cost Estimates

For each of the identified projects, a conceptual engineer's opinion of probable construction cost was developed. This included all grading and drainage costs, pavement base and surface costs, bridge costs, and miscellaneous costs (such as signage, signals, lighting, guardrail, etc.) Other estimated amounts for design, survey, utility relocation, right-of-way, and contingency were included as well. Table 11 includes the total estimated cost for each project. For the details of the cost estimates, see Appendix G.

## Table 11: Project Development List

| Proj \# | Project Location / Cost | Project Description | 2040 LOS Issues | Crash/Other Issues |
| :---: | :---: | :---: | :---: | :---: |
| 60W-1 | US 60 from west of Glenstone Avenue to the US 65 on-ramp \$16,781,000 | Provide an eastbound braided ramp roadway for direct access to the US 65 ramp and provide a Diverging Diamond Interchange (DDI) at Glenstone to reconfigure access to US 60 . Project should be coordinated with City's future Republic Road extension plans. | Glenstone \| North Ramp: LOS (AM: E, PM: F) Mainline, Glenstone-US 65: LOS (EB PM: D-E) Mainline, US 65-Glenstone: LOS (WB AM: D) | Mainline, National - US 65: High crash rate |
| 60W-2 | US 60/360 at Hwy MM \$934,000 | Signalize and add left-turn lanes at both ramp terminals. | North Ramp: LOS (AM: F, PM: E) South Ramp: LOS (AM/PM: F) | -- |
| 60W-3 | US 60 at Sunshine Street (Route 413) $\$ 4,846,000$ | Convert interchange to a DDI and relocate nearby drive access west of the interchange. | Initial analysis identified potential LOS issues, but refined analysis did not. Project was removed from further consideration. | -- |
| 60W-4 | US 60 at West Bypass (Route FF / US 160) \$4,936,000 | Convert interchange to a DDI and relocate nearby drive access west of the interchange. | Initial analysis identified potential LOS issues, but refined analysis did not. Project was removed from further consideration. | -- |
| 60W-5 | US 60 at US 65 $\$ 870,000$ | Extend the westbound-to-southbound deceleration ramp and the southbound-toeastbound acceleration ramp. | -- | SB-to-EB loop ramp: Substandard acceleration length entering US-60 |
| 60W-6 | US 60 at National Avenue \$1,248,000 | Add a 3rd left-turn lane at the eastbound offramp, add a third right-turn lane at the westbound off-ramp, and provide a mainline option exit lane to the eastbound off-ramp. | North Ramp: LOS (AM/PM: F) <br> South Ramp: LOS (AM: F, PM: E) | EB mainline, Campbell-Glenstone: High crash rate WB mainline, National-Glenstone: High crash rate |
| 60E-1 | US 60 at Route 125 $\$ 14, \mathbf{2 6 3 , 0 0 0}$ | Convert at-grade signalized intersection to a grade separated interchange with double "peanut" roundabouts. | Intersection: LOS (AM/PM: F) | Intersection: High crash rate WB mainline east of intersection: High crash rate |
| 60E-2 | US 60 from Highland Springs Boulevard to Hwy J/NN \$12,728,000 | Close at-grade intersections and construct new outer roads and new freeway roadways, and signalize the westbound off-ramp at the Highway $\mathrm{J} / \mathrm{NN}$ interchange. | Intersections: LOS (AM/PM: F) J / NN North Ramp: LOS (AM: F) | WB mainline west of intersection: High crash rate EB mainline, Highland Springs - FR 189: High crash rate |
| 60E-3 | US 60 at Farm Road 189 \$24,908,000 | Convert at-grade intersection to a gradeseparated interchange. Close at-grade intersections, and construct new outer roads and new freeway segments from Highland Springs Boulevard to Highway J / NN interchange. Signalize the westbound off-ramp at the Highway J/ NN interchange. | Intersection: LOS (AM/PM: F) J / NN North Ramp: LOS (AM: F) | WB mainline east/west of intersection: High crash rate EB mainline, Highland Springs - FR 189: High crash rate |
| 60E-4 | US 60 from Hwy J/ NN to just east of Farm Road 213 $\$ 15,277,000$ | US 60 from Hwy J / NN to just east of Farm Road 213 - Close at-grade intersections and construct new outer roads and new freeway roadways. | Intersections: LOS (AM/PM: Range from E to F) | WB mainline west of FR 213 intersection: High crash rate $E B$ mainline east of $J / N N$ intersection: High crash rate |


| Proj\# | Project Location / Cost | Project Description | 2040 LOS Issues | Crash/Other Issues |
| :---: | :---: | :---: | :---: | :---: |
| 60E-5 | US 60 from just east of Farm Road 213 to Route 125 <br> \$12,314,000 | Close at-grade intersections and construct new outer roads and new freeway roadways. | Intersections: LOS (AM/PM: Range from D to F) | -- |
| 60E-6 | US 60 from Route 125 to Farm Road 247 \$11,508,000 | Close at-grade intersections and construct new outer roads and new freeway roadways. | Intersections: LOS (AM: D) | WB mainline east of Hwy Route 125: High crash rate |
| 44-1 | Interstate 44 from Route 13 to US 65 \$29,628,000 | Provide auxiliary lanes between interchanges and provide an added 2nd right-turn lane for the westbound off-ramp at Route 13, including minor shoulder improvements at the Glenstone interchange. | Mainline, Route 13 - US-65: LOS (EB/WB PM: D) Kansas North Ramp: 2040 LOS (AM: F) | WB Mainline, Rte. 13 - Glenstone: High crash rate Glenstone \| WB ramp terminal: High crash rate Kansas | both ramp terminals: High crash rate |
| 44-2 | Interstate 44 at Highway MM / Highway B \$4,487,000 | Construct roundabouts at both ramp terminals (tie-in frontage road on the north-side) and extend all acceleration and deceleration ramps. | North Ramp: LOS (AM: E and PM: F) South Ramp: LOS (PM: D) | -- |
| 44-3 | Interstate 44 at Chestnut Expressway (Route 266) \$416,000 | Extend and provide positive separation for westbound acceleration lane. | -- | WB mainline west of interchange: High crash rate |
| 44-4 | Interstate 44 at Kearney Street (Route 744) \$1,119,000 | Extend and provide positive separation for westbound acceleration lane. | -- | WB acceleration lane from Kearney St: High crash rate |
| 44-5 | Interstate 44 at West Bypass (US 160) \$678,000 | Add a 2nd left-turn lane at the westbound offramp traffic signal and extend the eastbound deceleration and westbound acceleration lanes. | North Ramp: LOS (AM: D) | EB mainline west of interchange: High crash rate Both ramp terminals: High crash rate |
| 44-6 | Interstate 44 at US 65 $\$ 15,072,000$ | Construct a southbound-to-eastbound flyover ramp and eliminate the existing southbound-toeastbound cloverleaf ramp. | -- | Cloverleaf: Substandard weave distance |
| 44-7 | Interstate 44 at Mulroy Road (Farm Road 199) \$3,465,000 | Construct roundabouts at both ramp terminals (tie-in frontage road on the south-side) and extend all acceleration and deceleration ramps. | North Ramp: LOS (AM/PM: F) <br> South Ramp: LOS (AM: D) | -- |
| 44-8 | $\begin{aligned} & \text { Interstate } 44 \text { at Route } 125 \\ & \quad \$ 1,199,000 \end{aligned}$ | Signalize the westbound off-ramp terminal, extend the eastbound acceleration and deceleration ramps and westbound acceleration ramp, and close the eastbound off and on-ramps at the old weigh station east of Route 125. | North Ramp: LOS (AM/PM: F) | WB mainline east of interchange: High crash rate |

## Prioritization

Once the projects were identified, the next step was to prioritize the list in order to determine which projects would be the best to implement in the near-term vs. which projects could be put on a longer-term schedule for when additional funding becomes available.

The prioritization was based on Benefit/Cost (B/C) ratios estimated for each recommended project. The methodology was based on standard B/C analyses used for USDOT projects, but was simplified where appropriate to efficiently conduct high-level comparisons suitable for prioritization in the Statewide Transportation Improvement Program (STIP).

The cost (C) portion of the B/C ratio was based on order-of-magnitude estimates developed as described in the previous section. Annual maintenance costs were not estimated as part of this project; they would be anticipated to be correlated with construction costs and were not needed for this comparative analysis.

The benefit (B) portion of the ratio consists of two components: (1) a delay (travel-time) component, and (2) a safety component.

Note: Two other types of benefits are often considered in $B / C$ analyses of transportation projects: vehicle operating cost savings and emissions cost savings. Benefit estimates for these two categories are typically based on vehicle-miles traveled (VMT) and changes in speed. For the purposes of this analysis, overall VMTs are not expected to change appreciably with the improvements studied. Although speeds would be typically expected to improve with operational improvements, operating cost and emissions cost savings typically constitute a fairly small share ( $10-15 \%$ ) of overall benefit estimates. Their inclusion would not be expected to substantially alter the results of this comparative prioritization study.

## Assessing Benefits over Time

To compare all projects on an equal footing, travel-time and safety benefits were calculated for an analysis period covering 2018-2040. Essentially, each improvement was artificially assumed to be constructed in 2018 and to provide benefits until 2040 (the year for which long-term projections were available from the OTO travel demand model). This simplified analysis implicitly assumed a service life for each improvement that lasts until at least 2040. It was structured to answer the question: "Which improvement should be constructed first?" Benefits were monetized for each year, and a discount rate was applied to calculate a present value, as in the equation below:

Present value $=\sum_{n=2018}^{2040} B_{n}(P \mid F, i, n)=\sum_{n=2018}^{2040} B_{n}(i+1)^{-\Delta n}=\sum_{n=2018}^{2040} B_{n}(1.04)^{-\Delta n}$
Where $B_{n}$ represents the travel-time and safety benefits in year $n, i$ is the discount rate (4\%), $P / F, i, n$ is the discount factor, and $\Delta n$ is the number of years "out" from 2018 (e.g., $\Delta n_{2018}=0, \Delta n_{2040}=22$ ).

## Travel-Time Benefits

For projects that result in traffic operational improvements, these improvements were translated to person-time savings (typically delay reductions). The economic benefits were assessed through the concept of Value of Time (VOT) - more specifically, the Value of Travel Time Savings (VTTS).

The USDOT publication Revised Departmental Guidance on Valuation of Travel Time in Economic Analysis, September 27, $2016^{1}$ was a source of guidance in developing assumptions regarding VTTS.

The basic calculation can be stated as follows:

## Travel Time Benefits = (Travel Time Savings) x (\$ Value of Travel Time Savings)

Each of the two parts on the right side of the equation is discussed below.

## Travel Time Savings

Annual travel time savings were calculated as the change in annual vehicle-hours traveled (VHT) associated with each operational improvement. This analysis examined two types of improvements:

- Mainline freeway improvements: The peak-period delay-per-vehicle results from FREEVAL were multiplied by the total number of vehicles in the study corridor during the peak period to obtain peak-period VHT.
- Intersection improvements: The peak-hour delay-per-vehicle results from Synchro were multiplied by the total number of vehicles entering the intersection during the peak period to obtain peak-hour VHT. For off-system intersections affected by the improvements, where counts have not been obtained, estimates were made based on data from nearby intersections for which data were available.

In both cases, VHT reductions were summed over both peak hours/periods, and multiplied by 365 to obtain an estimate of annual peak-period reduction in VHT. These annual estimates were then interpolated over the multi-year analysis period as described above.

## Value of Travel Time Savings (VTTS)

Table 12 summarizes the development of VTTS values for the three study corridors. Per USDOT guidance, VTTS values for non-freight travel were divided into "Local" and "Intercity" trip types, which were further divided into "Personal" and "Business" trip purposes. For each category, factors were applied to the median hourly wage rate to determine a VTTS per personhour. Vehicle occupancy data, in this case extracted from the OTO travel demand model, was used to convert these values to VTTS per vehicle-hour. As Table 12 indicates, assumptions

[^0]regarding the split between local and intercity trips on each corridor were used to develop final corridor-specific VTTS values.

For freight travel, no distinctions were made between local and intercity travel. A slightly higher factor was applied to the median hourly wage rate to reflect truck driver wages and benefits. Vehicle occupancies were assumed to be 1.0 for freight.

Table 12: Computation of Value of Travel Time Savings (VTTS) for the Springfield Freeway Study Corridors

|  |  |  | Non- | eight |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Freight |
|  |  | Personal | Business | Personal | Business |  |
| Ratio for fringe benefit | s adjustment* | 1.0 | 1.46 | 1.0 | 1.46 | 1.54 |
| Estimated average total hourly comp | nsation, $\mathrm{MO}^{* *}$ | \$16.46 | \$24.03 | \$16.46 | \$24.03 | \$27.81 |
| VTTS per person-hour as \% of | otal earnings* | 50\% | 100\% | 70\% | 100\% | 100\% |
| VTTS per | person-hour | \$8.23 | \$24.03 | \$11.52 | \$24.03 | \$27.81 |
| \% of travel that is person | vs. business* | 95.4\% | 4.6\% | 78.6\% | 21.4\% | -- |
| Blended VTTS per | person-hour |  |  |  |  | \$27.81 |
| Average Vehicle Occup | ancy (AVO)*** |  |  |  |  | 1.00 |
| VTTS pe | vehicle-hour |  |  |  |  | \$27.81 |
|  | I-44 |  |  |  |  | 27\% |
| Estimated \% of travel type by facility (derived from counts, flow maps) | US-60 West |  |  |  |  | 5\% |
|  | US-60 East |  |  |  |  | 5\% |
| VTTS per vehicle-hour, by facility | I-44 | \$19.37 |  |  |  |  |
|  | US-60 West | \$15.18 |  |  |  |  |
|  | US-60 East | \$16.39 |  |  |  |  |

*Source: USDOT, 2016
${ }^{* *}$ Non-freight based on Missouri median hourly wage of $\$ 16.46$ (May 2016, BLS); freight based on 2015 national truckdriver hourly wage of $\$ 17,71$ adjusted by $2.00 \%$ inflation to a 2016 value of $\$ 18.06$
***Source: Non-freight = OTO travel demand model, freight = NHTS
Figure 22 is a graphical illustration of how the travel-time component of these benefits was calculated.

Figure 22: Calculation of Travel-Time Benefits


Using the methodology described above, the total travel time benefit for the lifetime of each of the 20 projects is shown in Table 13.

Table 13: Operational Benefits

|  |  | Total Delay (veh-hrs), Both Peak hours |  |  |  |  |  | Project <br> Lifetime Delay Benefit, 2018-2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2018 |  | 2040 |  | $\Delta$ |  |  |
| Project | Segment | NoBuild | Build | No- <br> Build | Build | 2018 | 2040 |  |
| 60W-1 | US-60, National to US-65 | 273.4 | 99.1 | 901.3 | 195.7 | -174.3 | -705.6 | \$14,919,410 |
| 60W-2 | US-60/360, at MM | 4.5 | 10.4 | 8.9 | 15.9 | 5.9 | 7.0 | -\$504,240 |
| 60W-3* | US-60/360, at Route-413 (Sunshine) | 28.2 | 54.2 | 36.0 | 140.6 | 25.9 | 104.6 | \$2,220,849 |
| 60W-4* | US-60, at Route FF / US 160 (West Bypass) | 48.9 | 42.0 | 69.0 | 85.2 | -6.8 | 16.2 | \$585,463 |
| 60W-5 | US-60, at US-65 | 1.8 | 1.5 | 2.2 | 2.0 | -0.2 | -0.1 | \$19,872 |
| 60W-6 | US-60, at National | 108.4 | 69.4 | 1225.3 | 240.6 | -39.0 | -984.7 | \$3,337,919 |
| 60E-1 | US-60, at Route 125 | 241.2 | 11.4 | 302.4 | 16.1 | -229.8 | -286.3 | \$21,243,570 |
| 60E-2 | US-60, Highland Springs to J/ NN | 28.4 | 8.5 | 166.6 | 12.3 | -19.9 | -154.3 | \$1,843,421 |
| 60E-3 | US-60, at FR 189 | 28.4 | 8.5 | 166.6 | 12.3 | -19.9 | -154.3 | \$1,843,421 |
| 60E-4 | US-60, J/ NN to East of FR 213 | 10.6 | 9.4 | 19.3 | 13.4 | -1.2 | -5.8 | \$114,927 |
| 60E-5 | US-60, East of FR 213 to Rte. 125 | 243.5 | 13.6 | 309.3 | 22.1 | -229.9 | -287.2 | \$21,253,834 |
| 60E-6 | US-60, Route 125 to FR 247 | 241.2 | 13.6 | 301.2 | 22.1 | -227.6 | -279.1 | \$21,037,503 |
| 44-1 | I-44, Route 13 (KS Expwy) to US-65 | 54.2 | 40.7 | 86.9 | 63.2 | -13.5 | -23.7 | \$1,478,372 |
| 44-2** | I-44, at MM/B | 13.2 | 13.3 | 33.8 | 19.8 | 0.1 | -14.0 | -\$10,582 |
| 44-3 | I-44, at Chestnut Expwy | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | \$0 |
| 44-4 | 1-44, West of Route 744 (Kearney) | 1.4 | 1.1 | 2.0 | 1.5 | -0.3 | -0.4 | \$35,973 |
| 44-5 | I-44, at Highway 160 (West Bypass) | 29.4 | 20.6 | 45.8 | 31.6 | -8.9 | -14.2 | \$967,075 |
| 44-6*** | I-44, at US-65 | 2.8 | 3.0 | 4.7 | 5.0 | 0.2 | 0.2 | -\$24,944 |
| 44-7 | I-44, at Mulroy | 9.2 | 9.0 | 34.3 | 21.4 | -0.2 | -12.9 | \$21,230 |
| 44-8 | I-44, at Route 125 | 6.3 | 5.7 | 222.7 | 16.8 | -0.6 | -205.9 | \$69,972 |

* Projects 60W-3 and 60W-4 were not carried forward after refined operational analysis did not indicate a need.
**Project 44-2 includes roundabouts at both terminals. Although the project would reduce delays and improve the LOS at the westbound ramp intersection to acceptable levels, it would increase average delays at the eastbound ramps - although not in a meaningful way, as those ramps would still function at LOS B or better. These offsetting improvements result in a slightly negative calculated operational benefit, which is more than offset by the large safety benefit the roundabouts would provide.
${ }^{* * *}$ Project 44-6 was recommended from a safety point and an AASHTO design standpoint; operational issues are not apparent today. The proposed improvement combines off-ramp traffic from two ramps to one (and similarly on-ramp traffic), concentrating volumes and slightly increasing average delays (although remaining at very good levels of service).


## Safety Benefits

Safety benefits were based on each highway improvement's anticipated reduction in crashes. A simplified crash-reduction forecasting process was used for this prioritization study. For each of the improvements recommended, HDR examined relevant Crash Modification Factors from the Highway Safety Manual and FHWA's Crash Modification Factor (CMF) Clearinghouse. The CMFs used are listed in Appendix H. Those factors were then used to develop an expected crash-reduction percentage. In some cases, improvements were only expected to address certain crash types, and this was taken into account when developing the percentage. This percentage was applied to the historical annual crash experience at each location to arrive at an expected annual crash reduction. This crash reduction was then extrapolated to the entire multi-year analysis period similar to the delay reduction.

HDR applied the crash costs shown in Table 14 to the crash reductions to estimate the expected safety benefits of the proposed projects. The distribution of crash severity at a given location was assumed to remain constant over time.

For a graphical representation, the calculation of the safety benefits would be similar to the second row of graphs in Figure 22, replacing the product $\Delta \mathrm{VHT} \times$ VTTS with the number of

Table 14: Comprehensive Crash Cost Assumptions
\(\left.$$
\begin{array}{lc}\begin{array}{l}\text { Severity } \\
\text { Level }\end{array} & \begin{array}{c}\text { Comprehensive } \\
\text { Crash Cost }\end{array}
$$ <br>
\hline Fatality \& \$ 4,008,900 <br>
Disabling Injury \& \$ 216,000 <br>

Evident Injury \& \$ 79,000\end{array}\right\}\) Blended cost for | Minor Injury $=\$ 62,000$ |
| :--- |
| Possible Injury |
| PDO | | $\$ 44,900$ |
| :--- |
| Source: Highway Safety Manual |
| (Blended cost developed by HDR) | crashes reduced $x$ the average crash cost. The "No-Build" annual number of crashes was assumed to grow linearly at the same rate as traffic volumes (i.e., a steady crash rate over time).

Table 15 provides the estimated number of crashes by severity expected to be eliminated per year for each of the studied projects. The total safety benefit for the lifetime of each project is also provided.

Table 15: Safety Benefits

|  |  | Crashes Eliminated per Year |  |  |  |  | ProjectLifetime SafetyBenefit, 2018-2040 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Project | Segment | PDO | Minor <br> Injury | Disabling Injury | Fatal | Total |  |
| 60W-1 | US-60, National to US-65 | 11.5 | 4.6 | 0.3 | 0.0 | 16.4 | \$7,117,924 |
| 60W-2 | US-60/360, at MM | 0.7 | 0.3 | 0.0 | 0.0 | 1.0 | \$406,868 |
| 60W-3* | US-60/360, at Route 413 (Sunshine) | 2.4 | 4.8 | 0.4 | 0.0 | 4.3 | \$2,690,591 |
| 60W-4* | US-60, at Route FF / US 160 (West Bypass) | 2.4 | 0.7 | 0.4 | 0.0 | 2.8 | \$1,198,633 |
| 60W-5 | US-60, at US-65 | 2.2 | 1.2 | 0.0 | 0.0 | 3.4 | \$1,611,596 |
| 60W-6 | US-60, at National | 1.0 | 0.6 | 0.0 | 0.0 | 1.5 | \$798,917 |
| 60E-1 | US-60, at Route 125 | 9.0 | 1.8 | 0.1 | 0.0 | 10.9 | \$3,561,746 |
| 60E-2 | US-60, Highland Springs to J/ NN | 7.2 | 2.7 | 0.7 | 0.0 | 10.6 | \$6,269,664 |
| 60E-3 | US-60, at FR 189 | 7.2 | 2.7 | 0.7 | 0.0 | 10.6 | \$6,269,664 |
| 60E-4 | US-60, J / NN to East of FR 213 | 3.5 | 0.9 | 0.9 | 0.0 | 5.4 | \$4,775,530 |
| 60E-5 | US-60, East of FR 213 to Rte. 125 | 1.6 | 0.7 | 0.2 | 0.0 | 2.5 | \$1,803,325 |
| 60E-6 | US-60, Route 125 to FR 247 | 0.6 | 0.2 | 0.0 | 0.0 | 0.8 | \$322,188 |
| 44-1 | I-44, Route 13 (KS Expwy) to US-65 | 4.3 | 2.4 | 0.2 | 0.0 | 6.9 | \$6,564,257 |
| 44-2 | 1-44, at MM/B | 3.4 | 0.8 | 0.1 | 0.0 | 4.4 | \$3,226,480 |
| 44-3 | I-44, at Chestnut Expwy | 0.3 | 0.0 | 0.0 | 0.0 | 0.4 | \$84,400 |
| 44-4 | 1-44, West of Route 744 (Kearney) | 0.1 | 0.0 | 0.0 | 0.0 | 0.1 | \$10,830 |
| 44-5 | I-44, at Highway 160 (West Bypass) | 2.0 | 0.8 | 0.1 | 0.0 | 3.0 | \$1,656,411 |
| 44-6 | I-44, at US-65 | 2.1 | 0.5 | 0.0 | 0.0 | 2.5 | \$712,917 |
| 44-7 | I-44, at Mulroy | 0.9 | 0.4 | 0.1 | 0.0 | 1.4 | \$1,921,079 |
| 44-8 | 1-44, at Route 125 | 1.3 | 0.1 | 0.0 | 0.1 | 1.5 | \$6,434,223 |

* Projects 60W-3 and 60W-4 were not carried forward after refined operational analysis did not indicate a need.


## Other Benefits

Although delay and safety benefits were the main components of the benefit side of the B/C equation, the prioritization methodology allowed for a category of "other" benefits to be factored in. Only one project was assigned such a benefit - the US 60 East Corridor between Harmony Avenue and Farm Road 219. The benefit was computed to account for the travel time savings that could be expected due to the roadway improvement's expected ability to eliminate the flooding issues along this segment. Based on information from MoDOT staff, this study assumes a flooding event approximately once every five years for a duration of four weeks. During these flooding events, all westbound traffic must be detoured to the eastbound lanes, with one lane operating in each direction in a head-to-head configuration. The crossover to the eastbound lanes occurs at Farm Road 219, and the crossover back to the westbound lanes occurs at Harmony Avenue, which represents a 6,300-foot detour. For the purposes of the benefit calculation, it was assumed that during this detour, peak hour speeds would be reduced from 60 mph to 30 mph and non-peak hour speeds would be reduced to 45 mph . This reduction in travel time was assigned to the hourly traffic volumes for peak and non-peak hours to determine a total event delay. This event delay was normalized to the service life of the mainline lane reconstruction project.

## Benefit / Cost (B/C) Ratio vs. Net Benefit

Ranking projects purely by their benefit-to-cost (B/C) ratio may inadvertently push lower-cost projects to the top of the list, given that it is easier for their benefits to far outweigh their costs than it is with very large, expensive projects. An alternative ranking method involves computing the net benefit of each project (sum of benefits minus the cost, instead of benefits divided by cost). Table 16 shows a prioritized listing of each project using the B/C methodology and Table 17 shows the prioritized listing using the net benefit methodology, for comparison. Figure 23 shows each project on a map with rankings from both prioritization methods provided.

If large projects (>\$9M) and small projects are considered in two different groups, the rankings of the two methods are fairly similar.

As stated in the Executive Summary, the top four large ( $>\$ 9 \mathrm{M}$ ) projects are the same "bundle" in both lists, and really represent two projects: (1) US-60 / Route 125 grade separation, Project 60E-1, and (2) a braided ramp improvement on US-60 in the area from Glenstone Avenue to US-65, Project 60W-1. Projects 60E-5 and 60E-6, the remaining two projects, both obtain nearly all their traffic delay benefits from the US-60 / Route 125 grade separation, and thus should ultimately be prioritized much lower on the list.

The fifth large project, Project 60E-2, is conversion of US-60 to a freeway from Highland Springs Road to Route $\mathrm{J} / \mathrm{NN}$. Its $\mathrm{B} / \mathrm{C}$ ratio is below 1.0 , but from a planning perspective, it is a reasonable project and a reasonable step toward furthering a grade-separated facility on US-60 heading east from US-65.

For smaller projects, the prioritization is very similar using the two methods as well, with five projects falling at or above a $\mathrm{B} / \mathrm{C}$ ratio of 0.9 .

Table 16: Prioritized Projects - Benefit/Cost Methodology


[^1]* Projects 60E-5 and 60E-6 obtain nearly all their traffic delay benefits from project $60 \mathrm{E}-1$, and so are not considered high priority.
** Projects below a B/C ratio of 0.8 should not be considered a high priority within the horizon year (2040).

Table 17: Prioritized Projects - Net Benefit Methodology

| Rank | ID | Segment | Description | Delay Benefits | Safety Benefits | Other <br> Benefits | Total Benefits | Construction Cost | Net Benefit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 60E-1 | US-60, at Route 125 | Convert to Interchange | \$21,243,570 | \$3,561,746 | \$0 | \$24,805,317 | \$11,883,000 | \$12,922,317 |
| 2 | 605-5 | US-60, Eastoffr 213 to Rte. 125 | dose atgrades; add outer reads | \$21,253,034 | \$1,003,325 |  | \$23,057,159 | \$10,104,000 | \$12,863,15? |
| 3 | 6056 | US 60, Route 125 to FR 247 | close at grades; add outer roads | \$21,037,503 | \$310,894 | \$0 | \$21,357,396 | \$0,238,000 | \$12,119,39\% |
| 4 | 60W-1 | US-60, National to US-65 | EB Braided Ramp + Interchange improvements | \$14,919,410 | \$7,117,924 | \$0 | \$22,037,334 | \$14,591,000 | \$7,446,334 |
| 5 | 44-8 | I-44, at Route 125 | Signalize WB ramp, accel/decel improvements, close weigh staion | \$69,972 | \$6,434,223 | \$0 | \$6,504,194 | \$1,049,000 | \$5,455,194 |
| 6 | 60W-6 | US-60, at National | Add turn lanes; improve ramps | \$3,337,919 | \$798,917 | \$0 | \$4,136,836 | \$1,088,000 | \$3,048,836 |
| 7 | 44-5 | I-44, at Highway 160 (West Bypass) | 2nd LT lane WB off-ramp, acceldecl improvements | \$967,075 | \$1,656,411 | \$0 | \$2,623,485 | \$588,000 | \$2,035,485 |
| 8 | 60W-5 | US-60, at US-65 | Accel/Decel improvements | \$19,872 | \$1,611,596 | \$0 | \$1,631,469 | \$750,000 | \$881,468 |
| 9 | 44-3 | 1-44, at Chestut Expwy | Extend and provide positive separation for WB accel | \$0 | \$84,400 | \$0 | \$84,400 | \$356,000 | -\$271,600 |
| 10 | 44-2 | 1-44, at MM/B | Roundabouts at both terminals, acceldecel improvements | -\$10,582 | \$3,226,480 | \$0 | \$3,215,898 | \$3,697,000 | -\$481,102 |
| 11 | 44-4 | 1-44, West of Route 744 (Kearney) | Extend and provide positive separation for WB accel | \$35,973 | \$10,830 | \$0 | \$46,803 | \$919,000 | -\$872,197 |
| 12 | 60W-2 | US-60/360, atMM | Signals and LT lanes at both ramps | -\$504,240 | \$406,868 | \$0 | -\$97,373 | \$814,000 | -\$911,373 |
| 13 | 44-7 | 1-44, at Muliroy | Roundabouts at both terminals, acceldecel improvements | \$21,230 | \$1,921,079 | \$0 | \$1,942,310 | \$2,895,000 | -\$952,690 |
| 14 | 60E-2 | US-60, Highland Springs to J/ NN | close at-grades + add outer roads | \$1,843,421 | \$6,269,664 | \$0 | \$8,113,085 | \$10,558,000 | - $\$ 2,444,915$ |
| 15 | 60E-4 | US-60, J/ NN to East of FR 213 | close atgrades; add outer roads + signalize WB ramps at J / NN | \$114,927 | \$4,775,530 | \$401,750 | \$5,292,207 | \$12,697,000 | -\$7,404,793 |
| 16 | 44-6 | I-44, at US-65 | SB-to-EB flyover | -\$24,944 | \$712,917 | \$0 | \$687,973 | \$13,102,000 | -\$12,414,028 |
| 17 | 60E-3 | US-60, atFR 189 | Convertto Interchange + add outer roads | \$1,843,421 | \$6,269,664 | \$0 | \$8,113,085 | \$20,558,000 | -\$12,444,915 |
| 18 | 44-1 | I-44, Route 13 (KS Expwy) to US-65 | Aux lanes + Interchange Improvements | \$1,478,372 | \$6,564,257 | \$0 | \$8,042,628 | \$25,758,000 | - - $17,715,3{ }^{\text {a }}$ 2 |

[^2]* Projects 60E-5 and 60E-6 obtain nearly all their traffic delay benefits from project $60 \mathrm{E}-1$, and so are not considered high priority.
** Projects with negative benefits should typically not be considered a high priority within the horizon year (2040); however, projects within a reasonable B/C ratio, as shown in Table 16, could be considered.

Figure 23: Prioritized Projects


## Appendix A

## No-Build Mainline and Ramp Volume Diagrams

 (2017 and 2040)
## US 60 West Corridor - Peak Hour Mainline and Ramp Volumes

## 2017



## 2040



US 60 East Corridor - Peak Hour Mainline and Ramp Volumes


## 2040



## I-44 Corridor - Peak Hour Mainline and Ramp Volumes

## 2017



## 2040



## Appendix B

2017 No-Build Operational Analysis

## 2017 No-Build Mainline Analysis Tables

US 60 West Corridor - Eastbound

| Description | Type | Adjusted Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Density (veh/mi/ln) | V/C | LOS | Density (veh/mi/ln) | V/C |
| US-60 Before I-44 EB On-Ramp | Basic | 2,176 | A | 1.1 | 0.03 | A | 2.3 | 0.07 |
| I-44 EB On-Ramp | Merge | 2,311 | A | 2.2 | 0.31 | A | 3.6 | 0.35 |
| Between I-44 EB On-Ramp and Hwy MM Off-Ramp | Basic | 4,622 | A | 5.3 | 0.15 | A | 6.0 | 0.18 |
| Hwy MM Off-Ramp | Diverge | 4,622 | A | 4.5 | 0.15 | A | 5.4 | 0.18 |
| Between Hwy MM Off-Ramp and On-Ramp | Basic | 4,633 | A | 5.1 | 0.15 | A | 5.6 | 0.16 |
| Hwy MM On-Ramp | Merge | 4,654 | A | 9.9 | 0.25 | A | 9.8 | 0.24 |
| Between Hwy MM On-Ramp and MO-413 Off-Ramp | Basic | 4,654 | A | 8.4 | 0.25 | A | 8.2 | 0.24 |
| MO-413 Off-Ramp | Diverge | 4,654 | A | 7.8 | 0.25 | A | 7.5 | 0.24 |
| Between MO-413 Off-Ramp and On-Ramp | Basic | 4,648 | A | 7.8 | 0.23 | A | 7.6 | 0.22 |
| MO-413 On-Ramp | Merge | 4,681 | B | 16.1 | 0.40 | B | 13.7 | 0.33 |
| Between MO-413 On-Ramp and US-160 Off-Ramp | Basic | 4,681 | B | 13.8 | 0.40 | B | 11.4 | 0.33 |
| US-160 Off-Ramp | Diverge | 4,681 | B | 15.1 | 0.40 | B | 12.3 | 0.33 |
| Between US-160 Off-Ramp and On-Ramp | Basic | 4,673 | B | 12.4 | 0.36 | A | 9.6 | 0.28 |
| US-160 On-Ramp | Merge | 4,702 | C | 22.7 | 0.57 | B | 17.2 | 0.42 |
| Between US-160 On-Ramp and MO-13 Off-Ramp | Basic | 4,702 | C | 19.7 | 0.57 | B | 14.4 | 0.42 |
| MO-13 Off-Ramp | Diverge | 4,702 | C | 21.5 | 0.57 | B | 15.2 | 0.42 |
| Between MO-13 Off-Ramp and On-Ramp | Basic | 4,694 | B | 16.9 | 0.49 | B | 12.5 | 0.37 |
| MO-13 On-Ramp | Merge | 4,687 | C | 23.0 | 0.73 | C | 21.2 | 0.69 |
| Between MO-13 On-Ramp and S Campbell Off-Ramp | Basic | 7,031 | B | 16.8 | 0.49 | B | 15.7 | 0.46 |
| S Campbell Off-Ramp | Diverge | 4,687 | C | 21.0 | 0.73 | B | 19.1 | 0.69 |
| Between S Campbell Off-Ramp and On-Ramp | Basic | 4,681 | C | 19.0 | 0.55 | B | 17.9 | 0.52 |
| Between S Campbell On-Ramp and S National Off-Ramp | Weave | 5,232 | C | 27.8 | 0.79 | C | 22.8 | 0.63 |
| Between S National Off-Ramp and S National On-Ramp | Basic | 4,627 | C | 20.2 | 0.59 | F | 51.0 | 0.61 |
| S National On-Ramp | Merge | 4,629 | C | 23.5 | 0.74 | E | 71.3 | 0.88 |
| Between S National On-Ramp and Republic Off-Ramp | Basic | 6,944 | B | 16.9 | 0.49 | F | 119.1 | 0.59 |
| Republic Off-Ramp | Diverge | 4,629 | C | 21.3 | 0.74 | E | 84.4 | 0.88 |
| Between Republic Off-Ramp and BUS-65 On-Ramp | Basic | 4,593 | C | 19.6 | 0.57 | F | 101.2 | 0.75 |
| BUS-65 On-Ramp | Merge | 4,597 | C | 21.8 | 0.59 | E | 68.8 | 0.96 |
| Republic On-Ramp | Merge | 4,598 | B | 19.9 | 0.64 | D | 32.9 | 1.05 |
| Between Republic On-Ramp and US-65 Off-Ramp | Basic | 6,897 | B | 14.6 | 0.43 | C | 23.2 | 0.70 |
| US-65 Off-Ramp | Diverge | 4,598 | B | 17.2 | 0.64 | D | 31.6 | 1.05 |
| Between US-65 Off-Ramp and US-65 SB On-Ramp | Basic | 4,758 | A | 4.1 | 0.12 | B | 11.2 | 0.35 |
| US-65 SB On-Ramp | Merge | 4,490 | A | 8.3 | 0.17 | B | 16.7 | 0.42 |
| US-65 NB On-Ramp | Merge | 4,460 | A | 5.6 | 0.20 | B | 13.8 | 0.44 |
| After US-65 NB On-Ramp | Basic | 4,460 | A | 6.7 | 0.20 | B | 14.2 | 0.44 |

## 2017 No-Build Mainline Analysis Tables cont.

US 60 West Corridor - Westbound

| Description | Type | Adjusted Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | $\begin{aligned} & \begin{array}{c} \text { Density } \\ \text { (veh/mi/ln) } \end{array} \end{aligned}$ | V/C | LOS | Density (veh/mi/ln) | V/C |
| US-60 Before US-65 NB Off-Ramp | Basic | 4,607 | B | 15.5 | 0.45 | A | 9.1 | 0.27 |
| US-65 NB Off-Ramp | Diverge | 4,607 | B | 13.4 | 0.45 | A | 5.7 | 0.27 |
| US-65 SB Off-Ramp | Diverge | 4,627 | B | 18.4 | 0.18 | B | 10.8 | 0.09 |
| Between US-65 SB Off-Ramp and US-65 SB On-Ramp | Basic | 4,658 | A | 5.3 | 0.15 | A | 2.4 | 0.07 |
| US-65 SB On-Ramp | Merge | 7,017 | B | 11.3 | 0.33 | B | 11.6 | 0.53 |
| US-65 NB On-Ramp | Merge | 7,043 | C | 21.2 | 0.55 | B | 18.5 | 0.68 |
| Between US-65 NB On-Ramp and S Glenstone Off-Ramp | Basic | 7,043 | C | 19.1 | 0.55 | B | 16.9 | 0.68 |
| S Glenstone Off-Ramp | Diverge | 7,043 | B | 19.1 | 0.55 | B | 16.9 | 0.68 |
| Between S Glenstone Off-Ramp and On-Ramp | Basic | 4,680 | C | 20.7 | 0.60 | C | 18.6 | 0.75 |
| S Glenstone On-Ramp | Merge | 4,686 | C | 21.9 | 0.69 | C | 22.0 | 0.91 |
| Between S Glenstone On-Ramp and S National Off-Ramp | Basic | 7,028 | B | 15.9 | 0.46 | B | 16.1 | 0.61 |
| S National Off-Ramp | Diverge | 4,686 | B | 19.4 | 0.69 | B | 19.8 | 0.91 |
| Between S National Off-Ramp and On-Ramp | Basic | 4,670 | B | 17.4 | 0.51 | C | 18.2 | 0.69 |
| Between National On-Ramp and S Campbell Off-Ramp | Weave | 5,555 | B | 18.8 | 0.55 | C | 21.7 | 0.70 |
| Between S Campbell Off-Ramp and On-Ramp | Basic | 4,656 | B | 13.2 | 0.38 | B | 16.3 | 0.58 |
| S Campbell On-Ramp | Merge | 4,675 | B | 15.4 | 0.52 | B | 18.6 | 0.72 |
| Between S Campbell On-Ramp and MO-13 Off-Ramp | Basic | 7,013 | B | 12.0 | 0.35 | B | 14.0 | 0.48 |
| MO-13 Off-Ramp | Diverge | 4,675 | B | 12.4 | 0.52 | B | 16.0 | 0.72 |
| Between MO-13 Off-Ramp and On-Ramp | Basic | 4,571 | A | 6.0 | 0.17 | B | 14.2 | 0.49 |
| MO-13 On-Ramp | Merge | 4,631 | B | 11.6 | 0.29 | C | 21.6 | 0.63 |
| Between MO-13 On-Ramp and US-160 Off-Ramp | Basic | 4,631 | A | 9.8 | 0.29 | C | 19.0 | 0.63 |
| US-160 Off-Ramp | Diverge | 4,631 | B | 10.1 | 0.29 | C | 21.2 | 0.63 |
| Between US-160 Off-Ramp and US-160 On-Ramp | Basic | 4,506 | A | 4.8 | 0.14 | B | 11.1 | 0.37 |
| US-160 On-Ramp | Merge | 4,599 | A | 9.7 | 0.22 | B | 15.9 | 0.43 |
| Between US-160 On-Ramp and MO-413 Off-Ramp | Basic | 4,599 | A | 7.5 | 0.22 | B | 13.3 | 0.43 |
| MO-413 Off-Ramp | Diverge | 4,599 | A | 3.0 | 0.22 | A | 9.9 | 0.43 |
| Between MO-413 Off-Ramp and On-Ramp | Basic | 4,513 | A | 5.0 | 0.15 | A | 6.8 | 0.22 |
| MO-413 On-Ramp | Merge | 4,544 | A | 6.5 | 0.16 | A | 8.8 | 0.24 |
| Between MO-413 On-Ramp and Hwy MM Off-Ramp | Basic | 4,544 | A | 5.6 | 0.16 | A | 7.6 | 0.24 |
| Hwy MM Off-Ramp | Diverge | 4,544 | A | 4.5 | 0.16 | A | 6.9 | 0.24 |
| Between Hwy MM Off-Ramp and On-Ramp | Basic | 4,521 | A | 4.0 | 0.12 | A | 5.0 | 0.16 |
| Hwy MM On-Ramp | Merge | 4,490 | A | 5.0 | 0.12 | A | 6.3 | 0.17 |
| Between Hwy MM On-Ramp and I-44 EB Off-Ramp | Basic | 4,490 | A | 4.1 | 0.12 | A | 5.2 | 0.17 |
| I-44 EB Off-Ramp | Diverge | 4,490 | A | 4.1 | 0.12 | A | 5.2 | 0.17 |
| US 60 After l-44 EB Off-Ramp | Basic | 2,273 | A | 5.6 | 0.16 | A | 9.0 | 0.29 |

## 2017 No-Build Mainline Analysis Tables cont.

US 60 East Corridor - Eastbound

| Description | Type | Adjusted Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Density (veh/mil/n) | V/C | LOS | Density (veh/mi/ln) | V/C |
| US-60 Before Rte NN Off-Ramp | Basic | 4,364 | A | 5.5 | 0.17 | B | 11.9 | 0.36 |
| Rte NN Off-Ramp | Diverge | 4,364 | A | 4.9 | 0.17 | B | 12.6 | 0.36 |
| Between Rte NN Off-Ramp and On-Ramp | Basic | 4,355 | A | 4.9 | 0.15 | A | 9.5 | 0.29 |
| Rte NN On-Ramp | Merge | 4,365 | A | 5.7 | 0.17 | B | 10.9 | 0.31 |
| Between Rte NN On-Ramp and Farm Road 247 OffRamp | Basic | 4,360 | A | 5.2 | 0.16 | A | 9.9 | 0.30 |
| Farm Road 247 Off-Ramp | Diverge | 4,360 | B | 10.3 | 0.16 | B | 16.0 | 0.30 |
| US-60 After Farm Road 247 Off-Ramp | Basic | 4,354 | A | 4.8 | 0.15 | A | 8.7 | 0.26 |

US 60 East Corridor - Westbound

| Description | Type | Adjusted Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | $\begin{gathered} \text { Density } \\ \text { (veh/mi/ln) } \end{gathered}$ | V/C | LOS | Density (veh/mi/ln) | V/C |
| US-60 Before Farm Road 247 On-Ramp | Basic | 4,364 | A | 10.8 | 0.33 | A | 6.8 | 0.21 |
| Farm Road 247 On-Ramp | Merge | 4,367 | B | 12.5 | 0.35 | A | 7.8 | 0.21 |
| $\begin{array}{l}\text { Between Farm Road } 247 \text { On-Ramp and Rte NN Off- } \\ \text { Ramp }\end{array}$ | Basic | 4,367 | B | 11.3 | 0.35 | A | 7.0 | 0.21 |
| Rte NN Off-Ramp | Diverge | 4,368 | B | 12.4 | 0.35 | A | 7.3 | 0.22 |
| Between Rte NN Off-Ramp and On-Ramp | Basic | 4,363 | A | 10.8 | 0.33 | A | 6.3 | 0.19 |
| Rte NN On-Ramp | Merge | 4,380 | B | 13.4 | 0.42 | A | 6.7 | 0.23 |
| US-60 After Rte NN On-Ramp | Basic | 4,380 | B | 13.7 | 0.42 | A | 7.5 | 0.23 |

## 2017 No-Build Mainline Analysis Tables cont.

I-44 Corridor - Eastbound

| Description | Type | Adjusted Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Density (veh/mi/ln) | V/C | LOS | Density (veh/mi/ln) | V/C |
| 1-44 Before US-360 SB Off-Ramp | Basic | 3,780 | B | 12.6 | 0.37 | B | 15.0 | 0.44 |
| US-360 SB Off-Ramp | Diverge | 3,780 | A | 8.7 | 0.37 | B | 11.7 | 0.44 |
| Between US-360 SB Off-Ramp and NB On-Ramp | Basic | 3,298 | A | 7.8 | 0.23 | A | 10.3 | 0.30 |
| US-360 NB On-Ramp | Merge | 3,476 | A | 9.3 | 0.26 | B | 11.3 | 0.32 |
| Between US-360 NB On-Ramp and Hwy MM Off-Ramp | Basic | 3,476 | A | 9.1 | 0.26 | B | 11.0 | 0.32 |
| Hwy MM Off-Ramp | Diverge | 3,476 | B | 12.6 | 0.26 | B | 14.9 | 0.32 |
| Between Hwy MM Off-Ramp and Hwy MM On-Ramp | Basic | 3,450 | A | 8.9 | 0.26 | A | 10.7 | 0.31 |
| Hwy MM On-Ramp | Merge | 3,764 | B | 15.5 | 0.36 | B | 15.1 | 0.35 |
| Between Hwy MM On-Ramp and MO-266 Off-Ramp | Basic | 3,764 | B | 12.3 | 0.36 | B | 12.1 | 0.35 |
| MO-266 Off-Ramp | Diverge | 3,764 | B | 14.0 | 0.36 | B | 13.8 | 0.35 |
| Between MO-266 Off-Ramp and On-Ramp | Basic | 3,511 | A | 9.4 | 0.27 | A | 10.4 | 0.30 |
| MO-266 On-Ramp | Merge | 3,751 | B | 14.7 | 0.35 | B | 14.9 | 0.36 |
| Between MO-266 On-Ramp and West Bypass Off-Ramp | Basic | 3,381 | B | 13.5 | 0.39 | B | 13.9 | 0.40 |
| West Bypass Off-Ramp | Diverge | 3,381 | B | 14.9 | 0.39 | B | 15.4 | 0.40 |
| Between West Bypass Off-Ramp and On-Ramp | Basic | 3,583 | A | 10.1 | 0.29 | A | 10.9 | 0.32 |
| West Bypass On-Ramp | Merge | 3,991 | C | 20.4 | 0.50 | C | 21.1 | 0.51 |
| Between West Bypass On-Ramp and M0-13 Off-Ramp | Basic | 3,991 | B | 17.1 | 0.50 | B | 17.6 | 0.51 |
| MO-13 Off-Ramp | Diverge | 3,991 | C | 21.2 | 0.50 | C | 21.8 | 0.51 |
| Between MO-13 Off-Ramp and On-Ramp | Basic | 3,903 | B | 14.9 | 0.43 | B | 15.2 | 0.44 |
| MO-13 On-Ramp | Merge | 4,067 | C | 22.9 | 0.57 | C | 24.3 | 0.61 |
| Between MO-13 On-Ramp and Glenstone Off-Ramp | Basic | 4,067 | C | 19.8 | 0.57 | C | 21.0 | 0.61 |
| Glenstone Off-Ramp | Diverge | 4,067 | C | 22.0 | 0.57 | C | 23.3 | 0.61 |
| Between Glenstone Off-Ramp and On-Ramp | Basic | 3,807 | B | 13.0 | 0.38 | B | 17.0 | 0.50 |
| Glenstone On-Ramp | Merge | 3,941 | B | 19.6 | 0.46 | C | 25.5 | 0.61 |
| Between Glenstone On-Ramp and US-65 SB Off-Ramp | Basic | 3,941 | B | 15.8 | 0.46 | C | 21.3 | 0.61 |
| US-65 SB Off-Ramp | Diverge | 3,941 | B | 18.0 | 0.46 | C | 24.3 | 0.61 |
| Between US-65 SB Off-Ramp and SB On-Ramp | Basic | 3,264 | A | 7.6 | 0.22 | B | 13.3 | 0.39 |
| US-65 SB On-Ramp and NB Off-Ramp | Weave | 4,333 | A | 6.5 | 0.21 | B | 11.4 | 0.34 |
| Between US-65 NB Off-Ramp and NB On-Ramp | Basic | 3,346 | A | 8.1 | 0.24 | B | 12.4 | 0.36 |
| US-65 NB On-Ramp | Merge | 3,788 | B | 15.2 | 0.37 | C | 23.9 | 0.60 |
| $\begin{array}{l}\text { Between US-65 NB On-Ramp and Farm Road } 199 \text { Off- } \\ \text { Ramp }\end{array}$ | Basic | 3,788 | B | 12.7 | 0.37 | C | 20.8 | 0.60 |
| Farm Road 199 Off-Ramp | Diverge | 3,788 | B | 13.2 | 0.37 | C | 22.8 | 0.60 |
| Between Farm Road 199 Off-Ramp and On-Ramp | Basic | 3,619 | A | 10.5 | 0.30 | C | 19.3 | 0.56 |
| Farm Road 199 On-Ramp | Merge | 3,643 | B | 12.8 | 0.31 | C | 22.9 | 0.58 |
| Between Farm Road 199 On-Ramp and MO-125 Off- Ramp | Basic | 3,643 | A | 10.7 | 0.31 | C | 20.0 | 0.58 |
| MO-125 Off-Ramp | Diverge | 3,643 | B | 10.8 | 0.31 | C | 21.8 | 0.58 |
| Between MO-125 Off-Ramp and On-Ramp | Basic | 3,463 | A | 9.0 | 0.26 | B | 17.2 | 0.50 |
| MO-125 On-Ramp | Merge | 3,570 | B | 12.0 | 0.29 | C | 21.0 | 0.53 |
| 1-44 After MO-125 On-Ramp | Basic | 3,570 | A | 9.9 | 0.29 | C | 18.3 | 0.53 |

## 2017 No-Build Mainline Analysis Tables cont.

I-44 Corridor - Westbound

| Description | Type | Adjusted Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | $\begin{gathered} \text { Density } \\ \text { (veh/mi/ln) } \end{gathered}$ | V/C | LOS | Density (veh/mi/ln) | V/C |
| I-44 Before MO-125 Off-Ramp | Basic | 3,780 | A | 7.4 | 0.22 | A | 7.9 | 0.23 |
| MO-125 Off-Ramp | Diverge | 3,780 | A | -0.3 | 0.22 | A | 0.3 | 0.23 |
| Between MO-125 Off-Ramp and On-Ramp | Basic | 3,658 | A | 6.4 | 0.19 | A | 6.8 | 0.20 |
| MO-125 On-Ramp | Merge | 3,982 | B | 11.8 | 0.29 | B | 10.7 | 0.26 |
| Between MO-125 On-Ramp and Farm Road 199 OffRamp | Basic | 3,982 | A | 10.0 | 0.29 | A | 9.1 | 0.26 |
| Farm Road 199 Off-Ramp | Diverge | 3,982 | B | 11.1 | 0.29 | A | 9.9 | 0.26 |
| Between Farm Road 199 Off-Ramp and On-Ramp | Basic | 3,927 | A | 9.1 | 0.27 | A | 8.7 | 0.25 |
| Farm Road 199 On-Ramp | Merge | 4,020 | B | 13.0 | 0.31 | B | 13.2 | 0.32 |
| Between Farm Road 199 On-Ramp and US-65 NB OffRamp | Basic | 4,020 | A | 10.7 | 0.31 | A | 10.9 | 0.32 |
| US-65 NB Off-Ramp | Diverge | 4,020 | A | 9.9 | 0.31 | B | 10.0 | 0.32 |
| US-65 SB Off-Ramp | Diverge | 3,913 | B | 12.6 | 0.26 | B | 12.8 | 0.27 |
| Between US-65 SB Off-Ramp and US-65 On-Ramp | Basic | 3,143 | A | 4.1 | 0.12 | A | 5.2 | 0.15 |
| US-65 On-Ramp | Merge | 4,179 | B | 12.8 | 0.44 | B | 18.1 | 0.58 |
| Between US-65 On-Ramp and Glenstone Off-Ramp | Basic | 4,179 | B | 15.0 | 0.44 | C | 20.2 | 0.58 |
| Glenstone Off-Ramp | Diverge | 4,179 | C | 20.8 | 0.44 | C | 26.8 | 0.58 |
| Between Glenstone Off-Ramp and On-Ramp | Basic | 4,059 | B | 11.5 | 0.34 | B | 16.7 | 0.49 |
| Glenstone On-Ramp | Merge | 4,161 | B | 17.5 | 0.42 | C | 26.4 | 0.66 |
| Between Glenstone On-Ramp and MO-13 Off-Ramp | Basic | 4,161 | B | 14.3 | 0.42 | C | 23.1 | 0.66 |
| MO-13 Off-Ramp | Diverge | 4,161 | B | 15.3 | 0.42 | C | 25.1 | 0.66 |
| Between MO-13 Off-Ramp and On-Ramp | Basic | 3,976 | A | 9.9 | 0.29 | B | 16.7 | 0.49 |
| MO-13 On-Ramp | Merge | 4,067 | B | 15.2 | 0.34 | C | 23.2 | 0.56 |
| Between MO-13 On-Ramp and West Bypass Off-Ramp | Basic | 4,067 | B | 11.7 | 0.34 | C | 19.2 | 0.56 |
| West Bypass Off-Ramp | Diverge | 4,067 | B | 13.4 | 0.34 | C | 22.4 | 0.56 |
| Between West Bypass Off-Ramp and On-Ramp | Basic | 3,729 | A | 7.0 | 0.20 | B | 12.2 | 0.36 |
| West Bypass On-Ramp | Merge | 3,499 | B | 10.9 | 0.26 | B | 17.2 | 0.44 |
| Between West Bypass On-Ramp and Kearney On-Ramp | Basic | 3,499 | A | 8.9 | 0.26 | B | 15.0 | 0.44 |
| Kearney On-Ramp | Merge | 3,913 | B | 12.4 | 0.26 | B | 18.5 | 0.42 |
| Between Kearney On-Ramp and MO-266 Off-Ramp | Basic | 3,913 | A | 8.9 | 0.26 | B | 14.4 | 0.42 |
| MO-266 Off-Ramp | Diverge | 3,913 | B | 10.2 | 0.26 | B | 16.8 | 0.42 |
| Between MO-266 Off-Ramp and On-Ramp | Basic | 3,772 | A | 7.4 | 0.22 | B | 11.4 | 0.33 |
| MO-266 On-Ramp | Merge | 3,884 | A | 5.6 | 0.25 | B | 11.0 | 0.40 |
| Between MO-266 On-Ramp and Hwy MM Off-Ramp | Basic | 3,884 | A | 8.6 | 0.25 | B | 13.6 | 0.40 |
| Hwy MM Off-Ramp | Diverge | 3,884 | B | 11.0 | 0.25 | B | 17.0 | 0.40 |
| Between Hwy MM Off-Ramp and On-Ramp | Basic | 3,772 | A | 7.4 | 0.22 | A | 10.8 | 0.31 |
| Hwy MM On-Ramp | Merge | 3,794 | A | 9.4 | 0.22 | B | 13.2 | 0.32 |
| Between Hwy MM On-Ramp and US-360 SB Off-Ramp | Basic | 3,794 | A | 7.6 | 0.22 | B | 11.0 | 0.32 |
| US-360 SB Off-Ramp | Diverge | 3,794 | A | 6.1 | 0.22 | B | 10.2 | 0.32 |
| Between US-360 SB Off-Ramp and US-360 NB On-Ramp | Basic | 3,729 | A | 7.0 | 0.20 | A | 9.9 | 0.29 |
| US-360 NB On-Ramp | Merge | 4,042 | B | 11.0 | 0.32 | B | 14.9 | 0.43 |
| 1-44 After US-360 NB On-Ramp | Merge | 4,042 | B | 11.1 | 0.32 | B | 14.8 | 0.43 |

## 2017 No-Build Intersection Analysis Tables

US 60 Corridors

| $\begin{gathered} \text { Synchro } \\ \text { ID } \end{gathered}$ | Intersection | AM |  | PM |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS | Delay (s/veh) | LOS | Delay (s/veh) |
| US 60 West Corridor |  |  |  |  |  |
| 118* | US 60 WB Ramps \& Hwy MM | C | 21.5 | D | 25.3 |
| 115* | US 60 EB Ramps \& Hwy MM | F | 52 | E | 43 |
| 6 | US 60 WB Ramps \& Sunshine St | B | 10.6 | C | 21.1 |
| 12 | US 60 EB Ramps \& Sunshine St | A | 5.3 | A | 6.2 |
| 17 | US 60 WB Ramps \& West Bypass | B | 12.3 | C | 27.6 |
| 20 | US 60 EB Ramps \& West Bypass | B | 15.2 | B | 10.8 |
| 88 | US 60 WB Ramps \& Kansas Expwy | C | 34.5 | C | 24.5 |
| 93 | US 60 EB Ramps \& Kansas Expwy | C | 32 | F | 109.2 |
| 95 | US 60 EB Ramps Right \& Kansas Expwy | A | 4.1 | A | 5.4 |
| 31 | Campbell Ave \& Republic Rd | E | 61.8 | E | 58.7 |
| 28 | Campbell Ave \& US 60 WB Ramps | B | 12.1 | C | 23.2 |
| 24 | Campbell Ave \& US 60 EB Ramps | B | 15.5 | B | 11.3 |
| 36 | Campbell Ave \& El Camino Alto | C | 21.3 | C | 34 |
| 56* | US 60 \& National Ave WB On-Ramp | A | 0 | A | 0 |
| 64 | US 60 \& National Ave WB Off-Ramp Left | A | 3 | B | 12.1 |
| 66 | US 60 \& National Ave North DDI Intersection | C | 27.2 | C | 27.2 |
| 68 | US 60 \& National Ave WB Off-Ramp Right | B | 14.9 | A | 7.6 |
| 62* | US 60 \& National Ave EB On-Ramp | C | 15.6 | F | 197.1 |
| 77 | US 60 \& National Ave EB Off-Ramp Left | B | 10.1 | A | 6.2 |
| 79 | US 60 \& National Ave South DDI Intersection | C | 29.2 | C | 33.3 |
| 81 | US 60 \& National Ave EB Off-Ramp Right | B | 16.3 | B | 10.2 |
| 46 | US 60 WB Ramps \& Glenstone Ave | D | 41.5 | E | 64.7 |
| 43 | US 60 EB Ramps \& Republic Rd/Glenstone | C | 33.4 | C | 27.4 |
| US 60 East Corridor |  |  |  |  |  |
| 5* | US 60 \& Highland Springs Blvd (N) | E | 38.5 | C | 15.9 |
| $6 *$ | US 60 \& Highland Springs Blvd (S) | D | 25.8 | F | 573.3 |
| 8* | US 60 \& Farm Rd 189 (N) | F | 231.5 | D | 25.6 |
| 9* | US 60 \& Farm Rd 189 (S) | C | 20.2 | F | 120.2 |
| 12* | US 60 \& Farm Rd 193 (N) | F | 102.1 | D | 30.6 |
| $13^{*}$ | US 60 \& Farm Rd 193 (S) | C | 17.2 | F | 77.3 |
| $60^{*}$ | US 60 WB Ramps \& Route NN/J | D | 34.1 | B | 13.4 |
| $63^{*}$ | US 60 EB Ramps \& Route NN/J | B | 12.6 | B | 12 |
| 16* | US 60 \& Farm Rd 205 (N) | D | 33.9 | C | 21.3 |
| 17* | US 60 \& Farm Rd 205 (S) | C | 17.7 | E | 47 |
| $20^{*}$ | US 60 \& Farm Rd 213 (N) | E | 38 | C | 18.1 |
| 21* | US 60 \& Farm Rd 213 (S) | B | 14.6 | D | 30.9 |
| $24^{*}$ | US 60 \& Farm Rd 219 (N) | F | 52.1 | C | 18.2 |
| 25* | US 60 \& Farm Rd 219 (S) | C | 15.2 | D | 30.9 |
| 29* | US 60 \& Farm Rd 223 (N) | F | 78.4 | C | 20.8 |
| 30* | US 60 \& Farm Rd 223 (S) | B | 14.8 | C | 18.9 |
| 33* | US 60 \& Farm Rd 229 (N) | E | 46.8 | C | 19.2 |
| $34^{*}$ | US 60 \& Farm Rd 229 (S) | B | 11.5 | C | 15.9 |
| 36 | US 60 \& Hwy 125 (N) | F | 1750.5 | F | 502 |
| 37 | US 60 \& Hwy 125 (S) | F | 113.1 | F | 207.9 |
| 40* | US 60 \& Farm Rd 241 (N) | C | 19 | B | 12.5 |
| 41* | US 60 \& Farm Rd 241 (S) | C | 17.2 | D | 32.7 |
| 53* | US 60 EB Off-Ramp \& Farm Rd 247 | A | 7.8 | A | 8.6 |

*At unsignalized intersections, LOS and delay for the worst movement is shown.

## 2017 No-Build Intersection Analysis Tables cont.

## I-44 Corridor

| Synchro <br> ID | Intersection | AM |  | PM |  |
| :---: | :--- | :---: | :---: | :---: | :---: |
|  |  | LOS | Delay (s/veh) | LOS | Delay (s/veh) |
| $117^{*}$ | I-44 WB Ramps \& Hwy MM | C | 21.4 | F | 75.4 |
| $113^{*}$ | I-44 EB Ramps \& Hwy MM | C | 17 | C | 22.4 |
| 101 | I-44 WB Ramps \& Chestnut Expwy | D | 36.8 | C | 30.1 |
| 96 | I-44 EB Ramps \& Chestnut Expwy | B | 18.6 | C | 22.1 |
| 85 | I-44 WB Ramps \& West Bypass | C | 27.1 | B | 14.8 |
| 81 | I-44 EB Ramps \& West Bypass | B | 10.4 | A | 9.5 |
| 54 | I-44 \& Route 13 EB Off-Ramp Right | A | 3.5 | A | 4.5 |
| 62 | I-44 \& Route 13 South DDI Intersection | B | 18.9 | D | 45.8 |
| 65 | I-44 \& Route 13 WB Off-Ramp Right | A | 4.5 | A | 9.2 |
| 66 | I-44 \& Route 13 North DDI Intersection | B | 19.7 | C | 33.1 |
| $67^{*}$ | I-44 \& Route 13 WB Off-Ramp Left | C | 22.1 | C | 15.3 |
| $59^{*}$ | I-44 \& Route 13 WB On-Ramp | A | 9.4 | B | 10.1 |
| 40 | I-44 WB Ramps \& Glenstone Ave | C | 22.5 | D | 38.9 |
| 36 | I-44 EB Ramps \& Glenstone Ave | C | 33 | C | 25.8 |
| $26^{*}$ | I-44 WB Ramps \& N Mulroy Rd | B | 14 | C | 22.3 |
| $17^{*}$ | I-44 EB Ramps \& N Mulroy Rd | B | 12 | B | 11 |
| $8^{*}$ | I-44 WB Ramps \& Hwy 125 | E | 38 | C | 22.4 |
| 7 | I-44 EB Ramps \& Hwy 125 | B | 10.7 | B | 11.3 |

*At unsignalized intersections, LOS and delay for the worst movement is shown.

## Appendix C

## 2040 No-Build Operational Analysis

## 2040 No-Build Mainline Analysis Tables

US 60 West Corridor - Eastbound

| Description | Type | Adjusted <br> Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Density (veh/mi/ln) | D/C | LOS | Density (veh/mi/ln) | D/C |
| US-60 Before I-44 EB On-Ramp | Basic | 2,176 | A | 1.6 | 0.05 | A | 3.0 | 0.09 |
| I-44 EB On-Ramp | Merge | 2,311 | A | 4.3 | 0.41 | A | 6.2 | 0.48 |
| Between l-44 EB On-Ramp and Hwy MM Off-Ramp | Basic | 4,622 | A | 7.0 | 0.21 | A | 8.2 | 0.24 |
| Hwy MM Off-Ramp | Diverge | 4,622 | A | 6.6 | 0.21 | A | 8.0 | 0.24 |
| Between Hwy MM Off-Ramp and On-Ramp | Basic | 4,633 | A | 6.9 | 0.20 | A | 7.7 | 0.23 |
| Hwy MM On-Ramp | Merge | 4,654 | B | 13.1 | 0.33 | B | 12.8 | 0.32 |
| Between Hwy MM On-Ramp and MO-413 Off-Ramp | Basic | 4,654 | B | 11.3 | 0.33 | A | 11.0 | 0.32 |
| MO-413 Off-Ramp | Diverge | 4,654 | B | 11.3 | 0.33 | B | 10.9 | 0.32 |
| Between MO-413 Off-Ramp and On-Ramp | Basic | 4,648 | A | 10.7 | 0.31 | A | 10.3 | 0.30 |
| M0-413 On-Ramp | Merge | 4,681 | C | 21.2 | 0.54 | B | 17.9 | 0.45 |
| Between MO-413 On-Ramp and US-160 Off-Ramp | Basic | 4,681 | C | 18.5 | 0.54 | B | 15.3 | 0.45 |
| US-160 Off-Ramp | Diverge | 4,681 | C | 20.8 | 0.54 | B | 16.9 | 0.45 |
| Between US-160 Off-Ramp and On-Ramp | Basic | 4,673 | B | 16.9 | 0.49 | B | 13.1 | 0.38 |
| US-160 On-Ramp | Merge | 4,702 | C | 27.9 | 0.71 | C | 22.3 | 0.56 |
| Between US-160 On-Ramp and MO-13 Off-Ramp | Basic | 4,702 | C | 25.5 | 0.71 | C | 19.2 | 0.56 |
| MO-13 Off-Ramp | Diverge | 4,702 | C | 27.2 | 0.71 | C | 20.9 | 0.56 |
| Between MO-13 Off-Ramp and On-Ramp | Basic | 4,694 | C | 19.4 | 0.56 | B | 18.0 | 0.46 |
| MO-13 On-Ramp | Merge | 4,687 | C | 27.5 | 0.86 | D | 32.8 | 0.84 |
| Between MO-13 On-Ramp and S Campbell Off-Ramp | Basic | 7,031 | C | 19.7 | 0.57 | F | 56.0 | 0.56 |
| S Campbell Off-Ramp | Diverge | 4,687 | C | 26.2 | 0.86 | E | 53.2 | 0.84 |
| Between S Campbell Off-Ramp and On-Ramp | Basic | 4,681 | C | 20.9 | 0.60 | E | 40.5 | 0.61 |
| Between S Campbell On-Ramp and S National Off-Ramp | Weave | 5,232 | D | 30.2 | 0.83 | F | 97.9 | 0.72 |
| Between S National Off-Ramp and S National On-Ramp | Basic | 4,627 | C | 21.4 | 0.62 | F | 119.1 | 0.67 |
| S National On-Ramp | Merge | 4,629 | C | 26.5 | 0.83 | E | 87.4 | 1.03 |
| Between S National On-Ramp and Republic Off-Ramp | Basic | 6,944 | C | 18.9 | 0.55 | F | 124.4 | 0.68 |
| Republic Off-Ramp | Diverge | 4,629 | C | 24.8 | 0.83 | E | 89.5 | 1.03 |
| Between Republic Off-Ramp and BUS-65 On-Ramp | Basic | 4,593 | C | 22.6 | 0.65 | F | 107.6 | 0.86 |
| BUS-65 On-Ramp | Merge | 4,597 | C | 25.0 | 0.67 | E | 70.4 | 1.12 |
| Republic On-Ramp | Merge | 4,598 | C | 23.4 | 0.73 | D | 30.8 | 1.22 |
| Between Republic On-Ramp and US-65 Off-Ramp | Basic | 6,897 | B | 16.7 | 0.49 | C | 21.6 | 0.81 |
| US-65 Off-Ramp | Diverge | 4,598 | C | 21.0 | 0.73 | D | 29.2 | 1.22 |
| Between US-65 Off-Ramp and US-65 SB On-Ramp | Basic | 4,758 | A | 4.2 | 0.12 | B | 11.4 | 0.43 |
| US-65 SB On-Ramp | Merge | 4,490 | A | 9.0 | 0.19 | B | 17.6 | 0.52 |
| US-65 NB On-Ramp | Merge | 4,460 | A | 7.7 | 0.26 | B | 15.6 | 0.57 |
| After US-65 NB On-Ramp | Basic | 4,460 | A | 8.8 | 0.26 | B | 15.9 | 0.57 |

## 2040 No-Build Mainline Analysis Tables cont.

US 60 West Corridor - Westbound

| Description | Type | Adjusted Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Density (veh/mi/ln) | D/C | LOS | Density (veh/mi/ln) | D/C |
| US-60 Before US-65 NB Off-Ramp | Basic | 4,607 | C | 18.7 | 0.55 | A | 11.0 | 0.32 |
| US-65 NB Off-Ramp | Diverge | 4,607 | B | 17.2 | 0.55 | A | 7.9 | 0.32 |
| US-65 SB Off-Ramp | Diverge | 4,627 | C | 22.3 | 0.24 | B | 13.0 | 0.12 |
| Between US-65 SB Off-Ramp and US-65 SB On-Ramp | Basic | 4,658 | A | 7.0 | 0.20 | A | 3.2 | 0.09 |
| US-65 SB On-Ramp | Merge | 7,017 | B | 14.2 | 0.41 | B | 12.1 | 0.63 |
| US-65 NB On-Ramp | Merge | 7,043 | D | 28.2 | 0.71 | C | 22.3 | 0.85 |
| Between US-65 NB On-Ramp and S Glenstone Off-Ramp | Basic | 7,043 | C | 25.1 | 0.71 | C | 20.0 | 0.85 |
| S Glenstone Off-Ramp | Diverge | 7,043 | C | 25.1 | 0.71 | C | 20.0 | 0.85 |
| Between S Glenstone Off-Ramp and On-Ramp | Basic | 4,680 | D | 27.7 | 0.76 | C | 22.0 | 0.93 |
| S Glenstone On-Ramp | Merge | 4,686 | D | 28.7 | 0.88 | C | 26.4 | 1.12 |
| Between S Glenstone On-Ramp and S National Off-Ramp | Basic | 7,028 | C | 20.2 | 0.59 | C | 18.9 | 0.75 |
| S National Off-Ramp | Diverge | 4,686 | C | 26.9 | 0.88 | C | 24.8 | 1.12 |
| Between S National Off-Ramp and On-Ramp | Basic | 4,670 | C | 22.6 | 0.65 | C | 20.6 | 0.81 |
| Between National On-Ramp and S Campbell Off-Ramp | Weave | 5,555 | C | 24.5 | 0.67 | C | 25.9 | 0.82 |
| Between S Campbell Off-Ramp and On-Ramp | Basic | 4,656 | B | 17.0 | 0.50 | C | 19.1 | 0.70 |
| S Campbell On-Ramp | Merge | 4,675 | C | 20.3 | 0.66 | C | 22.3 | 0.86 |
| Between S Campbell On-Ramp and MO-13 Off-Ramp | Basic | 7,013 | B | 15.0 | 0.44 | B | 16.3 | 0.57 |
| MO-13 Off-Ramp | Diverge | 4,675 | B | 17.8 | 0.66 | C | 20.1 | 0.86 |
| Between MO-13 Off-Ramp and On-Ramp | Basic | 4,571 | A | 9.5 | 0.28 | B | 17.1 | 0.60 |
| MO-13 On-Ramp | Merge | 4,631 | B | 16.7 | 0.42 | C | 26.1 | 0.78 |
| Between MO-13 On-Ramp and US-160 Off-Ramp | Basic | 4,631 | B | 14.5 | 0.42 | C | 23.9 | 0.78 |
| US-160 Off-Ramp | Diverge | 4,631 | B | 15.8 | 0.42 | C | 26.3 | 0.78 |
| Between US-160 Off-Ramp and US-160 On-Ramp | Basic | 4,506 | A | 8.4 | 0.25 | B | 13.9 | 0.47 |
| US-160 On-Ramp | Merge | 4,599 | B | 14.3 | 0.34 | B | 19.3 | 0.54 |
| Between US-160 On-Ramp and MO-413 Off-Ramp | Basic | 4,599 | B | 11.8 | 0.34 | B | 16.3 | 0.54 |
| MO-413 Off-Ramp | Diverge | 4,599 | A | 8.1 | 0.34 | B | 13.6 | 0.54 |
| Between MO-413 Off-Ramp and On-Ramp | Basic | 4,513 | A | 8.9 | 0.26 | A | 8.8 | 0.29 |
| MO-413 On-Ramp | Merge | 4,544 | B | 10.9 | 0.28 | B | 11.1 | 0.32 |
| Between MO-413 On-Ramp and Hwy MM Off-Ramp | Basic | 4,544 | A | 9.6 | 0.28 | A | 9.8 | 0.32 |
| Hwy MM Off-Ramp | Diverge | 4,544 | A | 9.3 | 0.28 | A | 9.5 | 0.32 |
| Between Hwy MM Off-Ramp and On-Ramp | Basic | 4,521 | A | 7.5 | 0.22 | A | 6.5 | 0.21 |
| Hwy MM On-Ramp | Merge | 4,490 | A | 9.0 | 0.23 | A | 7.9 | 0.22 |
| Between Hwy MM On-Ramp and I-44 EB Off-Ramp | Basic | 4,490 | A | 7.7 | 0.23 | A | 6.7 | 0.22 |
| l-44 EB Off-Ramp | Diverge | 4,490 | A | 7.7 | 0.23 | A | 6.7 | 0.22 |
| US 60 After I-44 EB Off-Ramp | Basic | 2,273 | B | 12.2 | 0.36 | B | 11.8 | 0.39 |

## 2040 No-Build Mainline Analysis Tables cont.

US 60 East Corridor - Eastbound

| Description | Type | Adjusted Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Density (veh/mi/ln) | D/C | LOS | Density (veh/mi/ln) | D/C |
| US-60 Before Rte NN Off-Ramp | Basic | 4,364 | A | 6.9 | 0.21 | B | 14.8 | 0.45 |
| Rte NN Off-Ramp | Diverge | 4,364 | A | 6.7 | 0.21 | B | 16.1 | 0.45 |
| Between Rte NN Off-Ramp and On-Ramp | Basic | 4,355 | A | 6.3 | 0.19 | B | 12.0 | 0.37 |
| Rte NN On-Ramp | Merge | 4,365 | A | 7.4 | 0.21 | B | 13.9 | 0.40 |
| Between Rte NN On-Ramp and Farm Road 247 OffRamp | Basic | 4,360 | A | 7.1 | 0.21 | B | 13.4 | 0.41 |
| Farm Road 247 Off-Ramp | Diverge | 4,360 | B | 12.7 | 0.21 | C | 20.3 | 0.41 |
| US-60 After Farm Road 247 Off-Ramp | Basic | 4,354 | A | 6.7 | 0.20 | B | 12.0 | 0.36 |

US 60 East Corridor - Westbound

| Description | Type | Adjusted Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Density (veh/mi/ln) | D/C | LOS | Density (veh/mi/ln) | D/C |
| US-60 Before Farm Road 247 On-Ramp | Basic | 4,364 | B | 13.6 | 0.43 | A | 8.5 | 0.27 |
| Farm Road 247 On-Ramp | Merge | 4,367 | B | 15.7 | 0.45 | A | 9.8 | 0.28 |
| Between Farm Road 247 On-Ramp and Rte NN OffRamp | Basic | 4,367 | B | 14.2 | 0.45 | A | 8.8 | 0.28 |
| Rte NN Off-Ramp | Diverge | 4,368 | B | 15.5 | 0.45 | A | 9.1 | 0.28 |
| Between Rte NN Off-Ramp and On-Ramp | Basic | 4,363 | B | 12.9 | 0.41 | A | 7.3 | 0.23 |
| Rte NN On-Ramp | Merge | 4,380 | B | 16.3 | 0.51 | A | 8.0 | 0.27 |
| US-60 After Rte NN On-Ramp | Basic | 4,380 | B | 16.2 | 0.51 | A | 8.5 | 0.27 |

## 2040 No-Build Mainline Analysis Tables cont.

I-44 Corridor - Eastbound

| Description | Type | Adjusted Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Density (veh/mi/ln) | D/C | LOS | Density (veh/mi/ln) | D/C |
| I-44 Before US-360 SB Off-Ramp | Basic | 3,780 | B | 16.9 | 0.49 | C | 20.4 | 0.59 |
| US-360 SB Off-Ramp | Diverge | 3,780 | B | 13.9 | 0.49 | B | 18.0 | 0.59 |
| Between US-360 SB Off-Ramp and NB On-Ramp | Basic | 3,298 | A | 10.5 | 0.31 | B | 13.8 | 0.40 |
| US-360 NB On-Ramp | Merge | 3,476 | B | 12.6 | 0.35 | B | 15.3 | 0.43 |
| Between US-360 NB On-Ramp and Hwy MM Off-Ramp | Basic | 3,476 | B | 12.1 | 0.35 | B | 14.6 | 0.43 |
| Hwy MM Off-Ramp | Diverge | 3,476 | B | 16.2 | 0.35 | B | 19.3 | 0.43 |
| Between Hwy MM Off-Ramp and Hwy MM On-Ramp | Basic | 3,450 | B | 11.8 | 0.35 | B | 14.3 | 0.42 |
| Hwy MM On-Ramp | Merge | 3,764 | B | 19.6 | 0.46 | B | 19.2 | 0.46 |
| Between Hwy MM On-Ramp and MO-266 Off-Ramp | Basic | 3,764 | B | 15.9 | 0.46 | B | 15.9 | 0.46 |
| MO-266 Off-Ramp | Diverge | 3,764 | B | 18.3 | 0.46 | B | 18.3 | 0.46 |
| Between MO-266 Off-Ramp and On-Ramp | Basic | 3,511 | B | 12.2 | 0.35 | B | 13.6 | 0.40 |
| MO-266 On-Ramp | Merge | 3,751 | B | 19.7 | 0.48 | B | 19.7 | 0.48 |
| Between MO-266 On-Ramp and West Bypass Off-Ramp | Basic | 3,381 | C | 18.2 | 0.53 | C | 18.6 | 0.54 |
| West Bypass Off-Ramp | Diverge | 3,381 | C | 20.6 | 0.53 | C | 21.0 | 0.54 |
| Between West Bypass Off-Ramp and On-Ramp | Basic | 3,583 | B | 12.8 | 0.37 | B | 13.9 | 0.41 |
| West Bypass On-Ramp | Merge | 3,991 | C | 24.6 | 0.61 | C | 25.6 | 0.63 |
| Between West Bypass On-Ramp and M0-13 Off-Ramp | Basic | 3,991 | C | 21.0 | 0.61 | C | 21.9 | 0.63 |
| MO-13 Off-Ramp | Diverge | 3,991 | C | 25.5 | 0.61 | C | 26.5 | 0.63 |
| Between MO-13 Off-Ramp and On-Ramp | Basic | 3,903 | C | 18.1 | 0.53 | C | 18.9 | 0.55 |
| MO-13 On-Ramp | Merge | 4,067 | C | 27.4 | 0.69 | D | 29.1 | 0.73 |
| Between MO-13 On-Ramp and Glenstone Off-Ramp | Basic | 4,067 | C | 24.5 | 0.69 | D | 26.4 | 0.73 |
| Glenstone Off-Ramp | Diverge | 4,067 | C | 26.8 | 0.69 | D | 28.5 | 0.73 |
| Between Glenstone Off-Ramp and On-Ramp | Basic | 3,807 | B | 15.4 | 0.45 | C | 20.3 | 0.59 |
| Glenstone On-Ramp | Merge | 3,941 | C | 22.7 | 0.54 | D | 29.9 | 0.73 |
| Between Glenstone On-Ramp and US-65 SB Off-Ramp | Basic | 3,941 | C | 18.5 | 0.54 | D | 26.3 | 0.73 |
| US-65 SB Off-Ramp | Diverge | 3,941 | C | 21.2 | 0.54 | D | 29.0 | 0.73 |
| Between US-65 SB Off-Ramp and SB On-Ramp | Basic | 3,264 | A | 9.5 | 0.28 | B | 16.5 | 0.48 |
| US-65 SB On-Ramp and NB Off-Ramp | Weave | 4,333 | A | 8.2 | 0.26 | B | 14.5 | 0.42 |
| Between US-65 NB Off-Ramp and NB On-Ramp | Basic | 3,346 | A | 10.1 | 0.29 | B | 15.3 | 0.45 |
| US-65 NB On-Ramp | Merge | 3,788 | B | 18.0 | 0.44 | D | 28.2 | 0.71 |
| Between US-65 NB On-Ramp and Farm Road 199 Off- <br> Ramp | Basic | 3,788 | B | 15.0 | 0.44 | C | 25.4 | 0.71 |
| Farm Road 199 Off-Ramp | Diverge | 3,788 | B | 16.1 | 0.44 | C | 27.2 | 0.71 |
| Between Farm Road 199 Off-Ramp and On-Ramp | Basic | 3,619 | B | 12.6 | 0.37 | C | 23.4 | 0.67 |
| Farm Road 199 On-Ramp | Merge | 3,643 | B | 15.8 | 0.39 | C | 27.5 | 0.70 |
| Between Farm Road 199 On-Ramp and MO-125 Off- <br> Ramp | Basic | 3,643 | B | 13.3 | 0.39 | C | 25.1 | 0.70 |
| MO-125 Off-Ramp | Diverge | 3,643 | B | 13.9 | 0.39 | C | 26.9 | 0.70 |
| Between MO-125 Off-Ramp and On-Ramp | Basic | 3,463 | A | 11.0 | 0.32 | C | 21.4 | 0.62 |
| MO-125 On-Ramp | Merge | 3,570 | B | 16.0 | 0.39 | C | 27.2 | 0.69 |
| I-44 After MO-125 On-Ramp | Basic | 3,570 | B | 13.3 | 0.39 | C | 24.6 | 0.69 |

## 2040 No-Build Mainline Analysis Tables cont.

I-44 Corridor - Westbound

| Description | Type | Adjusted Capacity (vph) | AM |  |  | PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Density (veh/mi/ln) | D/C | LOS | Density (veh/mi/ln) | D/C |
| I-44 Before MO-125 Off-Ramp | Basic | 3,780 | A | 10.7 | 0.31 | B | 11.8 | 0.34 |
| MO-125 Off-Ramp | Diverge | 3,780 | A | 3.6 | 0.31 | A | 4.9 | 0.34 |
| Between MO-125 Off-Ramp and On-Ramp | Basic | 3,658 | A | 8.6 | 0.25 | A | 9.2 | 0.27 |
| M0-125 On-Ramp | Merge | 3,982 | B | 15.1 | 0.38 | B | 13.8 | 0.34 |
| Between MO-125 On-Ramp and Farm Road 199 OffRamp | Basic | 3,982 | B | 12.9 | 0.38 | B | 11.8 | 0.34 |
| Farm Road 199 Off-Ramp | Diverge | 3,982 | B | 14.5 | 0.38 | B | 13.2 | 0.34 |
| Between Farm Road 199 Off-Ramp and On-Ramp | Basic | 3,927 | B | 11.3 | 0.33 | B | 11.0 | 0.32 |
| Farm Road 199 On-Ramp | Merge | 4,020 | B | 16.2 | 0.39 | B | 16.5 | 0.40 |
| Between Farm Road 199 On-Ramp and US-65 NB Off- <br> Ramp | Basic | 4,020 | B | 13.5 | 0.39 | B | 13.8 | 0.40 |
| US-65 NB Off-Ramp | Diverge | 4,020 | B | 13.2 | 0.39 | B | 13.5 | 0.40 |
| US-65 SB Off-Ramp | Diverge | 3,913 | B | 16.0 | 0.33 | B | 16.3 | 0.34 |
| Between US-65 SB Off-Ramp and US-65 On-Ramp | Basic | 3,143 | A | 5.4 | 0.16 | A | 7.0 | 0.20 |
| US-65 On-Ramp | Merge | 4,179 | B | 16.3 | 0.52 | C | 23.6 | 0.72 |
| Between US-65 On-Ramp and Glenstone Off-Ramp | Basic | 4,179 | B | 18.0 | 0.52 | D | 26.0 | 0.72 |
| Glenstone Off-Ramp | Diverge | 4,179 | C | 24.3 | 0.52 | D | 32.6 | 0.72 |
| Between Glenstone Off-Ramp and On-Ramp | Basic | 4,059 | B | 14.3 | 0.42 | C | 20.9 | 0.60 |
| Glenstone On-Ramp | Merge | 4,161 | C | 20.8 | 0.51 | D | 31.3 | 0.79 |
| Between Glenstone On-Ramp and MO-13 Off-Ramp | Basic | 4,161 | B | 17.3 | 0.51 | D | 29.3 | 0.79 |
| MO-13 Off-Ramp | Diverge | 4,161 | B | 18.9 | 0.51 | D | 30.5 | 0.79 |
| Between MO-13 Off-Ramp and On-Ramp | Basic | 3,976 | B | 11.7 | 0.34 | C | 20.9 | 0.60 |
| MO-13 On-Ramp | Merge | 4,067 | B | 17.8 | 0.41 | D | 28.7 | 0.70 |
| Between MO-13 On-Ramp and West Bypass Off-Ramp | Basic | 4,067 | B | 14.0 | 0.41 | C | 25.1 | 0.70 |
| West Bypass Off-Ramp | Diverge | 4,067 | B | 16.2 | 0.41 | D | 28.3 | 0.70 |
| Between West Bypass Off-Ramp and On-Ramp | Basic | 3,729 | A | 9.2 | 0.27 | B | 16.3 | 0.47 |
| West Bypass On-Ramp | Merge | 3,499 | B | 14.0 | 0.35 | C | 22.4 | 0.58 |
| Between West Bypass On-Ramp and Kearney On-Ramp | Basic | 3,499 | B | 12.0 | 0.35 | C | 20.1 | 0.58 |
| Kearney On-Ramp | Merge | 3,913 | B | 16.0 | 0.34 | C | 24.3 | 0.56 |
| Between Kearney On-Ramp and MO-266 Off-Ramp | Basic | 3,913 | B | 11.8 | 0.34 | C | 19.3 | 0.56 |
| MO-266 Off-Ramp | Diverge | 3,913 | B | 13.7 | 0.34 | C | 22.6 | 0.56 |
| Between MO-266 Off-Ramp and On-Ramp | Basic | 3,772 | A | 9.6 | 0.28 | B | 14.8 | 0.43 |
| MO-266 On-Ramp | Merge | 3,884 | A | 9.3 | 0.35 | B | 15.3 | 0.51 |
| Between MO-266 On-Ramp and Hwy MM Off-Ramp | Basic | 3,884 | B | 11.8 | 0.35 | B | 17.4 | 0.51 |
| Hwy MM Off-Ramp | Diverge | 3,884 | B | 14.9 | 0.35 | C | 21.6 | 0.51 |
| Between Hwy MM Off-Ramp and On-Ramp | Basic | 3,772 | A | 10.5 | 0.31 | B | 14.3 | 0.42 |
| Hwy MM On-Ramp | Merge | 3,794 | B | 12.9 | 0.31 | B | 17.1 | 0.43 |
| Between Hwy MM On-Ramp and US-360 SB Off-Ramp | Basic | 3,794 | A | 10.8 | 0.31 | B | 14.6 | 0.43 |
| US-360 SB Off-Ramp | Diverge | 3,794 | A | 9.9 | 0.31 | B | 14.6 | 0.43 |
| Between US-360 SB Off-Ramp and US-360 NB On-Ramp | Basic | 3,729 | A | 10.0 | 0.29 | B | 13.1 | 0.38 |
| US-360 NB On-Ramp | Merge | 4,042 | B | 16.6 | 0.47 | C | 20.5 | 0.57 |
| 1-44 After US-360 NB On-Ramp | Merge | 4,042 | B | 16.2 | 0.47 | B | 19.8 | 0.57 |

## 2040 No-Build Intersection Analysis Tables

US 60 Corridors

| $\begin{gathered} \text { Synchro } \\ \text { ID } \end{gathered}$ | Intersection | AM |  | PM |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS | Delay (s/veh) | LOS | Delay (s/veh) |
| US 60 West Corridor |  |  |  |  |  |
| 118* | US 60 WB Ramps \& Hwy MM | F | 64.3 | E | 42.4 |
| 115* | US 60 EB Ramps \& Hwy MM | F | 319.1 | F | 82.2 |
| 6 | US 60 WB Ramps \& Sunshine St | A | 8.8 | B | 19.7 |
| 12 | US 60 EB Ramps \& Sunshine St | A | 6.5 | A | 8.4 |
| 17 | US 60 WB Ramps \& West Bypass | B | 14.6 | C | 33.6 |
| 20 | US 60 EB Ramps \& West Bypass | B | 15.8 | B | 12.4 |
| 88 | US 60 WB Ramps \& Kansas Expwy | C | 25.3 | C | 25.7 |
| 93 | US 60 EB Ramps \& Kansas Expwy | B | 17 | C | 33 |
| 95 | US 60 EB Ramps Right \& Kansas Expwy | A | 4.1 | A | 4.8 |
| 31 | Campbell Ave \& Republic Rd | F | 90.1 | F | 169.4 |
| 28 | Campbell Ave \& US 60 WB Ramps | A | 8.6 | C | 20.4 |
| 24 | Campbell Ave \& US 60 EB Ramps | B | 13.7 | A | 7.1 |
| 36 | Campbell Ave \& El Camino Alto | C | 24.4 | C | 26.3 |
| 56* | US 60 \& National Ave WB On-Ramp | A | 0 | A | 0 |
| 64 | US 60 \& National Ave WB Off-Ramp Left | F | 1168.5 | F | 238.7 |
| 66 | US 60 \& National Ave North DDI Intersection | F | 89.4 | F | 149.3 |
| 68 | US 60 \& National Ave WB Off-Ramp Right | B | 16.8 | B | 12.5 |
| 62* | US 60 \& National Ave EB On-Ramp | B | 12 | F | 225 |
| 77 | US 60 \& National Ave EB Off-Ramp Left | C | 23.5 | B | 17.4 |
| 79 | US 60 \& National Ave South DDI Intersection | F | 148.6 | E | 76.8 |
| 81 | US 60 \& National Ave EB Off-Ramp Right | B | 11.7 | D | 43.5 |
| 46 | US 60 WB Ramps \& Glenstone Ave | E | 59 | F | 151 |
| 43 | US 60 EB Ramps \& Republic Rd/Glenstone | C | 20.5 | D | 47.8 |
| US 60 East Corridor |  |  |  |  |  |
| 5* | US 60 \& Highland Springs Blvd (N) | F | 103.2 | C | 20.2 |
| $6 *$ | US 60 \& Highland Springs Blvd (S) | F | 54.8 | F | 2249.6 |
| 8* | US 60 \& Farm Rd 189 (N) | F | 1219.6 | E | 38.8 |
| 9* | US 60 \& Farm Rd 189 (S) | E | 36.2 | F | 553.8 |
| 12* | US 60 \& Farm Rd 193 (N) | F | 862.8 | F | 88.3 |
| $13^{*}$ | US 60 \& Farm Rd 193 (S) | D | 27.6 | F | 493.5 |
| $60^{*}$ | US 60 WB Ramps \& Route NN/J | F | 93.4 | C | 18 |
| $63^{*}$ | US 60 EB Ramps \& Route NN/J | B | 14.5 | B | 14.6 |
| 16* | US 60 \& Farm Rd 205 (N) | F | 80.2 | E | 38.1 |
| 17* | US 60 \& Farm Rd 205 (S) | C | 23.5 | F | 123.1 |
| $20^{*}$ | US 60 \& Farm Rd 213 (N) | F | 85.5 | D | 26 |
| 21* | US 60 \& Farm Rd 213 (S) | C | 16.5 | E | 42.1 |
| 24* | US 60 \& Farm Rd 219 (N) | F | 180.5 | D | 26.1 |
| 25* | US 60 \& Farm Rd 219 (S) | C | 19.1 | F | 50 |
| 29* | US 60 \& Farm Rd 223 (N) | F | 275.2 | D | 31 |
| 30* | US 60 \& Farm Rd 223 (S) | C | 17.1 | D | 33.2 |
| 33* | US 60 \& Farm Rd 229 (N) | F | 192.2 | D | 28.1 |
| 34* | US 60 \& Farm Rd 229 (S) | B | 13 | C | 19.9 |
| 36 | US 60 \& Hwy 125 (N) | F | 1791.9 | F | 315 |
| 37 | US 60 \& Hwy 125 (S) | F | 289.1 | F | 363.1 |
| 40* | US 60 \& Farm Rd 241 (N) | D | 26.8 | A | 0 |
| 41* | US 60 \& Farm Rd 241 (S) | C | 24.4 | C | 22.4 |
| 53* | US 60 EB Off-Ramp \& Farm Rd 247 | A | 8.1 | A | 9.3 |

*At unsignalized intersections, LOS and delay for the worst movement is shown.

## 2040 No-Build Intersection Analysis Tables cont.

## I-44 Corridor

| Synchro <br> ID | Intersection | AM |  | PM |  |
| :---: | :--- | :---: | :---: | :---: | :---: |
|  |  | LOS | Delay (s/veh) | LOS | Delay (s/veh) |
| $117^{*}$ | I-44 WB Ramps \& Hwy MM | E | 38 | F | 244.6 |
| $113^{*}$ | I-44 EB Ramps \& Hwy MM | C | 22 | D | 30.2 |
| 101 | I-44 WB Ramps \& Chestnut Expwy | B | 12.1 | B | 15.4 |
| 96 | I-44 EB Ramps \& Chestnut Expwy | B | 11.4 | B | 13.9 |
| 85 | I-44 WB Ramps \& West Bypass | D | 41.3 | B | 11.7 |
| 81 | I-44 EB Ramps \& West Bypass | A | 6.2 | B | 10.5 |
| 54 | I-44 \& Route 13 EB Off-Ramp Right | A | 3 | A | 1.9 |
| 62 | I-44 \& Route 13 South DDI Intersection | B | 16.6 | C | 27 |
| 65 | I-44 \& Route 13 WB Off-Ramp Right | A | 5.5 | B | 18.3 |
| 66 | I-44 \& Route 13 North DDI Intersection | C | 21.3 | C | 24.4 |
| $67^{*}$ | I-44 \& Route 13 WB Off-Ramp Left | F | 74.3 | C | 22.2 |
| $59^{*}$ | I-44 \& Route 13 WB On-Ramp | A | 9.9 | B | 11.3 |
| 40 | I-44 WB Ramps \& Glenstone Ave | C | 20.9 | B | 19.5 |
| 36 | I-44 EB Ramps \& Glenstone Ave | C | 25.3 | B | 19.2 |
| $26^{*}$ | I-44 WB Ramps \& N Mulroy Rd | F | 174.6 | F | 508 |
| $17^{*}$ | I-44 EB Ramps \& N Mulroy Rd | D | 28.8 | C | 20.2 |
| $8^{*}$ | I-44 WB Ramps \& Hwy 125 | F | 7458 | F | 1695.9 |
| 7 | I-44 EB Ramps \& Hwy 125 | B | 16.6 | B | 13.9 |

*At unsignalized intersections, LOS and delay for the worst movement is shown.

## Appendix D

## Roadway Analysis Tables

## US 60 West Corridor

## Roadway Tables

J8P3032 : JAMES RIVER FREEWAY (360/60) HORIZONTAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  |  | Horizontal Geometrics |  |  | Horizontal Design Criteria |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station |  |  |  |  |  |  | 山 |  |  | 山 |
| CD-3690 | 4 | 29 | Ramp 1- WB 360-WB 44 | 04+53.67 | 0.09 | 40 | 40 | 0 | 1301 | 574 | 8.0\% | 600 | 444 | 8.0\% |
| CD-3690 | 4 | 29 | Ramp 1- WB 360-WB 44 | 07+51.80 | 0.01 | 40 | 40 | 0 | 876 | 984 | 6.8\% | 600 | 761 | 6.8\% |
| CD-3690 | 4 | 29 | Ramp 2- EB 44-EB 360 | 02+87.52 | 0.03 | 40 | 40 | 0 | 1579 | 1148 | 7.6\% | 600 | 583 | 7.6\% |
| CD-3690 | 4 | 29 | Ramp 3- WB 44-EB 360 Loop Ramp | 00+67.29 | 0.04 | 40 | 35 | 5 | 407 | 427 | 8.0\% | 600 | 444 | 8.0\% |
| CD-3690 | 4 | 29 | Ramp 3- WB 44-EB 360 Loop Ramp | 04+16.17 | 0.04 | 40 | 35 | 5 | 902 | 377 | 8.0\% | 600 | 444 | 8.0\% |
| CD-3690 | 4 | 29 | Ramp 3- WB 44-EB 360 Loop Ramp | 04+85.33 | 0.03 | 40 | 35 | 5 | 499 | 427 | 8.0\% | 600 | 444 | 8.0\% |
| CD-3690 | 4 | 29 | Ramp 4- WB 360-EB 44 | 04+26.06 | 0.16 | 40 | 40 | 0 | 2028 | 1148 | 7.6\% | 600 | 583 | 7.6\% |
| CD-3690 | 9 | 34 | ML Curve 1 | 10+62.20 | 0.67 Rt . | 70 | 65 | 5 | 1208 | 3822 | 4.8\% | 2100 | 4100 | 4.8\% |
| CD-3690 | 14 | 39 | Ramp 1- MM-WB 360 | 00+46.63 | 1.62 | 40 | 40 | 0 | 305 | 1493 | 5.8\% | 600 | 1030 | 5.8\% |
| CD-3690 | 14 | 39 | Ramp 2- EB 360-MM | 00+65.65 | 1.67 | 40 | 40 | 0 | 424 | 968 | 7.6\% | 600 | 583 | 7.6\% |
| CD-3690 | 14 | 39 | Ramp 2-EB 360-MM | 03+18.62 | 1.82 | 25 | 25 | 0 | 600 | 968 | 7.6\% | 375 | 182 | 7.6\% |
| CD-3690 | 14 | 39 | Ramp 3-WB 360-MM | 01+59.42 | 1.94 | 25 | 25 | 0 | 600 | 968 | 7.6\% | 375 | 182 | 7.6\% |
| CD-3690 | 14 | 39 | Ramp 3- WB 360-MM | 04+08.42 | 2.08 | 40 | 40 | 0 | 424 | 968 | 7.6\% | 600 | 583 | 7.6\% |
| CD-3690 | 14 | 39 | Ramp 4- MM-EB 360 | 03+91.36 | 2.16 | 40 | 40 | 0 | 305 | 1493 | 5.8\% | 600 | 1030 | 5.8\% |
| CD-3690 | 23 | 48 | ML Curve 2 | 44+83.54 | 2.80 Rt . | 70 | 65 | 5 | 1106 | 2871 | 6.0\% | 2100 | 3150 | 6.0\% |
| CD-3690 | 25 | 50 | Ramp 1- Sunshine-WB 360 | 00+68.66 | 3.44 | 40 | 40 | 0 | 443 | 968 | 7.6\% | 600 | 583 | 7.6\% |
| CD-3690 | 25 | 50 | Ramp 1- Sunshine-WB 360 | 03+34.88 | 3.59 | 40 | 40 | 0 | 662 | 968 | 7.6\% | 600 | 583 | 7.6\% |
| CD-3690 | 25 | 50 | Ramp 2-EB 360-Sunshine | 00+57.15 | 3.44 | 40 | 40 | 0 | 372 | 1280 | 6.6\% | 600 | 808 | 6.6\% |
| CD-3690 | 25 | 50 | ML Curve 3 | 59+40.68 | 3.83 Rt . | 70 | 65 | 5 | 1081 | 6548 | 3.0\% | 2100 | 6930 | 3.0\% |
| 6-3.331 | 3 | 13 | Ramp 3- WB 360-Sunshine | 07+67.28 | 3.84 | 40 | 35 | 5 | 1178 | 2292 | 3.0\% | 600 | 2510 | 3.0\% |
| 6-3.331 | 3 | 13 | Ramp 4- Sunshine-EB 360 | 06+28.26 | 3.72 | 40 | 35 | 5 | 866 | 955 | 6.0\% | 600 | 965 | 6.0\% |
| 6-3.331 | 3 | 13 | Ramp 4-Sunshine-EB 360 | $14+42.39$ | 3.85 | 40 | 20 | 20 | 420 | 955 | 2.6\% | 600 | 2960 | 2.6\% |
| 6-3.331 | 3 | 13 | ML Curve 4 | 30+81.23 | 77.90 Rt. | 70 | 60 | 10 | 2667 | 6548 | 2.6\% | 2100 | 8090 | 2.6\% |
| 6-3.331 | 7 | 17 | ML Curve 5 | 91+27.60 | 78.88 Lt . | 70 | 55 | 15 | 2632 | 3820 | 4.0\% | 2100 | 5050 | 4.0\% |
| 6-3.331 | 9 | 19 | Ramp 1- FF-WB 60 | 01+09.67 | 79.49 | 40 | 25 | 15 | 218 | 955 | 4.0\% | 600 | 1770 | 4.0\% |
| 6-3.331 | 9 | 19 | Ramp 2-EB 60-FF | 01+59.11 | 79.51 | 40 | 25 | 15 | 315 | 955 | 4.0\% | 600 | 1770 | 4.0\% |

J8P3032 : JAMES RIVER FREEWAY (360/60) HORIZONTAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  |  | Horizontal Geometrics |  |  | Horizontal Design Criteria |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station | $\begin{aligned} & \underset{\sim}{\underset{\sim}{\sim}} \\ & \underset{\sim}{\underset{\sim}{0}} \\ & \underset{\sim}{0} \end{aligned}$ |  |  |  |  | $\begin{aligned} & \frac{n}{\overline{0}} \\ & \stackrel{\pi}{\pi} \\ & \hline \end{aligned}$ | 山 |  0 <br>  0 <br> $\tilde{0}$  <br> $\tilde{0}$  | $\begin{aligned} & \text { n } \\ & \substack{0 \\ 0\\ } \end{aligned}$ | 山 |
| 6-3.331 | 9 | 19 | Ramp 2-EB 60-FF | 10+68.69 | 79.68 | 25 | 25 | 0 | 406 | 955 | 8.0\% | 375 | 134 | 8.0\% |
| 6-3.331 | 9 | 19 | Ramp 3-WB 60-FF | 05+21.17 | 79.81 | 40 | 40 | 0 | 521 | 955 | 8.0\% | 600 | 444 | 8.0\% |
| 6-3.331 | 9 | 19 | Ramp 3-WB 60-FF | 11+94.24 | 79.92 | 25 | 25 | 0 | 431 | 955 | 8.0\% | 375 | 134 | 8.0\% |
| 6-3.331 | 9 | 19 | Ramp 4- FF-EB 60 | 08+59.72 | 79.92 | 40 | 40 | 0 | 282 | 955 | 8.0\% | 600 | 444 | 8.0\% |
| 6-3.331 | 13 | 23 | ML Curve 6 | 185+32.27 | 80.66 Rt . | 70 | 55 | 15 | 1369 | 2292 | 6.0\% | 2100 | 3150 | 6.0\% |
| 6-3.331 | 15 | 27 | Ramp 1- Kansas Ave-WB 60 | 01+89.27 | 82.16 | 40 | 40 | 0 | 377 | 1910 | 4.0\% | 600 | 1770 | 4.0\% |
| 6-3.331 | 15 | 27 | Ramp 2- EB 60-Kansas Ave | 02+70.63 | 82.18 | 40 | 40 | 0 | 538 | 1910 | 4.0\% | 600 | 1770 | 4.0\% |
| 8-3.286 | 5 | 21 | Ramp 3- WB 60-Kansas Ave | 08+90.00 | 82.51 | 40 | 40 | 0 | 1058 | 1910 | 5.0\% | 600 | 1310 | 5.0\% |
| 8-3.286 | 5 | 21 | Ramp 3- WB 60-Kansas Ave | 18+19.89 | 82.67 | 25 | 25 | 0 | 320 | 1910 | 5.0\% | 375 | 499 | 5.0\% |
| 8-3.286 | 5 | 21 | Ramp 4- Kansas Ave- EB 60 | 10+42.69 | 82.58 | 40 | 40 | 0 | 1070 | 1910 | 5.0\% | 600 | 1310 | 5.0\% |
| 6-3.331 | 16 | 28 | ML Curve 7 | $52+56.52$ | 82.46 Lt . | 70 | 55 | 15 | 1907 | 2865 | 5.0\% | 2100 | 3910 | 5.0\% |
| 8-3.286 | 11 | 27 | ML Curve 8 | 101+98.28 | 83.38 Rt . | 70 | 60 | 10 | 1788 | 1910 | 7.0\% | 2100 | 2580 | 7.0\% |
| 8-3.286 | 12 | 28 | Ramp 1- Campbell Ave-WB 60 | 02+02.06 | 83.59 | 40 | 35 | 5 | 400 | 1146 | 5.0\% | 600 | 1310 | 5.0\% |
| 8-3.286 | 12 | 28 | Ramp 1- Campbell Ave-WB 60 | 12+05.79 | 83.77 | 25 | 25 | 0 | 532 | 1146 | 5.0\% | 375 | 499 | 5.0\% |
| 8-3.286 | 12 | 28 | Ramp 3- WB 60-Campbell Ave | 11+64.72 | 84.05 | 40 | 30 | 10 | 343 | 1910 | 3.0\% | 600 | 2510 | 3.0\% |
| 8-3.286 | 12 | 28 | Ramp 4- Campbell Ave- EB 60 | 05+13.96 | 83.9 | 25 | 25 | 0 | 556 | 1146 | 5.0\% | 375 | 499 | 5.0\% |
| 8-3.286 | 12 | 28 | Ramp 4- Campbell Ave- EB 60 | $13+86.03$ | 84.05 | 40 | 35 | 5 | 380 | 1146 | 5.0\% | 600 | 1310 | 5.0\% |
| 10-3.352 | 5 | 23 | Ramp 1- National Ave-WB 60 | 03+36.76 | 84.7 | 40 | 30 | 10 | 667 | 1910 | 3.0\% | 600 | 2510 | 3.0\% |
| 10-3.352 | 5 | 23 | Ramp 1- National Ave-WB 60 | 12+15.99 | 84.84 | 25 | 25 | 0 | 541 | 1146 | 5.0\% | 375 | 499 | 5.0\% |
| 10-3.352 | 5 | 23 | Ramp 2-EB 60-National Ave | 02+23.52 | 84.63 | 40 | 40 | 0 | 446 | 2546 | 3.0\% | 600 | 2510 | 3.0\% |
| 10-3.352 | 5 | 23 | Ramp 3- WB 60-National Ave | 11+35.58 | 85.1 | 40 | 35 | 5 | 498 | 3274 | 2.0\% | 600 | 3970 | 2.0\% |
| 10-3.352 | 5 | 23 | Ramp 4- National Ave-EB 60 | 03+21.48 | 84.95 | 25 | 25 | 0 | 327 | 1910 | 3.0\% | 375 | 1070 | 3.0\% |
| 10-3.352 | 5 | 23 | Ramp 4- National Ave-EB 60 | 09+30.71 | 85.06 | 40 | 40 | 0 | 532 | 1146 | 6.0\% | 600 | 965 | 6.0\% |
| 10-3.352 | 5 | 23 | ML Curve 9 | 182+17.83 | 84.95 Lt . | 70 | 55 | 15 | 1091 | 2865 | 5.0\% | 2100 | 3910 | 5.0\% |
| 13-3.297 | 5 | 16 | ML Curve 10 | 210+42.00 | 85.49 Lt . | 70 | 55 | 15 | 1390 | 5730 | 2.6\% | 2100 | 8090 | 2.6\% |
| 14-CD10753 | 3 | 23 | Ramp 2-EB 60-Republic Rd | 02+01.31 | 85.98 | 40 | 40 | 0 | 400 | 1432 | 6.4\% | 600 | 857 | 6.4\% |

J8P3032 : JAMES RIVER FREEWAY (360/60) HORIZONTAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  |  | Horizontal Geometrics |  |  | Horizontal Design Criteria |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station | $\begin{aligned} & \underset{\sim}{\underset{\sim}{0}} \\ & \underset{\sim}{\underset{\sim}{0}} \\ & \underset{\sim}{0} \end{aligned}$ |  |  |  |  |  | 山 |  |  | 山 |
| 14-CD10753 | 4 | 24 | Ramp 2-EB 60-Republic Rd | 08+57.57 | 86.1 | 25 | 20 | 5 | 825 | 764 | 3.6\% | 375 | 845 | 3.6\% |
| 14-CD10753 | 4 | 24 | Ramp 5- Republic Rd-EB 60 | 06+65.07 | 86.13 | 40 | 15 | 25 | 651 | 477 | 4.0\% | 600 | 1770 | 4.0\% |
| 14-CD10753 | 4 | 24 | Ramp 5- Republic Rd-EB 60 | 11+31.63 | 86.16 | 40 | 40 | 0 | 400 | 955 | 8.0\% | 600 | 444 | 8.0\% |
| 13-3.297 | 9 | 20 | Ramp 1- Bus 60-WB 360 | 01+25.32 | 86.06 | 40 | 30 | 10 | 250 | 1432 | 4.0\% | 600 | 1770 | 4.0\% |
| 13-3.297 | 9 | 20 | Ramp 3-WB 360-Bus 60 | 05+33.56 | 86.4 | 35 | 35 | 0 | 677 | 1637 | 4.0\% | 525 | 1370 | 4.0\% |
| 13-3.297 | 9 | 20 | Ramp 4- Bus 60-EB 360 | 07+32.67 | 86.46 | 40 | 40 | 0 | 635 | 955 | 7.0\% | 600 | 716 | 7.0\% |
| 15-CD10233 | 4 | 62 | WB ML Curve 1 | 263+57.39 | 86.49 Lt . | 70 | 55 | 15 | 1379 | 2292 | 6.0\% | 2100 | 3150 | 6.0\% |
| 15-CD10233 | 4 | 62 | EB ML Curve 1 | 263+58.72 | 87.06 Lt. | 70 | 60 | 10 | 1235 | 2083 | 7.0\% | 2100 | 2580 | 7.0\% |
| 15-CD10233 | 6 | 64 | WB ML Curve 2 | 173+44.00 | 87.41 Rt . | 70 | 60 | 10 | 1135 | 2145 | 7.0\% | 2100 | 2580 | 7.0\% |
| 15-CD10233 | 6 | 64 | EB ML Curve 2 | $173+48.29$ | 87.70 Rt . | 70 | 60 | 10 | 1067 | 1915 | 7.0\% | 2100 | 2580 | 7.0\% |
| 15-CD10233 | 6 | 64 | EB ML Curve 3 | 182+90.68 | 88.49 Lt . | 70 | 70 | 0 | 119 | 16963 | 2.0\% | 2100 | 10700 | 2.0\% |
| 15-CD10233 | 6 | 64 | WB ML Curve 3 | 183+24.94 | 88.50 Rt . | 70 | 70 | 0 | 50 | 17037 | 2.0\% | 2100 | 10700 | 2.0\% |
| 15-CD10233 | 13 | 71 | 65 Ramp N-W | 604+63.16 | 87.97 | 40 | 40 | 0 | 867 | 1000 | 7.6\% | 600 | 583 | 7.6\% |
| 15-CD10233 | 13 | 71 | 65 Ramp N-W | 614+53.84 | 87.67 | 40 | 40 | 0 | 492 | 806 | 7.6\% | 600 | 583 | 7.6\% |
| 15-CD10233 | 25 | 83 | 65 Ramp S-W | 303+35.92 | 87.91 | 40 | 40 | 0 | 698 | 1000 | 7.6\% | 600 | 583 | 7.6\% |
| 15-CD10233 | 6 | 64 | ML Curve 11 | 204+21.70 | 87.70 | 70 | 70 | 0 | 1800 | 17000 | 6.2\% | 2100 | 3020 | 6.2\% |
| 15-CD10233 | 6 | 64 |  | 204+21.70 | 87.70 | 70 | 60 | 10 | 587 | 2260 | 6.2\% | 2100 | 3020 | 6.2\% |
| 15-CD10233 | 25 | 83 | 65 Ramp S-W | 339+25.56 | 88.08 | 40 | 40 | 0 | 2486 | 1018 | 6.0\% | 600 | 965 | 6.0\% |
| 15-CD10233 | 13 | 71 | 65 Ramp S-W | 346+18.57 | 87.49 | 40 | 40 | 0 | 349 | 1930 | 4.6\% | 600 | 1470 | 4.6\% |
| 15-CD10233 | 22 | 80 | 65 Ramp W-N | 222+47.00 | 87.88 | 45 | 40 | 5 | 2182 | 1161 | 5.6\% | 675 | 1390 | 5.6\% |
| 15-CD10233 | 22 | 80 | 65 Ramp W-N | 237+45.64 | 87.83 | 45 | 45 | 0 | 552 | 2000 | 5.2\% | 675 | 1560 | 5.2\% |
| 15-CD10233 | 13 | 71 | 65 Ramp E-N | 500+37.53 | 87.99 | 45 | 35 | 10 | 75 | 716 | 6.8\% | 675 | 990 | 6.8\% |
| 15-CD10233 | 13 | 71 | 65 Ramp E-N | 509+71.21 | 87.82 | 45 | 45 | 0 | 774 | 1000 | 7.6\% | 675 | 765 | 7.6\% |
| 15-CD10233 | 13 | 71 | 65 Ramp W-S | 106+67.86 | 87.75 | 20 | 20 | 0 | 1022 | 3820 | 3.0\% | 300 | 730 | 3.0\% |
| 15-CD10233 | 13 | 71 | 65 Ramp W-S | 117+64.57 | 87.83 | 20 | 20 | 0 | 326 | 1280 | 5.4\% | 300 | 258 | 5.4\% |
| 15-CD10233 | 13 | 71 | 65 Ramp E-S | 00+70.62 | 87.72 | 20 | 20 | 0 | 140 | 430 | 5.6\% | 300 | 236 | 5.6\% |

J8P3032 : JAMES RIVER FREEWAY (360/60) HORIZONTAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  |  | Horizontal Geometrics |  |  | Horizontal Design Criteria |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station | $\begin{aligned} & \underset{\sim}{\widetilde{\sim}} \\ & \underset{\sim}{\underset{\sim}{0}} \\ & \underset{\sim}{0} \end{aligned}$ |  |  |  |  | $\begin{aligned} & \text { n } \\ & \substack{0\\ } \\ & \hline \end{aligned}$ | 山 |  | . | 出 |
| 15-CD10233 | 13 | 71 | 65 Ramp E-S | 01+90.92 | 87.72 | 20 | 15 | 5 | 100 | 215 | 5.6\% | 300 | 236 | 5.6\% |
| 15-CD10233 | 13 | 71 | 65 Ramp E-S | 02+91.94 | 87.72 | 20 | 15 | 5 | 100 | 150 | 5.6\% | 300 | 236 | 5.6\% |
| 15-CD10233 | 13 | 71 | 65 Ramp E-S | 04+68.09 | 87.72 | 20 | 15 | 5 | 231 | 215 | 5.6\% | 300 | 236 | 5.6\% |
| 15-CD10233 | 13 | 71 | 65 Ramp E-S | 06+73.72 | 87.72 | 20 | 20 | 0 | 180 | 150 | 7.2\% | 300 | 125 | 7.2\% |
| 15-CD10233 | 13 | 71 | 65 Ramp E-S | 08+02.02 | 87.72 | 20 | 20 | 0 | 100 | 215 | 7.2\% | 300 | 125 | 7.2\% |
| 15-CD10233 | 13 | 71 | 65 Ramp E-S | 09+21.72 | 87.72 | 20 | 20 | 0 | 140 | 430 | 7.2\% | 300 | 125 | 7.2\% |
| 15-CD10233 | 13 | 71 | 65 Ramp N-E | 00+70.63 | 87.83 | 20 | 15 | 5 | 140 | 430 | -2.0\% | 300 | 1640 | -2.0\% |
| 15-CD10233 | 13 | 71 | 65 Ramp N-E | 01+90.92 | 87.83 | 20 | 15 | 5 | 100 | 215 | -2.0\% | 300 | 1640 | -2.0\% |
| 15-CD10233 | 13 | 71 | 65 Ramp N-E | 03+22.74 | 87.83 | 20 | 15 | 5 | 152 | 158 | -2.0\% | 300 | 1640 | -2.0\% |
| 15-CD10233 | 25 | 83 | 65 Ramp S-E | 403+76.97 | 87.87 | 40 | 40 | 0 | 721 | 1000 | 7.6\% | 600 | 583 | 7.6\% |
| 15-CD10233 | 13 | 71 | WB ML Curve 4 | 205+28.13 | 87.70 | 70 | 70 | 0 | 547 | 2430 | 6.2\% | 2100 | 3020 | 6.2\% |
| 15-CD10233 | 13 | 71 | EB ML Curve 4 | 206+05.82 | 87.70 | 70 | 70 | 0 | 17 | 16963 | 6.2\% | 2100 | 3020 | 6.2\% |
| 15-CD10233 | 13 | 71 |  | 206+05.82 | 87.70 | 70 | 70 | 0 | 496 | 2490 | 6.2\% | 2100 | 3020 | 6.2\% |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Indicates posted advisory speed |  |  | Does not meet design criteria |  |  |  |  |  |  |  |  |
|  |  |  | Indicates design speed listed on plans |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## J8P3032 JAMES RIVER FREEWAY (360/60) VERTICAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station |  |  |  | Type (Sag, Crest) |  |  |  | $\underline{\square}$ |  |  |  |  | Req SSD - (Tbl 3-34/36 Green Book) | $\begin{aligned} & 0 \\ & \hat{\sim} \\ & 0 \\ & \frac{0}{\pi} \\ & \hline \end{aligned}$ |  |
| CD-3690 | 5 | 30 | Ramp 1-WB 360-WB 44 | 00+75.00 | 40 | 40 | 0 | C | 902.23 | -0.30 | -2.00 | 393.70 | 1.70 | 43.10 | 120.00 | 530.72 | 305 | 1085.82 | 0.00 |
| CD-3690 | 5 | 30 | Ramp 1-WB 360-WB 44 | 05+66.30 | 40 | 40 | 0 | S | 459.32 | -2.00 | 0.69 | 170.60 | 2.69 | 63.40 | 120.00 | 170.69 | 305 | N/A | 92.59 |
| CD-3690 | 5 | 30 | Ramp 1-WB 360-WB 44 | 08+25.75 | 40 | 40 | 0 | C | 328.08 | 0.69 | -1.95 | 124.67 | 2.65 | 43.10 | 120.00 | 124.04 | 305 | 571.98 | 0.00 |
| CD-3690 | 5 | 30 | Ramp 2-EB 44-EB 360 | 00+37.50 | 40 | 40 | 0 | C | 246.06 | 0.07 | -1.30 | 180.45 | 1.37 | 43.10 | 120.00 | 179.22 | 305 | 908.90 | 0.00 |
| CD-3690 | 5 | 30 | Ramp 2-EB 44-EB 360 | 01+39.99 | 40 | 40 | 0 | S | 393.70 | -1.30 | 2.80 | 95.14 | 4.10 | 63.40 | 120.00 | 96.07 | 305 | N/A | 141.01 |
| CD-3690 | 5 | 30 | Ramp 2- EB 44-EB 360 | 03+65.03 | 40 | 40 | 0 | C | 295.28 | 2.80 | 1.05 | 167.32 | 1.75 | 43.10 | 120.00 | 168.83 | 305 | 764.56 | 0.00 |
| CD-3690 | 5 | 30 | Ramp 2- EB 44-EB 360 | 04+48.89 | 40 | 40 | 0 | C | 213.25 | 1.05 | -0.30 | 157.48 | 1.35 | 43.10 | 120.00 | 158.08 | 305 | 906.48 | 0.00 |
| CD-3690 | 5 | 30 | Ramp 3- WB 44-EB 360 Loop Ramp | 00+22.50 | 40 | 40 | 0 | C | 147.64 | 0.63 | -1.53 | 68.24 | 2.16 | 43.10 | 120.00 | 68.26 | 305 | 572.66 | 0.00 |
| CD-3690 | 5 | 30 | Ramp 3- WB 44-EB 360 Loop Ramp | 02+18.11 | 40 | 40 | 0 | S | 295.28 | -1.53 | 2.00 | 82.02 | 3.53 | 63.40 | 120.00 | 83.60 | 305 | N/A | 121.53 |
| CD-3690 | 5 | 30 | Ramp 3-WB 44-EB 360 Loop Ramp | 07+06.34 | 40 | 40 | 0 | C | 902.23 | 2.00 | -0.30 | 393.70 | 2.30 | 43.10 | 120.00 | 392.27 | 305 | 920.25 | 0.00 |
| CD-3690 | 5 | 30 | Ramp 4- WB 360-EB 44 | 00+37.50 | 40 | 40 | 0 | C | 246.06 | 0.30 | -1.07 | 180.45 | 1.37 | 43.10 | 120.00 | 180.13 | 305 | 912.93 | 0.00 |
| CD-3690 | 5 | 30 | Ramp 4- WB 360-EB 44 | 01+30.00 | 40 | 40 | 0 | C | 295.28 | -1.07 | -2.70 | 180.45 | 1.64 | 43.10 | 120.00 | 180.16 | 305 | 805.97 | 0.00 |
| CD-3690 | 5 | 30 | Ramp 4- WB 360-EB 44 | 05+00.00 | 40 | 40 | 0 | S | 442.91 | -2.70 | 2.01 | 95.14 | 4.71 | 63.40 | 120.00 | 94.04 | 305 | N/A | 162.06 |
| CD-3690 | 5 | 30 | Ramp 4- WB 360-EB 44 | 05+93.17 | 40 | 40 | 0 | C | 164.04 | 2.01 | 0.56 | 114.83 | 1.45 | 43.10 | 120.00 | 113.45 | 305 | 828.22 | 0.00 |
| CD-3690 | 3 | 28 | ML Curve 1 | 01+50.00 | 70 | 70 | 0 | C | 902.23 | 2.00 | -0.30 | 393.70 | 2.30 | 246.90 | 210.00 | 392.27 | 730 | 920.25 | 0.00 |
| CD-3690 | 9 | 34 | ML Curve 2 | 07+00.00 | 70 | 70 | 0 | S | 295.28 | -0.30 | 0.44 | 396.98 | 0.74 | 180.30 | 210.00 | 397.95 | 730 | N/A | 78.19 |
| CD-3690 | 9 | 34 | ML Curve 3 | 12+00.00 | 70 | 70 | 0 | C | 295.28 | 0.44 | -0.40 | 351.05 | 0.84 | 246.90 | 210.00 | 350.68 | 730 | 1429.11 | 0.00 |
| CD-3690 | 11 | 36 | ML Curve 4 | $16+28.00$ | 70 | 70 | 0 | S | 295.28 | -0.40 | 0.43 | 354.33 | 0.83 | 180.30 | 210.00 | 355.33 | 730 | N/A | 87.57 |
| CD-3690 | 12 | 37 | ML Curve 5 | $21+00.00$ | 70 | 70 | 0 | C | 295.28 | 0.43 | -0.37 | 370.73 | 0.80 | 246.90 | 210.00 | 370.48 | 730 | 1501.46 | 0.00 |
| CD-3690 | 15 | 40 | Ramp 1- MM-WB 360 | 00+30.00 | 40 | 40 | 0 | C | 196.85 | -0.37 | -1.18 | 239.50 | 0.82 | 43.10 | 120.00 | 240.94 | 305 | 1419.11 | 0.00 |
| CD-3690 | 15 | 40 | Ramp 1- MM-WB 360 | 01+40.00 | 40 | 40 | 0 | S | 410.10 | -1.18 | 2.66 | 108.27 | 3.84 | 63.40 | 120.00 | 106.74 | 305 | N/A | 132.20 |
| CD-3690 | 15 | 40 | Ramp 1- MM-WB 360 | 03+82.00 | 40 | 40 | 0 | C | 262.47 | 2.66 | 1.00 | 157.48 | 1.66 | 43.10 | 120.00 | 158.30 | 305 | 782.02 | 0.00 |
| CD-3690 | 15 | 40 | Ramp 2- EB 360-MM | 00+25.00 | 40 | 40 | 0 | C | 164.04 | -0.38 | -1.69 | 124.67 | 1.31 | 43.10 | 120.00 | 125.22 | 305 | 905.69 | 0.00 |
| CD-3690 | 15 | 40 | Ramp 2-EB 360-MM | 01+60.00 | 40 | 40 | 0 | S | 475.72 | -1.69 | 2.67 | 108.27 | 4.37 | 63.40 | 120.00 | 108.94 | 305 | N/A | 150.26 |
| CD-3690 | 15 | 40 | Ramp 2- EB 360-MM | 04+13.20 | 25 | 25 | 0 | C | 295.28 | 2.67 | 1.00 | 177.17 | 1.68 | 11.10 | 75.00 | 176.28 | 155 | 791.82 | 0.00 |
| CD-3690 | 15 | 40 | Ramp 3- WB 360-MM | 00+73.30 | 25 | 25 | 0 | C | 393.70 | -1.00 | -3.93 | 134.51 | 2.93 | 11.10 | 75.00 | 134.60 | 155 | 565.74 | 0.00 |
| CD-3690 | 15 | 40 | Ramp 3- WB 360-MM | 03+22.04 | 40 | 40 | 0 | S | 524.93 | -3.93 | 2.60 | 82.02 | 6.52 | 63.40 | 120.00 | 80.49 | 305 | N/A | 224.41 |

J8P3032 JAMES RIVER FREEWAY (360/60) VERTICAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station |  |  |  |  |  |  | $\begin{aligned} & \text { oे } \\ & \stackrel{0}{0} \\ & \frac{\pi}{0} \\ & \stackrel{H}{x} \\ & \hline \end{aligned}$ | $\checkmark$ |  |  |  |  |  | $\begin{aligned} & \text { ज } \\ & \text { N } \\ & \frac{0}{\tilde{0}} \\ & \hline \end{aligned}$ |  |
| CD-3690 | 15 | 40 | Ramp 3- WB 360-MM | 04+56.96 | 40 | 30 | 10 | C | 98.43 | 2.60 | 2.33 | 374.02 | 0.26 | 43.10 | 120.00 | 372.82 | 305 | 4136.33 | 0.00 |
| CD-3690 | 15 | 40 | Ramp 4- MM-EB 360 | 00+53.00 | 40 | 40 | 0 | C | 262.47 | -1.00 | -3.50 | 104.99 | 2.50 | 43.10 | 120.00 | 105.03 | 305 | 563.01 | 0.00 |
| CD-3690 | 15 | 40 | Ramp 4- MM-EB 360 | 02+75.00 | 40 | 40 | 0 | S | 557.74 | -3.50 | 3.20 | 82.02 | 6.70 | 63.40 | 120.00 | 83.21 | 305 | N/A | 230.64 |
| CD-3690 | 15 | 40 | Ramp 4- MM-EB 360 | 04+22.67 | 40 | 30 | 10 | C | 98.43 | 3.20 | 2.55 | 150.92 | 0.65 | 43.10 | 120.00 | 151.19 | 305 | 1706.66 | 0.00 |
| CD-3690 | 13 | 38 | ML Curve 6 | 33+31.00 | 70 | 70 | 0 | S | 590.55 | -0.37 | 2.56 | 203.41 | 2.92 | 180.30 | 210.00 | 202.11 | 730 | N/A | 307.91 |
| CD-3690 | 21 | 46 | ML Curve 7 | 40+76.32 | 70 | 70 | 0 | C | 1476.38 | 2.56 | -2.56 | 288.71 | 5.12 | 246.90 | 210.00 | 288.52 | 730 | 789.07 | 0.00 |
| CD-3690 | 23 | 48 | ML Curve 8 | $44+72.60$ | 70 | 70 | 0 | S | 459.32 | -2.56 | -0.30 | 203.41 | 2.26 | 180.30 | 210.00 | 203.15 | 730 | N/A | 238.26 |
| CD-3690 | 24 | 49 | ML Curve 9 | 51+25.00 | 70 | 70 | 0 | C | 492.13 | -0.30 | -0.91 | 813.65 | 0.61 | 246.90 | 210.00 | 813.43 | 730 | 2029.53 | 0.00 |
| CD-3690 | 24 | 49 | ML Curve 10 | $55+00.00$ | 70 | 70 | 0 | S | 656.17 | -0.91 | 1.10 | 328.08 | 2.01 | 180.30 | 210.00 | 327.27 | 730 | N/A | 211.28 |
| CD-3827 | 14 | 23 | Ramp 1- Sunshine-WB 360 | 00+50.83 | 40 | 40 | 0 | C | 295.28 | -0.27 | -2.04 | 167.32 | 1.76 | 43.10 | 120.00 | 167.58 | 305 | 760.01 | 0.00 |
| CD-3827 | 14 | 23 | Ramp 1- Sunshine-WB 360 | 03+90.00 | 40 | 40 | 0 | S | 295.28 | -2.04 | 1.00 | 98.43 | 3.04 | 63.40 | 120.00 | 97.26 | 305 | N/A | 104.46 |
| CD-3827 | 14 | 23 | Ramp 2- EB 360-Sunshine | 00+89.97 | 40 | 40 | 0 | C | 295.28 | -0.27 | -2.14 | 157.48 | 1.86 | 43.10 | 120.00 | 158.49 | 305 | 726.81 | 0.00 |
| CD-3827 | 14 | 23 | Ramp 2- EB 360-Sunshine | 02+71.60 | 25 | 25 | 0 | S | 328.08 | -2.14 | 1.00 | 104.99 | 3.14 | 25.50 | 75.00 | 104.59 | 155 | N/A | 42.16 |
| 6-3.331 | 5 | 15 | Ramp 3- WB 360-Sunshine | 01+30.00 | 25 | 25 | 0 | S | 234.00 | -0.50 | 2.40 | 81.00 | 2.90 | 25.50 | 75.00 | 80.69 | 155 | N/A | 38.98 |
| 6-3.331 | 5 | 15 | Ramp 3-WB 360-Sunshine | 06+30.51 | 40 | 40 | 0 | C | 636.00 | 2.40 | -1.45 | 165.00 | 3.85 | 43.10 | 120.00 | 165.19 | 305 | 597.07 | 0.00 |
| 6-3.331 | 5 | 15 | Ramp 4-Sunshine-EB 360 | 01+25.00 | 40 | 40 | 0 | S | 220.00 | -1.00 | 1.00 | 110.00 | 2.00 | 63.40 | 120.00 | 110.00 | 305 | N/A | 68.82 |
| 6-3.331 | 5 | 15 | Ramp 4-Sunshine-EB 360 | 09+48.48 | 40 | 40 | 0 | C | 1000.00 | 1.00 | -1.35 | 425.00 | 2.35 | 43.10 | 120.00 | 425.53 | 305 | 958.28 | 0.00 |
| CD-3690 | 25 | 50 | ML Curve 11 | 58+55.07 | 70 | 70 | 0 | C | 813.65 | 1.10 | -2.00 | 262.47 | 3.10 | 246.90 | 210.00 | 262.47 | 730 | 752.60 | 0.00 |
| CD-3827 | 14 | 23 | WB ML Curve 1 | 60+25.00 | 70 | 50 | 20 | C | 164.04 | -2.00 | -2.11 | 1532.15 | 0.11 | 246.90 | 210.00 | 1518.91 | 730 | 10072.76 | 0.00 |
| CD-3827 | 14 | 23 | WB ML Curve 2 | 60+75.00 | 70 | 50 | 20 | S | 164.04 | -2.11 | -2.00 | 1509.19 | 0.11 | 180.30 | 210.00 | 1518.91 | 730 | N/A | 11.38 |
| CD-3827 | 14 | 23 | EB ML Curve 1 | $60+25.00$ | 70 | 50 | 20 | C | 164.04 | -2.00 | -2.42 | 393.70 | 0.42 | 246.90 | 210.00 | 394.33 | 730 | 2675.77 | 0.00 |
| CD-3827 | 14 | 23 | EB ML Curve 2 | 60+75.00 | 70 | 50 | 20 | S | 164.04 | -2.42 | -2.00 | 393.70 | 0.42 | 180.30 | 210.00 | 394.33 | 730 | N/A | 43.84 |
| 6-3.331 | 4 | 14 | ML Curve 12 | $31+00.17$ | 70 | 70 | 0 | S | 300.00 | -2.00 | -1.70 | 1000.00 | 0.30 | 180.30 | 210.00 | 1000.00 | 730 | N/A | 31.61 |
| 6-3.331 | 7 | 17 | ML Curve 13 | $83+00.00$ | 70 | 70 | 0 | S | 1100.00 | -1.70 | 0.40 | 524.00 | 2.10 | 180.30 | 210.00 | 523.81 | 730 | N/A | 221.29 |
| 6-3.331 | 10 | 20 | ML Curve 14 | 127+56.30 | 70 | 70 | 0 | S | 1500.00 | 0.40 | 2.00 | 938.00 | 1.60 | 180.30 | 210.00 | 937.50 | 730 | N/A | 168.60 |
| 6-3.331 | 11 | 21 | Ramp 1- FF-WB 60 | 03+95.90 | 40 | 35 |  | S | 250.00 | 0.50 | 5.50 | 56.00 | 5.00 | 63.40 | 120.00 | 50.00 | 305 | N/A | 172.04 |
| 6-3.331 | 11 | 21 | Ramp 1- FF-WB 60 | 10+25.45 | 25 | 25 |  | C | 280.00 | 5.50 | 1.00 | 62.20 | 4.50 | 11.10 | 75.00 | 62.22 | 155 | 379.78 | 0.00 |
| 6-3.331 | 11 | 21 | Ramp 2-EB 60-FF | 04+51.90 | 40 | 35 |  | S | 250.00 | 0.50 | 5.00 | 55.60 | 4.50 | 63.40 | 120.00 | 55.56 | 305 | N/A | 154.84 |
| 6-3.331 | 11 | 21 | Ramp 2-EB 60-FF | 12+80.27 | 25 | 25 | 0 | C | 350.00 | 5.00 | 1.00 | 87.50 | 4.00 | 11.10 | 75.00 | 87.50 | 155 | 444.75 | 0.00 |
| 6-3.331 | 11 | 21 | Ramp 3- WB 60-FF | $11+00.00$ | 40 | 35 | 5 | S | 200.00 | -0.45 | 3.57 | 49.80 | 4.02 | 63.40 | 120.00 | 49.75 | 305 | N/A | 138.32 |

## J8P3032 JAMES RIVER FREEWAY (360/60) VERTICAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station |  |  | Speed Difference (MPH) | Type (Sag, Crest) |  |  |  | $\underline{\square}$ |  |  |  |  | Req SSD - (Tbl 3-34/36 Green Book) | $\begin{aligned} & 0 \\ & \tilde{0} \\ & \underline{U} \\ & \frac{U}{0} \end{aligned}$ |  |
| 6-3.331 | 11 | 21 | Ramp 4- FF-EB 360 | 02+79.52 | 40 | 40 | 0 | C | 200.00 | -0.30 | -4.50 | 47.60 | 4.20 | 43.10 | 120.00 | 47.62 | 305 | 356.90 | 0.00 |
| 6-3.331 | 11 | 21 | Ramp 4- FF-EB 360 | 11+00.00 | 25 | 25 | 0 | S | 450.00 | -4.50 | 4.00 | 52.90 | 8.50 | 25.50 | 75.00 | 52.94 | 155 | N/A | 114.25 |
| 4-3.324 | 9 | 24 | ML Curve 15 | 157+10.00 | 70 | 70 | 0 | C | 1400.00 | 2.00 | 0.80 | 1167.00 | 1.20 | 246.90 | 210.00 | 1166.67 | 730 | 1599.17 | 0.00 |
| 6-3.331 | 13 | 23 | ML Curve 16 | 189+40.00 | 70 | 70 | 0 | S | 1000.00 | 0.80 | 1.20 | 2500.00 | 0.40 | 180.30 | 210.00 | 2500.00 | 730 | N/A | 42.15 |
| 6-3.331 | 14 | 26 | ML Curve 17 | 210+50.00 | 70 | 70 | 0 | C | 1000.00 | 1.20 | -0.40 | 625.00 | 1.60 | 246.90 | 210.00 | 625.00 | 730 | 1174.38 | 0.00 |
| 6-3.331 | 15 | 29 | ML Curve 18 | 39+76.00 | 70 | 70 | 0 | C | 600.00 | -0.40 | -1.30 | 667.00 | 0.90 | 246.90 | 210.00 | 666.67 | 730 | 1498.89 | 0.00 |
| 6-3.331 | 15 | 29 | Ramp 1-Kansas Ave-WB 60 | 04+06.00 | 40 | 40 | 0 | S | 380.00 | -1.00 | 2.58 | 106.00 | 3.58 | 63.40 | 120.00 | 106.15 | 0 | N/A | 123.18 |
| 6-3.331 | 15 | 29 | Ramp 1- Kansas Ave-WB 60 | 10+12.00 | 40 | 40 | 0 | C | 300.00 | 2.58 | 1.00 | 189.00 | 1.58 | 43.10 | 120.00 | 189.87 | 305 | 832.91 | 0.00 |
| 6-3.331 | 15 | 29 | Ramp 2-EB 60-Kansas Ave | 04+05.98 | 40 | 40 | 0 | S | 220.00 | -1.30 | 0.68 | 110.00 | 1.98 | 63.40 | 120.00 | 111.00 | 0 | N/A | 68.20 |
| 6-3.331 | 15 | 29 | Ramp 2-EB 60-Kansas Ave | 08+94.31 | 25 | 25 | 0 | S | 300.00 | 0.68 | 1.50 | 375.00 | 0.82 | 25.50 | 75.00 | 367.20 | 0 | N/A | 10.98 |
| 6-3.331 | 15 | 29 | ML Curve 19 | $45+23.50$ | 70 | 70 | 0 | S | 300.00 | -1.30 | -1.06 | 1250.00 | 0.24 | 180.30 | 210.00 | 1250.00 | 0 | N/A | 25.29 |
| 8-3.286 | 8 | 24 | Ramp 3- WB 360-Kansas Ave | 03+26.29 | 25 | 25 | 0 | C | 400.00 | -1.00 | -3.20 | 182.00 | 2.20 | 11.10 | 75.00 | 181.82 | 155 | 690.45 | 0.00 |
| 8-3.286 | 8 | 24 | Ramp 3-WB 360-Kansas Ave | 14+75.00 | 40 | 40 | 0 | S | 300.00 | -3.20 | -2.00 | 250.00 | 1.20 | 63.40 | 120.00 | 250.00 | 0 | N/A | 41.29 |
| 8-3.286 | 8 | 24 | Ramp 4- Kansas Ave- EB 360 | 09+04.47 | 40 | 40 | 0 | S | 300.00 | -3.30 | -1.10 | 136.00 | 2.20 | 63.40 | 120.00 | 136.36 | 0 | N/A | 75.70 |
| 8-3.286 | 9 | 25 | ML Curve 20 | $81+77.50$ | 70 | 70 | 0 | S | 1000.00 | -1.06 | 0.90 | 510.00 | 1.96 | 180.30 | 210.00 | 510.20 | 0 | N/A | 206.54 |
| 8-3.286 | 14 | 30 | Ramp 1-Campbell Ave-WB 60 | 04+68.33 | 40 | 40 | 0 | C | 500.00 | 1.46 | -1.50 | 169.00 | 2.96 | 43.10 | 120.00 | 168.92 | 305 | 614.53 | 0.00 |
| 8-3.286 | 14 | 30 | Ramp 1-Campbell Ave-WB 60 | 13+00.00 | 40 | 40 | 0 | S | 300.00 | -1.50 | 0.68 | 150.00 | 2.18 | 63.40 | 120.00 | 137.49 | 0 | N/A | 75.08 |
| 8-3.286 | 14 | 30 | Ramp 2- EB 60-Campbell Ave | 06+64.00 | 40 | 40 | 0 | C | 400.00 | -0.12 | -3.50 | 118.00 | 3.38 | 43.10 | 120.00 | 118.34 | 305 | 519.23 | 0.00 |
| 8-3.286 | 14 | 30 | Ramp 2-EB 60-Campbell Ave | $12+72.50$ | 25 | 25 | 0 | S | 300.00 | -3.50 | 0.00 | 85.70 | 3.50 | 25.50 | 75.00 | 85.71 | 0 | N/A | 47.04 |
| 8-3.286 | 13 | 29 | ML Curve 21 | 126+00.00 | 70 | 70 | 0 | C | 1400.00 | 0.90 | -2.10 | 467.00 | 3.00 | 246.90 | 210.00 | 466.67 | 730 | 1003.53 | 0.00 |
| 8-3.286 | 14 | 30 | Ramp 3- WB 360-Campbell Ave | 02+25.00 | 25 | 25 | 0 | S | 300.00 | -0.55 | 2.50 | 98.40 | 3.05 | 25.50 | 75.00 | 98.36 | 0 | N/A | 40.99 |
| 8-3.286 | 14 | 30 | Ramp 3- WB 360-Campbell Ave | 07+00.74 | 40 | 40 | 0 | C | 600.00 | 2.50 | -1.50 | 150.00 | 4.00 | 43.10 | 120.00 | 150.00 | 305 | 568.95 | 0.00 |
| 8-3.286 | 14 | 30 | Ramp 4-Campbell Ave- EB 360 | 00+32.63 | 40 | 40 | 0 | S | 280.00 | 0.00 | 2.80 | 100.00 | 2.80 | 63.40 | 120.00 | 100.00 | 0 | N/A | 96.34 |
| 8-3.286 | 14 | 30 | Ramp 4- Campbell Ave- EB 360 | 10+20.05 | 40 | 40 | 0 | C | 600.00 | 2.80 | -1.50 | 140.00 | 4.30 | 43.10 | 120.00 | 139.53 | 305 | 548.74 | 0.00 |
| 9-3.288 | 9 | 21 | ML Curve 22 | $148+00.00$ | 70 | 70 | 0 | S | 500.00 | -2.10 | 0.00 | 238.00 | 2.10 | 180.30 | 210.00 | 238.10 | 0 | N/A | 221.29 |
| 10-3.352 | 6 | 24 | ML Curve 23 | 173+34.94 | 70 | 70 | 0 | S | 900.00 | 0.00 | 1.54 | 584.00 | 1.54 | 180.30 | 210.00 | 584.42 | 0 | N/A | 162.28 |
| 10-3.352 | 7 | 31 | Ramp 1- National Ave-WB 60 | 05+82.98 | 40 | 40 | 0 | S | 500.00 | -0.40 | 4.50 | 102.00 | 4.90 | 63.40 | 120.00 | 102.04 | 0 | N/A | 168.60 |
| 10-3.352 | 7 | 31 | Ramp 1- National Ave-WB 60 | 13+00.00 | 40 | 40 | 0 | C | 300.00 | 4.50 | 1.00 | 86.00 | 3.50 | 43.10 | 120.00 | 85.71 | 305 | 458.29 | 0.00 |
| 10-3.352 | 7 | 31 | Ramp 2-EB 60-National Ave | 06+28.79 | 40 | 40 | 0 | S | 580.00 | -0.50 | 5.00 | 106.00 | 5.50 | 63.40 | 120.00 | 105.45 | 0 | N/A | 189.25 |
| 10-3.352 | 7 | 31 | Ramp 2-EB 60-National Ave | 12+89.50 | 25 | 25 | 0 | C | 300.00 | 5.00 | 1.00 | 75.00 | 4.00 | 11.10 | 75.00 | 75.00 | 155 | 419.75 | 0.00 |

## J8P3032 JAMES RIVER FREEWAY (360/60) VERTICAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \dot{ \pm} \\ \stackrel{0}{E} \\ \vdots \\ \vdots \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{gathered}$ | Location | Station |  |  | Speed Difference (MPH) |  |  | Entrance Grade \% |  | $\underline{\square}$ |  |  |  |  | Req SSD - (Tbl 3-34/36 Green Book) | $\begin{aligned} & 0 \\ & \hat{\sim} \\ & 0 \\ & \frac{0}{N} \\ & 0 \end{aligned}$ |  |
| 10-3.352 | 7 | 31 | Ramp 3- WB 60-National Ave | 03+00.00 | 25 | 25 | 0 | C | 150.00 | -1.00 | -2.00 | 150.00 | 1.00 | 11.10 | 75.00 | 150.00 | 155 | 1154.00 | 0.00 |
| 10-3.352 | 7 | 31 | Ramp 3-WB 60-National Ave | 08+06.27 | 40 | 40 | 0 | S | 380.00 | -2.00 | 2.00 | 95.00 | 4.00 | 63.40 | 120.00 | 95.00 | 0 | N/A | 137.63 |
| 10-3.352 | 7 | 31 | Ramp 4- National Ave-EB 60 | 02+00.00 | 40 | 40 | 0 | C | 200.00 | -1.00 | -2.40 | 143.00 | 1.40 | 43.10 | 120.00 | 142.86 | 305 | 870.71 | 0.00 |
| 10-3.352 | 7 | 31 | Ramp 4- National Ave-EB 61 | 08+30.45 | 40 | 40 | 0 | S | 450.00 | -2.40 | 3.00 | 83.00 | 5.40 | 63.40 | 120.00 | 83.33 | 0 | N/A | 185.81 |
| 13-3.297 | 8 | 19 | ML Curve 24 | 21+94.14 | 70 | 70 | 0 | C | 800.00 | 1.54 | -1.50 | 263.00 | 3.04 | 246.90 | 210.00 | 263.16 | 730 | 753.59 | 0.00 |
| 13-3.297 | 11 | 22 | Ramp 1- Bus 60-WB 360 | 05+08.10 | 40 | 35 | 5 | S | 410.00 | -1.73 | 5.00 | 61.00 | 6.73 | 63.40 | 120.00 | 60.92 | 0 | N/A | 231.57 |
| 13-3.297 | 11 | 22 | Ramp 1- Bus 60-WB 360 | 12+00.00 | 40 | 40 | 0 | C | 300.00 | 5.00 | 1.00 | 75.00 | 4.00 | 43.10 | 120.00 | 75.00 | 305 | 419.75 | 0.00 |
| 13-3.297 | 11 | 22 | Ramp 3-WB 360-Bus 60 | 02+00.00 | 40 | 40 | 0 | C | 200.00 | -1.00 | -1.93 | 215.00 | 0.93 | 43.10 | 120.00 | 215.05 | 305 | 1260.22 | 0.00 |
| 13-3.297 | 11 | 22 | Ramp 3-WB 360-Bus 60 | 08+12.71 | 40 | 40 | 0 | S | 300.00 | -1.93 | 1.60 | 85.00 | 3.53 | 63.40 | 120.00 | 84.99 | 0 | N/A | 121.46 |
| 13-3.297 | 11 | 22 | Ramp 4- Bus 60-EB 360 | 01+70.01 | 40 | 30 | 10 | C | 100.00 | -1.00 | -2.85 | 54.00 | 1.85 | 43.10 | 120.00 | 54.05 | 305 | 633.24 | 0.00 |
| 13-3.297 | 11 | 22 | Ramp 4-Bus 60-EB 360 | 06+00.00 | 40 | 35 | 5 | S | 330.00 | -2.85 | 2.73 | 59.00 | 5.58 | 63.40 | 120.00 | 59.14 | 0 | N/A | 192.00 |
| 13-3.297 | 10 | 21 | ML Curve 25 | 249+71.21 | 70 | 70 | 0 | S | 600.00 | -1.50 | 1.79 | 182.00 | 3.29 | 180.30 | 210.00 | 182.37 | 0 | N/A | 346.69 |
| 14-CD10753 | 14 | 34 | Ramp 2-EB 60-Republic Rd | 05+00.00 | 40 | 40 | 0 | C | 600.00 | -2.25 | -4.00 | 343.00 | 1.75 | 43.10 | 120.00 | 342.86 | 305 | 916.57 | 0.00 |
| 14-CD10753 | 14 | 34 | Ramp 2-EB 60-Republic Rd | 13+15.00 | 25 | 25 | 0 | S | 300.00 | -4.00 | 1.50 | 55.00 | 5.50 | 25.50 | 75.00 | 54.55 | 0 | N/A | 73.92 |
| 14-CD10753 | 14 | 34 | Ramp 5- Republic Rd-EB 60 | 02+30.00 | 40 | 35 | 5 | S | 300.00 | -1.50 | 4.25 | 52.00 | 5.75 | 63.40 | 120.00 | 52.17 | 0 | N/A | 197.85 |
| 14-CD10753 | 14 | 34 | Ramp 5- Republic Rd-EB 60 | 06+00.00 | 40 | 40 | 0 | C | 432.00 | 4.25 | 1.11 | 140.00 | 3.14 | 43.10 | 120.00 | 137.58 | 305 | 559.63 | 0.00 |
| 15-CD10233 | 7 | 65 | WB ML Curve 3 | 174+75.00 | 70 | 60 | 10 | C | 500.00 | -2.12 | -5.42 | 152.00 | 3.30 | 246.90 | 210.00 | 151.56 | 730 | 577.07 | 0.00 |
| 15-CD10233 | 7 | 65 | WB ML Curve 4 | 181+25.00 | 70 | 70 | 0 | C | 300.00 | -5.42 | -6.08 | 457.00 | 0.66 | 246.90 | 210.00 | 456.62 | 730 | 1792.31 | 0.00 |
| 15-CD10233 | 9 | 67 | ML Curve 26 | 189+00.00 | 70 | 60 | 10 | S | 750.00 | -6.05 | -0.72 | 141.00 | 5.33 | 180.30 | 210.00 | 140.82 | 0 | N/A | 561.23 |
| 15-CD10233 | 14 | 72 | ML Curve 27 | 196+75.00 | 70 | 65 | 5 | C | 650.00 | -0.72 | -3.89 | 205.00 | 3.17 | 246.90 | 210.00 | 205.18 | 730 | 665.59 | 0.00 |
| 15-CD10233 | 15 | 73 | WB ML Curve 5 | 205+25.00 | 70 | 70 | 0 | S | 700.00 | -3.89 | -0.27 | 193.00 | 3.62 | 180.30 | 210.00 | 193.16 | 0 | N/A | 381.88 |
| 15-CD10233 | 15 | 73 | EB ML Curve 3 | 204+75.00 | 70 | 60 | 10 | S | 550.00 | -4.50 | -0.59 | 141.00 | 3.91 | 180.30 | 210.00 | 140.59 | 0 | N/A | 412.23 |
| 15-CD10233 | 16 | 74 | US65 Ramp W-S | 109+75.00 | 20 | 20 | 0 | S | 300.00 | -1.95 | -1.26 | 436.00 | 0.69 | 16.50 | 60.00 | 436.05 | 0 | N/A | 5.92 |
| 15-CD10233 | 16 | 74 | US65 Ramp W-S | 118+00.00 | 20 | 20 | 0 | C | 400.00 | -1.26 | -4.96 | 108.00 | 3.70 | 6.10 | 60.00 | 108.25 | 115 | 492.02 | 0.00 |
| 15-CD10233 | 16 | 74 | US65 Ramp W-S | $124+75.00$ | 20 | 20 | 0 | S | 600.00 | -4.96 | 0.76 | 105.00 | 5.72 | 16.50 | 60.00 | 104.95 | 0 | N/A | 49.18 |
| 15-CD10233 | 17 | 75 | US65 Ramp W-N | 206+25.00 | 45 | 45 | 0 | S | 500.00 | -0.06 | 4.98 | 99.00 | 5.03 | 78.10 | 135.00 | 99.32 | 0 | N/A | 219.22 |
| 15-CD10233 | 17 | 75 | US65 Ramp W-N | 218+00.00 | 45 | 45 | 0 | C | 850.00 | 4.98 | -4.93 | 86.00 | 9.91 | 60.10 | 135.00 | 85.75 | 360 | 430.18 | 0.00 |
| 15-CD10233 | 23 | 81 | US65 Ramp W-N | 229+50.00 | 45 | 45 | 0 | S | 650.00 | -4.93 | 1.50 | 101.00 | 6.44 | 78.10 | 135.00 | 100.96 | 0 | N/A | 280.36 |
| 15-CD10233 | 18 | 76 | US65 Ramp S-W | $326+00.00$ | 40 | 40 | 0 | C | 1100.00 | 4.77 | -4.17 | 123.00 | 8.94 | 43.10 | 120.00 | 123.01 | 305 | 515.23 | 0.00 |
| 15-CD10233 | 18 | 76 | US65 Ramp S-W | $336+75.00$ | 40 | 40 | 0 | S | 650.00 | -4.17 | 1.92 | 107.00 | 6.09 | 63.40 | 120.00 | 106.77 | 0 | N/A | 209.48 |

J8P3032 JAMES RIVER FREEWAY (360/60) VERTICAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Location | Station |  |  |  |  |  |  |  | $\underline{\square}$ |  |  |  |  |  | $\begin{aligned} & \text { Nun } \\ & \text { - } \\ & \frac{0}{\pi} \\ & \hline \end{aligned}$ |  |
| 15-CD10233 | 19 | 77 | US65 Ramp E-S |  | 04+05.00 | 45 | 45 | 0 | S | 190.00 | 1.81 | 3.19 | 138.00 | 1.38 | 78.10 | 135.00 | 138.18 | 0 | N/A | 59.88 |
| 15-CD10233 | 19 | 77 | US65 Ramp N-W |  | 613+25.00 | 40 | 40 | 0 | S | 400.00 | -2.25 | 2.84 | 79.00 | 5.08 | 63.40 | 120.00 | 78.74 | 0 | N/A | 174.80 |
| 15-CD10233 | 28 | 86 | US 65 Ramp S-E |  | 403+75.00 | 20 | 20 | 0 | C | 250.00 | 1.68 | -1.24 | 85.00 | 2.92 | 6.10 | 60.00 | 85.50 | 115 | 494.02 | 0.00 |
| 15-CD10233 | 29 | 87 | US 65 Ramp S-W |  | 305+00.00 | 45 | 45 | 0 | S | 400.00 | -1.20 | 0.50 | 235.00 | 1.70 | 78.10 | 135.00 | 235.02 | 0 | N/A | 74.12 |
| 15-CD10233 | 29 | 87 | US 65 Ramp S-W |  | $312+00.00$ | 45 | 45 | 0 | S | 700.00 | 0.50 | 4.81 | 163.00 | 4.31 | 78.10 | 135.00 | 162.56 | 0 | N/A | 187.52 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | $\frac{\text { Indicates posted advisory speed }}{\text { Indicates design speed listed on plans }}$ |  |  |  |  |  |  |  |  |  | Does not meet design criteria |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

J8P3032 : JAMES RIVER FREEWAY (360/60) ACCELERATION \& DECELERATION GEOMETRICS

| Corridor Information |  |  |  |  |  |  | Ramp Geometrics |  |  |  |  | Ramp Criteria |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location |  | (HdW) pəəds duey ןeuoltexədo |  |  |  |  |  | ®o <br> $\stackrel{0}{0}$ <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br>  |  |  |  |
| CD-3690 | 4 | 29 | Ramp 1-WB 360-WB 44 | 70 | 40 | Acceleration | Parallel | 836.61 | 984.25 | 6.6\% | -2.00 | 1000 | 1.00 | 1000.00 |
| CD-3690 | 4 | 29 | Ramp 2- EB 44-EB 360 | 70 | 40 | Deceleration | Parallel | 836.61 | 1148.29 | 7.6\% | 2.00 | 440 | 1.00 | 440.00 |
| CD-3690 | 4 | 32 | Ramp 3- WB 44-EB 360 Loop Ramp | 70 | 35 | Deceleration | Parallel | 492.13 | 426.51 | 8.0\% | 1.00 | 490 | 1.00 | 490.00 |
| CD-3690 | 4 | 33 | Ramp 4- WB 360-EB 44 | 70 | 40 | Acceleration | Parallel | 590.55 | 1148.29 | 7.6\% | 0.56 | 1000 | 1.00 | 1000.00 |
| Current Project |  |  | Ramp 1- MM-WB 360 | 70 | 40 | Acceleration | Parallel | 579.70 | 1492.78 | 5.8\% | 0.37 | 1000 | 1.00 | 1000.00 |
| CD-3690 | 14 | 37 | Ramp 2-EB 360-MM | 70 | 40 | Deceleration | Parallel | 360.89 | 967.85 | 7.6\% | -0.37 | 440 | 1.00 | 440.00 |
| CD-3690 | 14 | 39 | Ramp 3- WB 360-MM | 70 | 30 | Deceleration | Parallel | 360.89 | 967.85 | 7.6\% | -2.56 | 520 | 1.00 | 520.00 |
| Current Project |  |  | Ramp 4- MM-EB 360 | 70 | 30 | Acceleration | Parallel | 665.70 | 1492.78 | 5.8\% | 2.56 | 1350 | 1.00 | 1350.00 |
| Current Project |  |  | Ramp 1- Sunshine-WB 360 | 70 | 40 | Acceleration | Parallel | 579.70 | 967.85 | 7.6\% | -0.90 | 1000 | 1.00 | 1000.00 |
| CD-3690 | 25 | 49 | Ramp 2-EB 360-Sunshine | 70 | 40 | Deceleration | Parallel | 360.89 | 1279.53 | 6.6\% | -0.90 | 440 | 1.00 | 440.00 |
| 6-3.331 | 3 | 13 | Ramp 3- WB 360-Sunshine | 70 | 35 | Deceleration | Parallel | 800.00 | 2291.83 | 3.0\% | 1.70 | 490 | 1.00 | 490.00 |
| Current Project |  |  | Ramp 4-Sunshine-EB 360 | 70 | 20 | Acceleration | Parallel | 820.00 | 954.93 | 2.4\% | -1.70 | 1520 | 1.00 | 1520.00 |
| Current Project |  |  | Ramp 1-FF-WB 60 | 70 | 25 | Acceleration | Parallel | 550.00 | 954.93 | 4.0\% | -1.00 | 1420 | 1.00 | 1420.00 |
| 6-3.331 | 9 | 19 | Ramp 2-EB 60-FF | 70 | 25 | Deceleration | Parallel | 40.00 | 954.93 | 4.0\% | 1.00 | 550 | 1.00 | 550.00 |
| 6-3.331 | 9 | 19 | Ramp 3- WB 60-FF | 70 | 35 | Deceleration | Parallel | 400.00 | 954.93 | 8.0\% | -2.00 | 490 | 1.00 | 490.00 |
| Current Project |  |  | Ramp 4-FF-EB 60 | 70 | 35 | Acceleration | Parallel | 580.00 | 954.93 | 8.0\% | 2.00 | 1230 | 1.00 | 1230.00 |
| Current Project |  |  | Ramp 1- Kansas Ave-WB 60 | 70 | 40 | Acceleration | Parallel | 550.00 | 1909.86 | 4.0\% | 0.40 | 1000 | 1.00 | 1000.00 |
| 6-3.331 | 15 | 27 | Ramp 2-EB60-Kansas Ave | 70 | 40 | Deceleration | Parallel | 350.00 | 1909.86 | 4.0\% | -0.40 | 440 | 1.00 | 440.00 |
| 8-3.286 | 5 | 21 | Ramp 3- WB 60-Kansas Ave | 70 | 40 | Deceleration | Parallel | NA | 1909.86 | 5.0\% | 1.00 | 440 | 1.00 | 440.00 |
| 8-3.286 | 5 | 21 | Ramp 4- Kansas Ave- EB 60 | 70 | 40 | Acceleration | Parallel | NA | 1909.86 | 5.0\% | -1.00 | 1000 | 1.00 | 1000.00 |
| 8-3.286 | 12 | 28 | Ramp 1- Campbell Ave-WB 60 | 70 | 35 | Acceleration | Parallel | NA | 1145.92 | 5.0\% | -0.90\% | 1230 | 1.00 | 1230.00 |
| 8-3.286 | 12 | 28 | Ramp 2-EB 60-Campbell Ave | 70 | 35 | Deceleration | Parallel | NA | 1145.95 | 5.0\% | -0.90\% | 490 | 1.00 | 490.00 |
| 8-3.286 | 12 | 28 | Ramp 3- WB 60-Campbell Ave | 70 | 25 | Deceleration | Parallel | NA | 1109.86 | 3.0\% | 2.10\% | 550 | 1.00 | 550.00 |
| 8-3.286 | 12 | 28 | Ramp 4- Campbell Ave- EB 60 | 70 | 35 | Acceleration | Parallel | NA | 1145.92 | 5.0\% | -2.10\% | 1230 | 1.00 | 1230.00 |

J8P3032 : JAMES RIVER FREEWAY (360/60) ACCELERATION \& DECELERATION GEOMETRICS

| Corridor Information |  |  |  |  |  |  | Ramp Geometrics |  |  |  |  | Ramp Criteria |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \overline{0} \\ & \stackrel{U}{U} \\ & \stackrel{\pi}{1} \\ & \stackrel{\rightharpoonup}{0} \\ & \stackrel{\pi}{0} \\ & \hline \end{aligned}$ | $$ |
| 10-3.352 | 5 | 23 | Ramp 1- National Ave-WB 60 | 70 | 30 | Acceleration | Parallel | NA | 1909.86 | 3.0\% | 0.00\% | 1350 | 1.00 | 1350.00 |
| 10-3.352 | 5 | 23 | Ramp 2- EB 60-National Ave | 70 | 40 | Deceleration | Parallel | NA | 2546.48 | 3.0\% | 0.00\% | 440 | 1.00 | 440.00 |
| 10-3.352 | 5 | 23,8 | Ramp 3- WB 60-National Ave | 70 | 35 | Deceleration | Parallel | 2800.00 | 3274.04 | 2.0\% | -1.54\% | 490 | 1.00 | 490.00 |
| 10-3.352 | 5 | 23,8 | Ramp 4- National Ave-EB 61 | 70 | 40 | Acceleration | Parallel | 2600.00 | 1145.95 | 6.0\% | 1.54\% | 1000 | 1.00 | 1000.00 |
| 14-CD10753 | 3 | 23,3 | Ramp 2-EB 60-Republic Rd | 70 | 40 | Deceleration | Parallel | 400.00 | 1432.39 | 6.4\% | -1.60\% | 440 | 1.00 | 440.00 |
| 14-CD10753 | 4 | 24,3 | Ramp 5- Republic Rd-EB 60 | 70 | 15 | Acceleration | Parallel | 450.00 | 954.93 | 8.0\% | 2.00\% | 1560 | 1.00 | 1560.00 |
| 13-3.297 | 5 | 20 | Ramp 1- Bus 60-WB 360 | 70 | 30 | Acceleration | Parallel | 400.00 | 1432.39 | 4.0\% | 0.00\% | 1350 | 1.00 | 1350.00 |
| 13-3.297 | 5 | 20 | Ramp 3- WB 360-Bus 60 | 70 | 40 | Deceleration | Parallel | NA | 1637.02 | 4.0\% | -1.54\% | 440 | 1.00 | 440.00 |
| 13-3.297 | 5 | 20 | Ramp 4- Bus 60-EB 360 | 70 | 35 | Acceleration | Parallel | NA | 954.93 | 7.0\% | 1.54\% | 1230 | 1.00 | 1230.00 |
| 15-CD10233 | 13 | 71 | 65 Ramp N-W | 70 | 40 | Acceleration | Parallel | 800.00 | 806.00 | 7.6\% | 2.25\% | 1000 | 1.00 | 1000.00 |
| 15-CD10233 | 13 | 71 | 65 Ramp N-E | 70 | 15 | Acceleration | Parallel | 300.00 | 430.00 | -2.0\% | -0.60\% | 1560 | 1.00 | 1560.00 |
| 15-CD10233 | 13 | 71 | 65 Ramp S-W | 70 | 45 | Acceleration | Parallel | NA | 1930.00 | 4.6\% |  | 820 | 1.00 | 820.00 |
| 15-CD10233 | 25 | 83 | 65 Ramp S-E | 70 | 40 | Acceleration | Parallel | 380.00 | 1000.00 | 7.6\% |  | 1000 | 1.00 | 1000.00 |
| 15-CD10233 | 13 | 71 | 65 Ramp W-N | 70 | 50 | Deceleration | Parallel | 850.00 | 2000.00 | 5.2\% |  | 340 | 1.00 | 340.00 |
| 15-CD10233 | 13 | 71 | 65 Ramp E-S | 70 | 15 | Deceleration | Parallel | 350.00 | 430.00 | 5.6\% | 0.27\% | 590 | 1.00 | 590.00 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | Does not meet design criteria |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | Current Ramp extension project |  |  |  |  |  |  |  |  |  |  |

## US 60 East Corridor

## Roadway Tables

J8P0683G \& JGP0683E: US-60 EAST FREEWAY HORIZONTAL GEOMETRICS

| J8P0683G \& JGP0683E: US-60 EAST FREEWAY HORIZONTAL GEOMETRICS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Corridor Information |  |  |  |  |  |  |  |  | Horizontal Geometrics |  |  | Horizontal Design Criteria |  |  |
|  |  |  | Location | Station |  |  |  |  |  |  | (1) |  |  | 山 |
| 1-3.190 | 3 | 14 | EB\&WB ML E. of US-65 | 217+70.00 | 87.93 | 60 | 60 | 0 |  |  |  | 900 | 0 | 0.0\% |
| 1-3.190 | 3 | 14 | Ramp 2 WB60-NB65 | 03+15.00 | 87.99 | 40 | 35 | 5 | 593.1 | 716.78 | 8.0\% | 600 | 444 | 8.0\% |
| 15-CD 10233 | CP8 | 105 | Ramp S-E NB65-EB60 | 413+12.48 | 88.05 | 40 | 40 | 0 | 619.63 | 716.20 | 8.0\% | 600 | 444 | 8.0\% |
| 1-3.190 | 4 | 16 | EB ML Curve 1 | 247+25.70 | 88.48 Rt . | 60 | 40 | 20 | 614.6 | 1432.69 | 8.0\% | 900 | 1200 | 8.0\% |
| 1-3.190 | 4 | 16 | EB ML Curve 2 | 259+19.40 | 88.73 Rt . | 60 | 60 | 0 | 1300 | 13588.18 | -2.0\% | 900 | 11500 | -2.0\% |
| 1-3.190 | 17 | 41 | EB ML Curve 3 | 643+95.50 | 95.98 Lt . | 60 | 50 | 10 | 1173.3 | 2864.93 | 6.0\% | 900 | 2320 | 6.0\% |
| 1-3.190 | 4 | 16 | WB ML Curve 1 | 247+82.00 | 88.49 Lt . | 60 | 50 | 10 | 751.1 | 1432.69 | 8.0\% | 900 | 1200 | 8.0\% |
| 5-8P0683D | 4 | 70 | WB ML Curve 2 (WB60C1) | 320+07.09 | 89.86 Lt . | 60 | 15 | 45 | 261.32 | 3000.00 | 5.0\% | 900 | 2960 | 5.0\% |
| 5-8P0683D | 4 | 70 | WB ML Curve 3 (WB60C2) | 325+38.74 | 89.96 Lt . | 60 | 15 | 45 | 268.64 | 3000.00 | 5.0\% | 900 | 2960 | 5.0\% |
| 5-8P0683D | 6 | 72 | WB ML Curve 4 (WB60C3) | 363+51.24 | 90.68 Lt . | 60 | 20 | 40 | 346.37 | 3000.00 | 5.0\% | 900 | 2960 | 5.0\% |
| 5-8P0683D | 6 | 72 | WB ML Curve 5 (WB60C4) | 369+54.11 | 90.79 Lt . | 60 | 20 | 40 | 326.12 | 3000.00 | 5.0\% | 900 | 2960 | 5.0\% |
| 3-3.025 |  | 21 | WB ML Curve 6 | 161+15.50 | 85.22 Lt . | 60 | 15 | 45 | 240.7 | 2292.00 | 3.6\% | 900 | 4400 | 3.6\% |
| 3-3.025 |  | 21 | WB ML Curve 7 | 166+01.10 | 85.29 Rt . | 60 | 15 | 45 | 281.3 | 2292.00 | 3.6\% | 900 | 4400 | 3.6\% |
| 1-3.190 |  | 41 | WB ML Curve 8 (Temp Conn) | 638+90.30 | 95.89 Lt . | 60 | 30 | 30 | 475 | 2864.93 | 6.0\% | 900 | 2320 | 6.0\% |
| 1-3.190 | 17 | 41 | WB ML Curve 9 (Lt Lane) | 647+83.20 | 96.03 Lt . | 60 | 50 | 10 | 809.2 | 2864.93 | 6.0\% | 900 | 2320 | 6.0\% |
| 5-8P0683D | 5 | 71 | Ramp 1 NN-WB60 Curve NWC1 | 03+50.01 | 90.18 | 40 | 40 | 0 | 688.47 | 1550.00 | 2.0\% | 600 | 3970 | 2.0\% |
| 5-8P0683D | 5 | 71 | Ramp 2 EB60-NN Curve SWC1 | 02+15.11 | 90.18 | 40 | 20 | 20 | 427.31 | 1500.00 | 2.0\% | 600 | 3970 | 2.0\% |
|  | 5 | 71 | Ramp 2 EB60-NN Curve SWC2 | 07+46.42 | 90.32 | 25 | 15 | 10 | 233.62 | 500.00 | 2.0\% | 375 | 1720 | 2.0\% |
| 5-8P0683D | 5 | 71 | Ramp 3 WB60-NN Curve NEC1 | 03+25.44 | 90.35 | 25 | 15 | 10 | 592.19 | 1014.00 | 2.0\% | 375 | 1720 | 2.0\% |
| 5-8P0683D | 5 | 71 | Ramp 3 WB60-NN Curve NEC2 | 08+57.09 | 90.52 | 45 | 25 | 20 | 481.96 | 2200.00 | 2.0\% | 675 | 4930 | 2.0\% |
| 5-8P0683D | 5 | 71 | Ramp 4 NN-EB60 Curve SEC1 | 06+59.77 | 90.49 | 40 | 20 | 20 | 273.56 | 1500.00 | 2.0\% | 600 | 3970 | 2.0\% |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Indicates posted advisory speed |  |  |  |  | Does not meet design criteria |  |  |  |  |  |  |  |  |  |
|  | Indicates design speed listed on plans |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

J8P0683G \& JGP0683E: US-60 EAST FREEWAY VERTICAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station |  |  |  |  |  |  | $\begin{aligned} & \text { do } \\ & \frac{0}{0} \\ & \frac{0}{0} \\ & \hline \mathbf{x} \\ & \hline \mathbf{x} \end{aligned}$ | $\underline{\square}$ |  |  |  |  | Req SSD - (Tbl 3-34/36 Green Book) | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & \frac{0}{0} \\ & \hline \end{aligned}$ |  |
| 1-3.190 | 3 | 14 | Ramp 2 WB60-NB65 | 04+68.90 | 40 | 40 | 0 | S | 600 | -0.80 | 3.00 | 157.89 | 3.8 | 63.4 | 120 | 157.9 | 305 | N/A | 131 |
| 1-3.190 | 3 | 14 | Ramp 4 NB65-EB60 | 13+69.60 | 40 | 40 | 0 | S | 188.8 | 0.00 | 1.40 | 134.86 | 1.4 | 63.4 | 120 | 134.9 | 305 | N/A | 48 |
| 1-3.190 | 3 | 14 | EB ML Curve 1 | 224+76.70 | 60 | 60 | 0 | S | 300 | 0.00 | 1.50 | 200.00 | 1.5 | 135.7 | 180 | 200.0 | 570 | N/A | 116 |
| 1-3.190 | 3 | 14 | EB ML Curve 2 | 234+75.00 | 60 | 45 | 15 | S | 500 | 1.50 | 7.00 | 90.91 | 5.5 | 135.7 | 180 | 90.9 | 570 | N/A | 426 |
| 1-3.190 | 4 | 16 | EB ML Curve 3 | 241+03.80 | 60 | 30 | 30 | S | 100 | 7.00 | 7.30 | 333.33 | 0.3 | 135.7 | 180 | 333.3 | 570 | N/A | 23 |
| 1-3.190 | 4 | 16 | EB ML Curve 4 | 244+03.80 | 60 | 30 | 30 | C | 100 | 7.30 | 6.72 | 172.41 | 0.58 | 150.6 | 180 | 172.4 | 570 | 1910 | 0 |
| 1-3.190 | 4 | 16 | EB ML Curve 5 | 258+60.00 | 60 | 55 | 5 | C | 1080 | 6.72 | -2.00 | 123.85 | 8.72 | 150.6 | 180 | 123.9 | 570 | 517 | 0 |
| 1-3.190 | 5 | 18 | EB ML Curve 6 | 274+49.40 | 60 | 55 | 5 | S | 400 | -2.00 | 1.26 | 122.70 | 3.26 | 135.7 | 180 | 122.7 | 570 | N/A | 252 |
| 1-3.190 | 6 | 20 | EB ML Curve 7 | 299+75.60 | 60 | 60 | 0 | C | 600 | 1.26 | 0.40 | 697.67 | 0.86 | 150.6 | 180 | 697.7 | 570 | 1555 | 0 |
| 5-8P0683D | 9 | 75 | WB ML Curve 1 | 319+50.00 | 60 | 60 | 0 | C | 600 | 3.34 | -0.62 | 151.52 | 3.96 | 150.6 | 180 | 151.5 | 570 | 572 | 0 |
| 5-8P0683D | 9 | 75 | WB ML Curve 2 | 324+00.00 | 80 | 80 | 0 | S | 300 | -0.62 | 0.44 | 283.02 | 1.06 | 231 | 240 | 283.0 | 910 | N/A | 146 |
| 5-8P0683D | 9 | 75 | WB ML Curve 3 | $328+00.00$ | 80 | 80 | 0 | C | 400 | 0.44 | -0.40 | 476.19 | 0.84 | 383.7 | 240 | 476.2 | 910 | 1485 | 0 |
| 1-3.190 | 7 | 22 | EB ML Curve 8 | 328+00.00 | 60 | 60 | 0 | C | 400 | 0.40 | -0.40 | 500.00 | 0.8 | 150.6 | 180 | 500.0 | 570 | 1549 | 0 |
| 5-8P0683D | 11 | 77 | Ramp 1 NN-WB60 Curve 1A | 01+00.00 | 30 | 25 | 5 | C | 80 | -0.40 | -0.80 | 200.00 | 0.4 | 18.5 | 90 | 200.0 | 200 | 2738 | 0 |
| 5-8P0683D | 11 | 77 | Ramp 1 NN-WB60 Curve 1B | 03+00.00 | 30 | 30 | 0 | S | 280 | -0.80 | 6.39 | 38.94 | 7.19 | 36.4 | 90 | 38.9 | 200 | N/A | 139 |
| 5-8P0683D | 11 | 77 | Ramp 1 NN-WB60 Curve 1C | 06+30.00 | 30 | 30 | 0 | C | 100 | 6.39 | 2.00 | 22.78 | 4.39 | 18.5 | 90 | 22.8 | 200 | 296 | 0 |
| 5-8P0683D | 11 | 77 | Ramp 2 EB60-NN Curve 2A | 00+80.00 | 40 | 30 | 10 | C | 100 | -0.40 | -1.02 | 161.29 | 0.62 | 43.1 | 120 | 161.3 | 305 | 1790 | 0 |
| 5-8P0683D | 11 | 77 | Ramp 2 EB60-NN Curve 2B | 03+30.00 | 40 | 40 | 0 | S | 320 | -1.02 | 3.72 | 67.51 | 4.74 | 63.4 | 120 | 67.5 | 305 | N/A | 163 |
| 5-8P0683D | 11 | 77 | Ramp 2 EB60-NN Curve 2C | 08+00.00 | 25 | 25 | 0 | C | 120 | 3.72 | 1.29 | 49.38 | 2.43 | 11.1 | 75 | 49.4 | 155 | 504 | 0 |
| 5-8P0683D | 11 | 77 | Ramp 3 WB60-NN Curve 3A | 01+00.00 | 25 | 25 | 0 | C | 100 | 0.60 | -4.10 | 21.28 | 4.7 | 11.1 | 75 | 21.3 | 155 | 280 | 0 |
| 5-8P0683D | 11 | 77 | Ramp 3 WB60-NN Curve 3B | 07+90.00 | 45 | 45 | 0 | S | 380 | -4.10 | 0.51 | 82.43 | 4.61 | 78.1 | 135 | 82.4 | 360 | N/A | 201 |
| 5-8P0683D | 11 | 77 | Ramp 4 NN-EB60 Curve 4A | 00+80.00 | 40 | 30 | 10 | C | 100 | -2.58 | -5.72 | 31.85 | 3.14 | 43.1 | 120 | 31.8 | 305 | 394 | 0 |
| 5-8P0683D | 11 | 77 | Ramp 4 NN-EB60 Curve 4B | 04+40.00 | 40 | 40 | 0 | S | 400 | -5.72 | 0.29 | 66.56 | 6.01 | 63.4 | 120 | 66.6 | 305 | N/A | 207 |
| 4-3.026 |  | 5 | WB ML Curve 4 | 209+50.00 | 60 |  | 60 | S | 400 | -5.00 | 1.20 | 64.52 | 6.2 | 135.7 | 180 | 64.5 | 570 | N/A | 480 |
| 4-3.026 |  | 5 | WB ML Curve 5 | 213+50.00 | 60 | 55 | 5 | C | 200 | 1.20 | -0.46 | 120.48 | 1.66 | 150.6 | 180 | 120.5 | 570 | 750 | 0 |
| 4-3.026 |  | 5 | WB ML Curve 6 | 216+50.00 | 60 | 30 | 30 | S | 200 | -0.46 | 4.29 | 42.11 | 4.75 | 135.7 | 180 | 42.1 | 570 | N/A | 368 |
| 4-3.026 |  | 5 | WB ML Curve 7 | 221+00.00 | 60 | 45 | 15 | C | 600 | 4.29 | -5.50 | 61.29 | 9.79 | 150.6 | 180 | 61.3 | 570 | 364 | 0 |

J8P0683G \& JGP0683E: US-60 EAST FREEWAY VERTICAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station |  |  |  |  |  |  | $\begin{aligned} & \text { do } \\ & \frac{0}{0} \\ & \frac{\pi}{0} \\ & \stackrel{H}{x} \\ & \hline \end{aligned}$ | $\underline{\square}$ |  |  |  |  |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & \frac{0}{0} \\ & 0 \end{aligned}$ |  |
| 4-3.026 |  | 5 | WB ML Curve 8 | 225+50.00 | 60 | 25 | 35 | S | 200 | -5.50 | 0.00 | 36.36 | 5.5 | 135.7 | 180 | 36.4 | 570 | N/A | 426 |
| 4-3.026 |  | 5 | WB ML Curve 9 | $229+73.00$ | 60 | 30 | 30 | S | 200 | 0.00 | 4.93 | 40.55 | 4.93 | 135.7 | 180 | 40.6 | 570 | N/A | 382 |
| 4-3.026 |  | 5 | WB ML Curve 10 | 234+75.00 | 60 | 55 | 5 | C | 600 | 4.93 | 0.70 | 141.71 | 4.23 | 150.6 | 180 | 141.7 | 570 | 553 | 0 |
| 4-3.026 |  | 6 | WB ML Curve 11 | 239+00.00 | 60 | 60 | 0 | S | 200 | 0.70 | 0.92 | 900.90 | 0.22 | 135.7 | 180 | 900.9 | 570 | N/A | 17 |
| 4-3.026 |  | 6 | WB ML Curve 12 | $242+20.00$ | 60 | 45 | 15 | C | 250 | 0.92 | -2.30 | 77.64 | 3.22 | 150.6 | 180 | 77.6 | 570 | 460 | 0 |
| 4-3.026 |  | 6 | WB ML Curve 13 | $245+00.00$ | 60 | 45 | 15 | S | 200 | -2.30 | 0.00 | 86.96 | 2.3 | 135.7 | 180 | 87.0 | 570 | N/A | 178 |
| 4-3.026 |  | 6 | WB ML Curve 14 | 251+00.00 | 60 | 50 | 10 | C | 300 | 0.00 | -2.79 | 107.53 | 2.79 | 150.6 | 180 | 107.5 | 570 | 537 | 0 |
| 4-3.026 |  | 6 | WB ML Curve 15 | 254+00.00 | 60 | 55 | 5 | S | 400 | -2.79 | 0.39 | 125.79 | 3.18 | 135.7 | 180 | 125.8 | 570 | N/A | 246 |
| 4-3.026 |  | 6 | WB ML Curve 16 | 261+00.00 | 60 | 60 | 0 | S | 200 | 0.39 | 1.77 | 145.35 | 1.38 | 135.7 | 180 | 145.3 | 570 | N/A | 107 |
| 4-3.026 |  | 7 | WB ML Curve 17 | 269+50.00 | 60 | 55 | 5 | C | 350 | 1.77 | -0.78 | 137.69 | 2.54 | 150.6 | 180 | 137.7 | 570 | 599 | 0 |
| 4-3.026 |  | 7 | WB ML Curve 18 | 273+75.00 | 60 | 45 | 15 | S | 300 | -0.77 | 2.89 | 82.06 | 3.66 | 135.7 | 180 | 82.1 | 570 | N/A | 283 |
| 4-3.026 |  | 7 | WB ML Curve 19 | $277+35.00$ | 60 | 60 | 0 | C | 400 | 2.89 | 1.00 | 211.64 | 1.89 | 150.6 | 180 | 211.6 | 570 | 771 | 0 |
| 4-3.026 |  | 7 | WB ML Curve 20 | 282+35.00 | 60 | 60 | 0 | C | 350 | 1.00 | 0.35 | 536.81 | 0.65 | 150.6 | 180 | 536.8 | 570 | 1830 | 0 |
| 4-3.026 |  | 7 | WB ML Curve 21 | 288+00.00 | 60 | 50 | 10 | S | 200 | 0.35 | 2.30 | 102.46 | 1.95 | 135.7 | 180 | 102.5 | 570 | N/A | 151 |
| 4-3.026 |  | 7 | WB ML Curve 22 | 293+00.00 | 60 | 45 | 15 | C | 350 | 2.30 | -2.30 | 76.09 | 4.6 | 150.6 | 180 | 76.1 | 570 | 410 | 0 |
| 4-3.026 |  | 7 | WB ML Curve 23 | 297+78.00 | 60 | 40 | 20 | S | 450 | -2.30 | 4.31 | 68.08 | 6.61 | 135.7 | 180 | 68.1 | 570 | N/A | 512 |
| 4-3.026 |  | 8 | WB ML Curve 24 | 302+60.00 | 60 | 45 | 15 | C | 480 | 4.31 | -3.28 | 63.24 | 7.59 | 150.6 | 180 | 63.2 | 570 | 369 | 0 |
| 4-3.026 |  | 8 | WB ML Curve 25 | $306+00.00$ | 60 | 35 | 25 | S | 200 | -3.28 | 0.24 | 56.82 | 3.52 | 135.7 | 180 | 56.8 | 570 | N/A | 273 |
| 4-3.026 |  | 8 | WB ML Curve 26 | $311+00.00$ | 60 | 35 | 25 | S | 300 | 0.24 | 5.60 | 55.97 | 5.36 | 135.7 | 180 | 56.0 | 570 | N/A | 415 |
| 4-3.026 |  | 8 | WB ML Curve 27 | $314+25.00$ | 60 | 60 | 0 | C | 300 | 5.60 | 4.18 | 211.27 | 1.42 | 150.6 | 180 | 211.3 | 570 | 910 | 0 |
| 4-3.026 |  | 8 | WB ML Curve 28 | $323+00.00$ | 60 | 50 | 10 | C | 550 | 4.18 | -1.73 | 93.14 | 5.91 | 150.6 | 180 | 93.1 | 570 | 448 | 0 |
| 4-3.026 |  | 8 | WB ML Curve 29 | 327+00.00 | 60 | 55 | 5 | S | 250 | -1.73 | 0.33 | 121.54 | 2.06 | 135.7 | 180 | 121.5 | 570 | N/A | 159 |
| 4-3.026 |  | 9 | WB ML Curve 30 | $330+75.00$ | 60 | 60 | 0 | S | 200 | 0.33 | 0.85 | 384.62 | 0.52 | 135.7 | 180 | 384.6 | 570 | N/A | 40 |
| 4-3.026 |  | 9 | WB ML Curve 31 | $333+75.00$ | 60 | 55 | 5 | C | 350 | 0.85 | -1.50 | 148.94 | 2.35 | 150.6 | 180 | 148.9 | 570 | 634 | 0 |
| 4-3.026 |  | 9 | WB ML Curve 32 | $336+75.00$ | 60 | 60 | 0 | S | 250 | -1.50 | 0.20 | 147.06 | 1.7 | 135.7 | 180 | 147.1 | 570 | N/A | 132 |
| 4-3.026 |  | 9 | WB ML Curve 33 | $342+75.00$ | 60 | 55 | 5 | S | 250 | 0.20 | 2.24 | 122.37 | 2.04 | 135.7 | 180 | 122.4 | 570 | N/A | 158 |
| 4-3.026 |  | 9 | WB ML Curve 34 | $346+00.00$ | 60 | 60 | 0 | C | 300 | 2.24 | 0.80 | 207.90 | 1.44 | 150.6 | 180 | 207.9 | 570 | 898 | 0 |
| 4-3.026 |  | 9 | WB ML Curve 35 | 350+00.00 | 60 | 55 | 5 | C | 400 | 0.80 | -1.99 | 143.52 | 2.79 | 150.6 | 180 | 143.5 | 570 | 587 | 0 |
| 4-3.026 |  | 10 | WB ML Curve 36 | 354+00.00 | 60 | 45 | 15 | S | 200 | -1.99 | 0.20 | 91.45 | 2.19 | 135.7 | 180 | 91.4 | 570 | N/A | 169 |
| 4-3.026 |  | 10 | WB ML Curve 37 | $362+00.00$ | 60 | 45 | 15 | S | 200 | 0.20 | 2.49 | 87.34 | 2.29 | 135.7 | 180 | 87.3 | 570 | N/A | 177 |

J8P0683G \& JGP0683E: US-60 EAST FREEWAY VERTICAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Location | Station |  |  |  |  |  |  | $\begin{aligned} & \text { do } \\ & \frac{0}{0} \\ & \frac{0}{0} \\ & +\frac{1}{x} \\ & \hline \end{aligned}$ | $\underline{\square}$ |  |  |  |  |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & \frac{0}{0} \\ & 0 \end{aligned}$ |  |
| 4-3.026 |  | 10 | WB ML Curve 38 |  | 364+75.00 | 60 | 60 | 0 | C | 350 | 2.49 | 0.79 | 205.76 | 1.7 | 150.6 | 180 | 205.8 | 570 | 809 | 0 |
| 4-3.026 |  | 10 | WB ML Curve 39 |  | 374+00.00 | 60 | 55 | 5 | C | 300 | 0.79 | -1.30 | 143.61 | 2.09 | 150.6 | 180 | 143.6 | 570 | 667 | 0 |
| 4-3.026 |  | 10 | WB ML Curve 40 |  | 377+00.00 | 60 | 60 | 0 | S | 200 | -1.30 | 0.00 | 153.85 | 1.3 | 135.7 | 180 | 153.8 | 570 | N/A | 101 |
| 4-3.026 |  | 10 | WB ML Curve 41 |  | $381+50.00$ | 60 | 60 | 0 | S | 500 | 0.00 | 3.19 | 156.99 | 3.19 | 135.7 | 180 | 157.0 | 570 | N/A | 247 |
| 4-3.026 |  | 10 | WB ML Curve 42 |  | $387+50.00$ | 60 | 55 | 5 | S | 300 | 3.19 | 0.59 | 115.38 | 2.6 | 135.7 | 180 | 115.4 | 570 | N/A | 201 |
| 4-3.026 |  | 11 | WB ML Curve 43 |  | 397+75.00 | 60 | 45 | 15 | C | 300 | 0.61 | -3.04 | 82.06 | 3.66 | 150.6 | 180 | 82.1 | 570 | 445 | 0 |
| 4-3.026 |  | 11 | WB ML Curve 44 |  | 401+50.00 | 60 | 35 | 25 | S | 200 | -3.04 | 0.56 | 55.57 | 3.6 | 135.7 | 180 | 55.6 | 570 | N/A | 279 |
| 4-3.026 |  | 11 | WB ML Curve 45 |  | 406+00.00 | 60 | 30 | 30 | S | 200 | 0.56 | -4.56 | 39.09 | 5.12 | 135.7 | 180 | 39.1 | 570 | N/A | 396 |
| 4-3.026 |  | 11 | WB ML Curve 46 |  | 409+75.00 | 60 | 45 | 15 | C | 400 | -4.56 | 0.25 | 83.16 | 4.81 | 150.6 | 180 | 83.2 | 570 | 424 | 0 |
| 4-3.026 |  | 11 | WB ML Curve 47 |  | 414+00.00 | 60 | 60 | 0 | S | 200 | 0.25 | 1.65 | 142.86 | 1.4 | 135.7 | 180 | 142.9 | 570 | N/A | 108 |
| 4-3.026 |  | 12 | WB ML Curve 48 |  | 418+00.00 | 60 | 45 | 15 | C | 350 | 1.65 | -3.40 | 69.31 | 5.05 | 150.6 | 180 | 69.3 | 570 | 389 | 0 |
| 4-3.026 |  | 12 | WB ML Curve 49 |  | 420+25.00 | 60 | 50 | 10 | S | 150 | -3.40 | 0.00 | 44.12 | 3.4 | 135.7 | 180 | 44.1 | 570 | N/A | 263 |
| 4-3.026 |  | 12 | WB ML Curve 50 |  | 426+00.00 | 60 | 60 | 0 | S | 200 | 0.00 | 1.11 | 180.18 | 1.11 | 135.7 | 180 | 180.2 | 570 | N/A | 86 |
| 4-3.026 |  | 12 | WB ML Curve 51 |  | $432+75.00$ | 60 | 55 | 5 | C | 300 | 1.11 | -1.50 | 114.94 | 2.61 | 150.6 | 180 | 114.9 | 570 | 563 | 0 |
| 4-3.026 |  | 12 | WB ML Curve 52 |  | $436+75.00$ | 60 |  | 60 | S | 200 | -1.50 |  | 133.33 | 1.5 | 135.7 | 180 | 133.3 | 570 | N/A | 116 |
| 4-3.026 |  | 12 | WB ML Curve 53 |  | 439+50.00 | 60 |  | 60 | C | 300 |  | -0.34 | 882.35 | 0.34 | 150.6 | 180 | 882.4 | 570 | 3324 | 0 |
| 5-8P0683D | 9 | 75 | WB ML Curve 54 |  | 353+50.00 | 80 | 80 | 0 | S | 400 | -0.40 | 0.70 | 363.64 | 1.1 | 231 | 240 | 363.6 | 910 | N/A | 151 |
| 1-3.190 | 7 | 22 | EB ML Curve 9 |  | 353+50.00 | 60 | 60 | 0 | S | 400 | -0.40 | 0.70 | 363.64 | 1.1 | 135.7 | 180 | 363.6 | 570 | N/A | 85 |
| 5-8P0683D | 9 | 75 | WB ML Curve 55 |  | 361+10.00 | 60 | 60 | 0 | S | 300 | 0.70 | 2.72 | 148.51 | 2.02 | 135.7 | 180 | 148.5 | 570 | N/A | 156 |
| 5-8P0683D | 9 | 75 | WB ML Curve 56 |  | $368+80.00$ | 60 | 60 | 0 | C | 880 | 2.72 | -2.85 | 157.99 | 5.57 | 150.6 | 180 | 158.0 | 570 | 584 | 0 |
| 1-3.190 | 9 | 26 | EB ML Curve 10 |  | 414+50.00 | 60 | 60 | 0 | C | 400 | 0.70 | -0.94 | 243.90 | 1.64 | 150.6 | 180 | 243.9 | 570 | 858 | 0 |
| 1-3.190 | 10 | 28 | EB ML Curve 11 |  | 440+00.00 | 60 | 60 | 0 | S | 400 | -0.94 | -0.40 | 740.74 | 0.54 | 135.7 | 180 | 740.7 | 570 | N/A | 42 |
| 1-3.190 | 11 | 30 | EB ML Curve 12 |  | 454+15.00 | 60 | 60 | 0 | S | 600 | -0.40 | 1.10 | 400.00 | 1.5 | 135.7 | 180 | 400.0 | 570 | N/A | 116 |
| 1-3.190 | 11 | 30 | EB ML Curve 13 |  | 470+00.00 | 60 | 60 | 0 | C | 800 | 1.10 | -0.80 | 421.05 | 1.9 | 150.6 | 180 | 421.1 | 570 | 968 | 0 |
| 1-3.190 | 12 | 32 | EB ML Curve 14 |  | 485+00.00 | 60 | 60 | 0 | S | 800 | -0.80 | 1.16 | 408.16 | 1.96 | 135.7 | 180 | 408.2 | 570 | N/A | 152 |
| 1-3.190 | 13 | 33 | EB ML Curve 15 |  | 512+50.00 | 60 | 60 | 0 | C | 400 | 1.16 | 0.64 | 769.23 | 0.52 | 150.6 | 180 | 769.2 | 570 | 2275 | 0 |
| 1-3.190 | 13 | 33 | EB ML Curve 16 |  | $533+70.70$ | 60 | 60 | 0 | S | 600 | 0.64 | 1.80 | 517.24 | 1.16 | 135.7 | 180 | 517.2 | 570 | N/A | 90 |
| 1-3.190 | 14 | 36 | EB ML Curve 17 |  | 551+25.00 | 60 | 60 | 0 | C | 1200 | 1.80 | -0.40 | 545.45 | 2.2 | 150.6 | 180 | 545.5 | 570 | 1085 | 0 |
| 1-3.190 | 15 | 38 | EB ML Curve 18 |  | 566+00.00 | 60 | 60 | 0 | S | 600 | -0.40 | 1.00 | 428.57 | 1.4 | 135.7 | 180 | 428.6 | 570 | N/A | 108 |
| 1-3.190 | 15 | 38 | EB ML Curve 19 |  | 576+60.70 | 60 | 60 | 0 | C | 600 | 1.00 | -0.40 | 428.57 | 1.4 | 150.6 | 180 | 428.6 | 570 | 1071 | 0 |

J8P0683G \& JGP0683E: US-60 EAST FREEWAY VERTICAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station |  |  |  |  |  |  | $\stackrel{\circ}{0}$ $\stackrel{0}{0}$ $\stackrel{0}{0}$ $\stackrel{\rightharpoonup}{x}$ $\stackrel{\rightharpoonup}{x}$ | $\underline{\square}$ |  |  |  |  |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  |
| 1-3.190 | 15 | 38 | EB ML Curve 20 | 587+70.60 | 60 | 60 | 0 | S | 600 | -0.40 | 0.96 | 441.18 | 1.36 | 135.7 | 180 | 441.2 | 570 | N/A | 105 |
| 1-3.190 | 16 | 39 | EB ML Curve 21 | 621+50.00 | 60 | 60 | 0 | C | 600 | 0.96 | 0.40 | 1071.43 | 0.56 | 150.6 | 180 | 1071.4 | 570 | 2227 | 0 |
| 1-3.190 | 17 | 41 | EB ML Curve 22 | $653+89.20$ | 60 | 60 | 0 | C | 600 | 0.40 | -0.80 | 500.00 | 1.2 | 150.6 | 180 | 500.0 | 570 | 1199 | 0 |
| 1-3.190 | 18 | 43 | WB ML Curve 57 | 653+25.30 | 60 | 60 | 0 | C | 600 | 0.40 | -0.80 | 500.00 | 1.2 | 150.6 | 180 | 500.0 | 570 | 1199 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Indicates posted advisory speed |  |  | Does not meet design criteria |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Indicates design speed listed on plans |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| J8P0683G \& JGP0683E: US-60 EAST FREEWAY ACCELERATION \& DECELERATION GEOMETRICS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Corridor Information |  |  |  |  |  |  | Ramp Geometrics |  |  |  |  | Ramp Criteria |  |  |
|  |  |  | Location |  |  |  |  |  |  |  |  | $\begin{aligned} & \frac{5}{40} \\ & \frac{0}{0} \\ & \frac{0}{4} \\ & \frac{0}{0} \\ & \frac{\pi}{0} \\ & \frac{\text { N }}{4} \end{aligned}$ |  |  |
| 5-8P0683D | 5 | 72 | Ramp 1 NN-WB60 | 60 | 25 | Acceleration | Parallel | 800.00 | 1550.00 | 2.0\% | 0.40\% | 1020 | 1.00 | 1020.00 |
| 5-8P0683D | 5 | 72 | Ramp 2 EB60-NN | 60 | 20 | Deceleration | Parallel | 350.00 | 1500.00 | 2.0\% | -0.40\% | 480 | 1.00 | 480.00 |
| 5-8P0683D | 5 | 72 | Ramp 3 WB60-NN | 60 | 25 | Deceleration | Parallel | 375.00 | 1014.00 | 2.0\% | -0.70\% | 460 | 1.00 | 460.00 |
| 5-8P0683D | 5 | 72 | Ramp 4 NN-EB60 | 60 | 20 | Acceleration | Parallel | 550.00 | 1500.00 | 2.0\% | 0.70\% | 1100 | 1.00 | 1100.00 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | Does not meet design criteria |  |  |  |  |  |  |  |  |  |  |

## I-44 Corridor

## Roadway Tables

J8I3044: I-44 FREEWAY HORIZONTAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  |  | Horizontal Geometrics |  |  | Horizontal Design Criteria |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\stackrel{\rightharpoonup}{\omega}$ $\stackrel{0}{E}$ 3 2 0 0 0 0 0 0 0 | Location | Station | $\begin{aligned} & \stackrel{\widetilde{\sim}}{\underset{\sim}{0}} \\ & \underset{\sim}{\underset{\sim}{0}} \\ & \underbrace{\prime}_{0} \end{aligned}$ |  |  |  |  |  | 山 |  |  | 山 |
| 1-3.176 | 8 | 38 | Ramp A- WB 44-County Road MM | 01+35.70 | 70.36 | 40 | 20 | 20 | 270.73 | 1273.57 | 2.0\% | 600 | 3970 | 2.0\% |
| 1-3.176 | 8 | 38 | Ramp B- County Road MM-WB 44 | 07+70.10 | 70.09 | 40 | 40 | 0 | 255.56 | 1273.57 | 6.0\% | 600 | 965 | 6.0\% |
| 1-3.176 | 8 | 38 | Ramp C- EB 44-County Road MM | 01+25.30 | 70.05 | 40 | 20 | 20 | 250.00 | 1432.69 | 2.0\% | 600 | 3970 | 2.0\% |
| 1-3.176 | 8 | 38 | Ramp D- County Road MM-EB 44 | 06+82.50 | 70.33 | 40 | 40 | 0 | 260.00 | 1146.28 | 6.0\% | 600 | 965 | 6.0\% |
| 1-3.176 | 13 | 45 | ML- Curve 1 | 640+55.70 | 72.03 RT | 70 | 70 | 0 | 2710.70 | 4583.75 | 5.0\% | 2100 | 3910 | 5.0\% |
| 1-3.176 | 22 | 65 | Old Ramp 1- EB 44-Rte 266 | 01+96.54 | 72.36 | 30 | 30 | 0 | 387.50 | 955.37 | 6.0\% | 450 | 506 | 6.0\% |
| 2.5-CD 120329 | 8 | 30 | Ramp 2-1- EB 44-Rte 266 | 01+31.19 | 72.51 | 25 | 15 | 10 | 250.22 | 337.03 | -2.0\% | 375 | 0 | -2.0\% |
| 2.5-CD 120329 | 7 | 29 | Ramp 4-Rte 266-WB 44 | 00+64.98 | 72.48 | 25 | 15 | 10 | 128.10 | 310.00 | 2.0\% | 375 | 1720 | 2.0\% |
| 1-3.176 | 22 | 65 | Old Ramp 4- Rte 266-WB 44 | 08+42.18 | 72.48 | 25 | 15 | 10 | 383.97 | 550.00 | 2.0\% | 375 | 1720 | 2.0\% |
| 1-3.176 | 22 | 65 | Old Ramp 4- Rte 266-WB 44 | 13+31.42 | 72.63 | 25 | 15 | 10 | 460.77 | 275.00 | 2.0\% | 375 | 1720 | 2.0\% |
| 1-3.176 | 22 | 65 | Old Ramp 4-Rte 266-WB 44 | 16+30.04 | 72.63 | 25 | 25 | 0 | 277.91 | 465.10 | 6.0\% | 375 | 332 | 6.0\% |
| 1-3.176 | 22 | 65 | Old Ramp 5-WB 44-Rte 266 | 03+32.45 | 72.68 | 40 | 35 | 5 | 622.06 | 716.78 | 6.0\% | 600 | 965 | 6.0\% |
| 2.5-CD 120329 | 7 | 29 | Ramp 5-WB 44-Rte 266 | 12+14.72 |  | 40 | 20 | 20 | 435.64 | 624.00 | 4.2\% | 600 | 1660 | 4.2\% |
| 2.5-CD 120329 | 7 | 29 | Ramp 5-WB 44-Rte 266 | 15+95.21 |  | 25 | 15 | 10 | 149.53 | 511.50 | 2.0\% | 375 | 1720 | 2.0\% |
| 1-3.176 | 22 | 65 | Old Ramp 7-Rte 266-EB 44 | 06+98.20 | 72.68 | 40 | 35 | 5 | 241.10 | 716.78 | 6.0\% | 600 | 965 | 6.0\% |
| 5-3.174B | 4 | 15 | Ramp 4- Rte 744-WB 44 Curve 4A | 10+27.70 | 74.90 | 40 | 40 | 0 | 488.50 | 716.78 | 8.0\% | 600 | 444 | 8.0\% |
| 5.5-3.247 | 27 | 44 | Ramp 1- Route 160-WB 44 | 01+49.11 | 75.34 | 40 | 40 | 0 | 295.83 | 954.93 | 8.0\% | 600 | 444 | 8.0\% |
| 5.5-3.247 | 27 | 44 | Ramp 2- EB 44-Route 160 | 01+95.87 | 75.37 | 40 | 40 | 0 | 386.39 | 954.93 | 8.0\% | 600 | 444 | 8.0\% |
| 5.5-3.247 | 27 | 44 | Ramp 3- WB 44-Route 160 | 09+89.84 | 75.69 | 40 | 40 | 0 | 476.04 | 1909.86 | 5.0\% | 600 | 1310 | 5.0\% |
| 5.5-3.247 | 27 | 44 | Ramp 4-Route 160-EB 44 | 10+56.27 | 75.70 | 40 | 40 | 0 | 292.38 | 1146.56 | 8.0\% | 600 | 444 | 8.0\% |
| 6-3.178 | 6 | 36 | ML- Curve 2 | $848+80.80$ | 75.96 | 70 | 65 | 5 | 2429.20 | 2864.93 | 6.0\% | 2100 | 3150 | 6.0\% |
| 6-3.178 | 22 | 51 | Ramp A- EB 44-Route 13 | 01+34.22 | 77.59 | 40 | 35 | 5 | 266.70 | 955.37 | 6.0\% | 600 | 965 | 6.0\% |
| 6-3.178 | 22 | 51 | Ramp B- Route 13-WB 44 | 07+90.70 | 77.60 | 40 | 35 | 5 | 279.20 | 955.37 | 6.0\% | 600 | 965 | 6.0\% |

J8I3044: I-44 FREEWAY HORIZONTAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  |  | Horizontal Geometrics |  |  | Horizontal Design Criteria |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station |  |  |  |  |  |  | 山 |  | $\begin{aligned} & \text { n } \\ & \stackrel{\bar{O}}{\pi} \\ & \end{aligned}$ | 山 |
| 6-3.178 | 24 | 53 | Ramp C- WB 44-Route 13 | 01+59.82 | 77.87 | 40 | 35 | 5 | 316.70 | 955.37 | 6.0\% | 600 | 965 | 6.0\% |
| 6-3.178 | 24 | 53 | Ramp D- Route 13-EB 44 | 07+37.15 | 77.87 | 40 | 35 | 5 | 300.00 | 955.37 | 6.0\% | 600 | 965 | 6.0\% |
| 7.5-CD 120808 | 21 | 67 | Ramp 1- Missouri H-WB 44 | 06+40.47 | 80.26 | 40 | 25 | 15 | 294.69 | 467.72 | 6.0\% | 600 | 965 | 6.0\% |
| 7.5-CD 120808 | 21 | 67 | Ramp 1- Missouri H-WB 44 | 11+96.28 | 80.18 | 40 | 30 | 10 | 517.40 | 690.00 | 6.0\% | 600 | 965 | 6.0\% |
| 7.5-CD 120808 | 23 | 69 | Ramp 3-EB 44-Missouri H | 02+94.67 | 80.27 | 40 | 30 | 10 | 556.96 | 689.77 | 6.0\% | 600 | 965 | 6.0\% |
| 7.5-CD 120808 | 23 | 69 | Ramp 3-EB 44-Missouri H | 09+26.70 | 80.36 | 25 | 25 | 0 | 285.09 | 371.00 | 6.0\% | 375 | 332 | 6.0\% |
| 8-3.157 | 70 | 55 | Ramp 6- WB 44-Missouri H | 02+94.70 | 80.55 | 40 | 30 | 10 | 556.50 | 690.00 | 6.0\% | 600 | 965 | 6.0\% |
| 7.5-CD 120808 | 25 | 71 | Ramp 6- WB 44-Missouri H | 09+62.43 | 80.46 | 25 | 25 | 0 | 433.88 | 467.72 | 6.0\% | 375 | 332 | 6.0\% |
| 7.5-CD 120808 | 27 | 73 | Ramp 8- Missouri H-EB 44 | 09+21.38 | 80.55 | 40 | 25 | 15 | 312.83 | 467.72 | 6.0\% | 600 | 965 | 6.0\% |
| 7.5-CD 120808 | 27 | 73 | Ramp 8- Missouri H-EB 44 | $12+75.53$ | 80.62 | 40 | 35 | 5 | 1443.50 | 934.83 | 6.0\% | 600 | 965 | 6.0\% |
| 8.75-3.229 | 4 | 11 | Ramp 1- Route 65 WB-NB Ramp Curve 1 | 04+00.60 | 82.67 | 40 | 40 | 0 | 758.61 | 954.93 | 8.0\% | 600 | 444 | 8.0\% |
| 8.75-3.229 | 4 | 11 | Ramp 1- Route 65 WB-NB Ramp Curve 2 | 15+13.52 |  | 40 | 40 | 0 | 758.04 | 954.93 | 8.0\% | 600 | 444 | 8.0\% |
| 9-CD 120427 | 34 | 62 | Ramp 2-Route 65 SB-WB Ramp Curve 1 | 201+19.92 | 82.28 | 45 | 40 | 5 | 248.90 | 1500.00 | 4.8\% | 675 | 1750 | 4.8\% |
| 9-CD 120427 | 35 | 63 | Ramp 2-Route 65 SB-WB Ramp Curve 2 | 214+69.64 | 82.39 | 45 | 40 | 5 | 1601.48 | 1200.00 | 5.6\% | 675 | 1390 | 5.6\% |
| 9-CD 120427 | 38 | 66 | Ramp 2-Route 65 SB-WB Ramp Curve 3 | 228+30.84 | 82.13 | 45 | 40 | 5 | 203.06 | 2000.00 | 4.2\% | 675 | 2080 | 4.2\% |
| 9-CD 120427 | 35 | 63 | Ramp 3- Route 65 NB-WB Flyover Ramp Curve 1 | $313+93.26$ | 82.47 | 45 | 35 | 10 | 1646.34 | 870.00 | 6.0\% | 675 | 1250 | 6.0\% |
| 8.5-3.203 | 5 | 9 | Ramp 4- Route 65 WB-SB Loop Curve 1 | 00+74.60 | 82.45 | 25 | 25 | 0 | 147.70 | 430.00 | 8.0\% | 375 | 134 | 8.0\% |
| 8.5-3.203 | 5 | 9 | Ramp 4- Route 65 WB-SB Loop Curve 2 |  |  | 25 | 25 | 0 | 869.40 | 215.00 | 8.0\% | 375 | 134 | 8.0\% |
| 8.5-3.203 | 5 | 9 | Ramp 4- Route 65 WB-SB Loop Curve 3 | 10+91.70 |  | 25 | 25 | 0 | 147.70 | 430.00 | 8.0\% | 375 | 134 | 8.0\% |
| 8.75-3.229 | 4 | 11 | Ramp 6- Route 65 SB-EB Loop Curve 1 | 00+94.12 |  | 25 | 25 | 0 | 185.32 | 430.00 | 8.0\% | 375 | 134 | 8.0\% |
| 8.75-3.229 | 4 | 11 | Ramp 6- Route 65 SB-EB Loop Curve 2 |  |  | 25 | 25 | 0 | 824.06 | 215.00 | 8.0\% | 375 | 134 | 8.0\% |
| 8.75-3.229 | 4 | 11 | Ramp 6- Route 65 SB-EB Loop Curve 3 | 11+03.50 | 82.45 | 25 | 25 | 0 | 185.32 | 430.00 | 8.0\% | 375 | 134 | 8.0\% |
| 9-CD 120427 | 35 | 63 | Ramp 7-Route 65 NB-EB Ramp Curve 1 | 701+31.94 |  | 45 | 40 | 5 | 262.97 | 1300.00 | 5.2\% | 675 | 1560 | 5.2\% |
| 9-CD 120427 | 35 | 63 | Ramp 7- Route 65 NB-EB Ramp Curve 2 | 708+99.90 |  | 45 | 40 | 5 | 831.53 | 1235.00 | 5.6\% | 675 | 1390 | 5.6\% |

J8I3044: I-44 FREEWAY HORIZONTAL GEOMETRICS

| Corridor Information |  |  |  |  |  |  |  |  | Horizontal Geometrics |  |  | Horizontal Design Criteria |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | Station |  |  |  |  |  | $\begin{aligned} & \stackrel{n}{\tilde{0}} \\ & \underset{\sim}{\pi} \\ & \hline \end{aligned}$ | 山 |  | . | 岃 |
| 9-CD 120427 | 35 | 63 | Ramp 7-Route 65 NB-EB Ramp Curve 3 | 716+11.88 | 82.62 | 45 | 35 | 10 | 606.07 | 1000.00 | 5.8\% | 675 | 1320 | 5.8\% |
| 9-CD 120427 | 39 | 67 | Ramp 7-Route 65 NB-EB Ramp Curve 4 | 728+61.34 | 82.90 | 45 | 45 | 0 | 203.49 | 2850.00 | 3.4\% | 675 | 2700 | 3.4\% |
| 8.5-3.203 | 5 | 9 | Ramp 8-Route 65 EB-SB Ramp Curve 1 | 04+00.70 | 82.35 | 40 | 40 | 0 | 758.80 | 955.00 | 8.0\% | 600 | 444 | 8.0\% |
| 8.5-3.203 | 4 | 8 | Ramp 8-Route 65 EB-SB Ramp Curve 2 | 15+76.00 | 82.49 | 40 | 40 | 0 | 758.80 | 955.00 | 8.0\% | 600 | 444 | 8.0\% |
| 9-CD 120427 | 35 | 63 | Ramp 9- Route 65 EB-NB Loop Curve 1 | 900+65.06 | 82.56 | 25 | 25 | 0 | 129.00 | 400.00 | 7.8\% | 375 | 164 | 7.8\% |
| 9-CD 120427 | 35 | 63 | Ramp 9- Route 65 EB-NB Loop Curve 2 | 903+78.44 |  | 25 | 25 | 0 | 357.99 | 200.00 | 7.8\% | 375 | 164 | 7.8\% |
| 9-CD 120427 | 35 | 63 | Ramp 9- Route 65 EB-NB Loop Curve 3 | 909+60.64 |  | 25 | 25 | 0 | 476.56 | 205.00 | 7.8\% | 375 | 164 | 7.8\% |
| 9-CD 120427 | 35 | 63 | Ramp 9- Route 65 EB-NB Loop Curve 4 | 910+24.05 |  | 25 | 25 | 0 | 120.14 | 410.00 | 7.8\% | 375 | 164 | 7.8\% |
| 12-CD 7155 | 5 | 10 | ML- Curve 3 (At Farm Road 199 Interchange) | 1444+67.29 | 84.80 RT | 70 | 55 | 15 | 2346.68 | 5729.65 | 2.8\% | 2100 | 7470 | 2.8\% |
| 12-CD 7155 | 4 | 9 | Ramp 1- Farm Road 199-WB 44 | 02+58.45 | 84.63 | 40 | 40 | 0 | 512.12 | 1538.64 | 5.0\% | 600 | 1310 | 5.0\% |
| 12-CD 7155 | 4 | 9 | Ramp 2- EB 44-Farm Road 199 | 02+60.33 | 84.60 | 40 | 40 | 0 | 520.11 | 4583.66 | 2.0\% | 600 | 3970 | 2.0\% |
| 12-CD 7155 | 5 | 10 | Ramp 3-WB 44-Farm Road 199 | 07+48.54 | 84.94 | 40 | 35 | 5 | 517.00 | 1272.95 | 5.0\% | 600 | 1310 | 5.0\% |
| 9.5-3.298 | 4 | 12 | Ramp 4- Farm Road 199-EB 44 | 03+82.86 | 84.85 | 25 | 25 | 0 | 299.29 | 763.93 | -2.0\% | 375 | 0 | -2.0\% |
| 12-CD 7155 | 5 | 10 | Ramp 4- Farm Road 199-EB 44 | 10+41.35 | 84.97 | 40 | 40 | 0 | 640.49 | 3104.23 | 3.0\% | 600 | 2510 | 3.0\% |
| 11-3.337 | 3 | 12 | ML- Curve 4 | 1592+62.15 | 87.60 RT | 70 | 70 | 0 | 1444.40 | 12732.43 | 0.0\% | 2100 | 12600 | 0.0\% |
| 11-3.337 | 3 | 12 | ML- Curve 5 (Near Route 125 Interchange) | 457+53.94 | 88.59 LT | 70 | 50 | 20 | 4123.03 | 5761.57 | 2.4\% | 2100 | 8810 | 2.4\% |
| 11-3.337 | 4 | 13 | Ramp 1- Route 125-WB 44 | 03+00.49 | 88.86 | 40 | 40 | 0 | 592.39 | 1432.39 | 6.0\% | 600 | 965 | 6.0\% |
| 11-3.337 | 4 | 13 | Ramp 2- EB 44-Route 125 | 03+06.79 | 88.77 | 40 | 40 | 0 | 604.44 | 1432.39 | 6.0\% | 600 | 965 | 6.0\% |
| 11-3.337 | 4 | 13 | Ramp 3- WB 44-Route 125 | 01+95.00 | 88.99 | 25 | 25 | 0 | 277.80 | 763.94 | 6.0\% | 375 | 332 | 6.0\% |
| 11-3.337 | 4 | 13 | Ramp 3-WB 44-Route 125 | 06+94.52 | 89.07 | 40 | 40 | 0 | 616.74 | 1145.16 | 7.0\% | 600 | 716 | 7.0\% |
| 11-3.337 | 4 | 13 | Ramp 4- Route 125-EB 44 | 05+71.72 | 89.07 | 40 | 40 | 0 | 749.45 | 1432.39 | 6.0\% | 600 | 965 | 6.0\% |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Indicates posted advisory speed |  |  | Does not meet design criteria |  |  |  |  |  |  |  |  |  |
|  |  | Indicates design speed listed on plans |  |  |  |  |  |  |  |  |  |  |  |  |


| J8I3044: I-44 FREEWAY VERTICAL GEOMETRICS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Corridor Information |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
|  |  |  | Location | Station |  | (HdW) paəds ןeuo!̣èədo | (HdW) әэиәдән!ด pәәds |  |  |  |  | $\checkmark$ |  |  |  |  |  | $\begin{aligned} & 0 \\ & \tilde{0} \\ & \frac{0}{0} \\ & \frac{0}{0} \end{aligned}$ |  |
| 1-3.176 | 4 | 33 | ML Curve 1 | 470+00.00 | 70 | 70 | 0 | C | 1200 | 1.93 | -0.94 | 418 | 2.87 | 246.90 | 210.00 | 417.83 | 730 | 949.56 | 0.00 |
| 1-3.176 | 5 | 34 | ML Curve 2 | 489+00.00 | 70 | 70 | 0 | S | 400 | -0.94 | 0.54 | 270 | 1.48 | 180.30 | 210.00 | 269.91 | 730 | N/A | 156.17 |
| 1-3.176 | 8 | 38 | Ramp A WB44-MM Curve A1 | 04+00.00 | 40 | 40 | 0 | S | 300 | -0.80 | 3.70 | 67 | 4.50 | 63.40 | 120.00 | 66.67 | 305 | N/A | 154.84 |
| 1-3.176 | 8 | 38 | Ramp A WB44-MM Curve A2 | 07+75.75 | 40 | 40 | 0 | C | 150 | 3.70 | 2.00 | 88 | 1.70 | 43.10 | 120.00 | 88.24 | 305 | 709.71 | 0.00 |
| 1-3.176 | 8 | 38 | Ramp B MM-WB44- Curve B1 | 01+23.30 | 40 | 40 | 0 | C | 200 | -2.00 | -4.15 | 93 | 2.15 | 43.10 | 120.00 | 93.02 | 305 | 601.86 | 0.00 |
| 1-3.176 | 8 | 38 | Ramp B MM-WB44- Curve B2 | 05+67.50 | 40 | 40 | 0 | S | 360 | -4.15 | -0.80 | 107 | 3.35 | 63.40 | 120.00 | 107.46 | 305 | N/A | 115.27 |
| 1-3.176 | 8 | 38 | Ramp C EB44-MM Curve C1 | 07+00.00 | 40 | 40 | 0 | S | 300 | 0.28 | 3.84 | 84 | 3.56 | 63.40 | 120.00 | 84.27 | 305 | N/A | 122.49 |
| 1-3.176 | 8 | 38 | Ramp C EB44-MM Curve C2 | 09+24.20 | 40 | 40 | 0 | C | 140 | 3.84 | 2.00 | 76 | 1.84 | 43.10 | 120.00 | 76.09 | 305 | 656.41 | 0.00 |
| 1-3.176 | 8 | 38 | Ramp D MM-EB44- Curve D1 | 01+12.53 | 40 | 40 | 0 | C | 200 | -2.42 | -3.98 | 128 | 1.56 | 43.10 | 120.00 | 128.21 | 305 | 791.67 | 0.00 |
| 1-3.176 | 8 | 38 | Ramp D MM-EB44- Curve D2 | 04+50.00 | 40 | 40 | 0 | S | 400 | -3.98 | 0.40 | 91 | 4.38 | 63.40 | 120.00 | 91.32 | 305 | N/A | 150.71 |
| 1-3.176 | 11 | 43 | ML Curve 3 | 595+00.00 | 70 | 70 | 0 | C | 1200 | 0.54 | -1.20 | 690 | 1.74 | 246.90 | 210.00 | 689.66 | 730 | 1220.11 | 0.00 |
| 1-3.176 | 13 | 45 | ML Curve 4 | 622+00.00 | 70 | 70 | 0 | S | 1000 | -1.20 | 0.80 | 500 | 2.00 | 180.30 | 210.00 | 500.00 | 730 | N/A | 210.75 |
| 1-3.176 | 18 | 57 | ML Curve 5 | 663+60.00 | 70 | 70 | 0 | C | 1000 | 0.80 | 0.32 | 2083 | 0.48 | 246.90 | 210.00 | 2083.33 | 730 | 2747.92 | 0.00 |
| 2.5-CD 120329 | 14 | 36 | Ramp 4A- WB 44-Rte 266 | 01+42.41 | 40 | 35 | 5 | S | 190 | -0.61 | 2.50 | 61 | 3.11 | 63.40 | 120.00 | 61.09 | 305 | N/A | 107.01 |
| 2.5-CD 120329 | 14 | 36 | Ramp 4- WB 44-Rte 266 | 13+17.49 | 40 | 40 | 0 | C | 170 | 0.74 | 0.24 | 340 | 0.50 | 43.10 | 120.00 | 340.00 | 305 | 2243.00 | 0.00 |
| 2.5-CD 120329 | 14 | 36 | Ramp 4- WB 44-Rte 266 | 15+49.31 | 40 | 40 | 0 | C | 200 | 0.24 | -2.50 | 73 | 2.74 | 43.10 | 120.00 | 72.99 | 305 | 493.80 | 0.00 |
| 2.5-CD 120329 | 14 | 36 | Ramp 5-Rte 266-WB 44 | 00+87.62 | 25 | 25 | 0 | C | 150 | 2.50 | -1.47 | 38 | 3.97 | 11.10 | 75.00 | 37.78 | 155 | 346.79 | 0.00 |
| 2.5-CD 120329 | 14 | 36 | Ramp 5-Rte 266-WB 44 | 02+50.00 | 25 | 25 | 0 | S | 100 | -1.47 | -0.16 | 76 | 1.31 | 25.50 | 75.00 | 76.34 | 155 | N/A | 17.61 |
| 3-3.174a | 3 | 8 | ML Curve 6 | 691+90.02 | 70 | 70 | 0 | S | 600 | 0.32 | 2.00 | 357 | 1.68 | 180.30 | 210.00 | 357.14 | 730 | N/A | 177.03 |
| 3-3.147a | 4 | 9 | ML Curve 7 | 704+84.70 | 70 | 70 | 0 | C | 1100 | 2.00 | -2.00 | 275 | 4.00 | 246.90 | 210.00 | 275.00 | 730 | 770.36 | 0.00 |
| 3-3.147a | 4 | 9 | ML Curve 8 | 714+88.10 | 70 | 70 | 0 | S | 600 | -2.00 | -0.30 | 353 | 1.70 | 180.30 | 210.00 | 352.94 | 730 | N/A | 179.14 |
| 4-3.174 | 5 | 15 | ML Curve 9 | 752+40.00 | 70 | 70 | 0 | C | 300 | -0.30 | -0.60 | 1000 | 0.30 | 246.90 | 210.00 | 1000.00 | 730 | 3746.67 | 0.00 |
| 5-3.174B | 3 | 14 | ML Curve 10 | 786+85.60 | 70 | 70 | 0 | S | 1200 | -0.60 | 3.00 | 333 | 3.60 | 180.30 | 210.00 | 333.33 | 730 | N/A | 379.35 |
| 5-3.174B | 4 | 15 | Ramp 4- Rte 744-WB 44 Curve 4A | 01+00.00 | 25 | 25 | 0 | S | 150 | -0.30 | 1.65 | 77 | 1.95 | 25.50 | 75.00 | 76.92 | 155 | N/A | 26.21 |
| 5-3.174B | 4 | 15 | Ramp 4- Rte 744-WB 44 Curve 4B | 09+25.00 | 40 | 40 | 0 | C | 300 | 1.65 | -0.90 | 118 | 2.55 | 43.10 | 120.00 | 117.65 | 305 | 573.14 | 0.00 |
| 5-3.174B | 5 | 16 | ML Curve 11 | 803+89.00 | 70 | 65 | 5 | C | 1400 | 3.00 | -3.00 | 233 | 6.00 | 246.90 | 210.00 | 233.33 | 730 | 709.60 | 0.00 |
| 6-3.178 | 5 | 35 | ML Curve 12 | 826+00.00 | 70 | 70 | 0 | S | 600 | -3.00 | -0.70 | 261 | 2.30 | 180.30 | 210.00 | 261.21 | 730 | N/A | 242.05 |
| 5.5-3.247 | 28 | 45 | Ramp 1 Route 160-WB 44 Curve 1A | 04+22.40 | 40 | 40 | 0 | S | 510 | -4.70 | 2.00 | 76 | 6.70 | 63.40 | 120.00 | 76.12 | 305 | N/A | 230.54 |
| 5.5-3.247 | 28 | 45 | Ramp 2 EB 44-Route 160 Curve 2A | 03+94.20 | 40 | 25 | 15 | S | 420 | -5.50 | 8.00 | 31 | \#\#\#\# | 63.40 | 120.00 | 31.11 | 305 | N/A | 464.52 |
| 5.5-3.247 | 28 | 45 | Ramp 3 WB44-Route 160 Curve 3A | 10+72.13 | 40 | 40 | 0 | C | 500 | 2.00 | -5.00 | 71 | 7.00 | 43.10 | 120.00 | 71.43 | 305 | 392.61 | 0.00 |
| 5.5-3.247 | 28 | 45 | Ramp 3 WB44-Route 160 Curve 3B | 07+86.10 | 40 | 40 | 0 | S | 400 | -5.00 | 0.33 | 75 | 5.33 | 63.40 | 120.00 | 75.12 | 305 | N/A | 183.23 |


| J8I3044: I-44 FREEWAY VERTICAL GEOMETRICS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Corridor Information |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
|  |  |  | Location | Station |  | (HdW) paəds ןeuo!̣èado | (HdW) әэиəдəย!の pəəds |  |  |  |  | $\underline{~}$ |  |  |  |  |  | $\begin{aligned} & 0 \\ & \tilde{\sim} \\ & \frac{0}{0} \\ & \frac{0}{0} \end{aligned}$ |  |
| 5.5-3.247 | 28 | 45 | Ramp 4 Route 160-EB 44 Curve 4A | 10+54.27 | 25 | 25 | 0 | C | 260 | -1.55 | -6.00 | 58 | 4.45 | 11.10 | 75.00 | 58.43 | 155 | 372.47 | 0.00 |
| 5.5-3.247 | 28 | 45 | Ramp 4 Route 160-EB 44 Curve 4B | 07+21.70 | 40 | 35 | 5 | S | 375 | -6.00 | 0.00 | 63 | 6.00 | 63.40 | 120.00 | 62.50 | 305 | N/A | 206.45 |
| 6-3.178 | 13 | 43 | ML Curve 13 | 875+00.00 | 70 | 70 | 0 | C | 400 | -0.70 | -1.00 | 1347 | 0.30 | 246.90 | 210.00 | 1346.80 | 730 | 3833.00 | 0.00 |
| 6-3.178 | 15 | 44 | ML Curve 14 | 1022+00.00 | 60 | 60 | 0 | S | 400 | -1.00 | 0.30 | 308 | 1.30 | 135.70 | 180.00 | 307.69 | 570 | N/A | 100.65 |
| 6-3.178 | 18 | 47 | ML Curve 15 | 1040+00.00 | 60 | 60 | 0 | S | 300 | 0.30 | 0.71 | 728 | 0.41 | 135.70 | 180.00 | 728.16 | 570 | N/A | 31.90 |
| 6-3.178 | 22 | 51 | ML Curve 16 | 1058+00.00 | 60 | 60 | 0 | C | 300 | 0.71 | 0.34 | 806 | 0.37 | 150.60 | 180.00 | 806.45 | 570 | 3050.54 | 0.00 |
| 6-3.178 | 25 | 54 | Ramp A EB 44-Route 13 Curve A1 | 03+50.00 | 40 | 40 | 0 | S | 300 | 0.44 | 4.50 | 74 | 4.06 | 63.40 | 120.00 | 73.89 | 305 | N/A | 139.70 |
| 6-3.178 | 25 | 54 | Ramp A EB 44-Route 13 Curve A2 | 08+00.00 | 40 | 40 | 0 | C | 180 | 4.50 | 1.00 | 51 | 3.50 | 43.10 | 120.00 | 51.43 | 305 | 398.29 | 0.00 |
| 6-3.178 | 25 | 54 | Ramp B Route 13-WB 44 Curve B1 | 01+14.70 | 40 | 40 | 0 | C | 150 | -2.16 | -4.26 | 72 | 2.10 | 43.10 | 120.00 | 71.60 | 305 | 590.04 | 0.00 |
| 6-3.178 | 25 | 54 | Ramp B Route 13-WB 44 Curve B2 | 05+79.60 | 40 | 40 | 0 | S | 400 | -4.26 | 0.42 | 86 | 4.68 | 63.40 | 120.00 | 85.56 | 305 | N/A | 160.86 |
| 6-3.178 | 25 | 54 | Ramp C WB 44-Route 13 Curve C1 | 03+60.00 | 40 | 40 | 0 | S | 350 | 0.00 | 4.50 | 78 | 4.50 | 63.40 | 120.00 | 77.78 | 305 | N/A | 154.84 |
| 6-3.178 | 25 | 54 | Ramp C WB 44-Route 13 Curve C2 | 07+01.40 | 40 | 40 | 0 | C | 180 | 4.50 | 1.00 | 51 | 3.50 | 43.10 | 120.00 | 51.43 | 305 | 398.29 | 0.00 |
| 6-3.178 | 25 | 54 | Ramp D Route 13-EB 44 Curve D1 | 01+20.00 | 40 | 40 | 0 | C | 150 | -2.00 | -5.16 | 47 | 3.16 | 43.10 | 120.00 | 47.47 | 305 | 416.46 | 0.00 |
| 6-3.178 | 25 | 54 | Ramp D Route 13-EB 44 Curve D2 | 02+76.00 | 40 | 15 | 25 | S | 50 | -5.16 | -4.88 | 179 | 0.28 | 63.40 | 120.00 | 178.57 | 305 | N/A | 9.63 |
| 6-3.178 | 25 | 54 | Ramp D Route 13-EB 44 Curve D3 | 05+00.00 | 40 | 40 | 0 | S | 400 | -4.88 | 1.00 | 68 | 5.88 | 63.40 | 120.00 | 68.03 | 305 | N/A | 202.32 |
| 6-3.178 | 24 | 53 | ML Curve 17 | 1082+85.60 | 60 | 60 | 0 | S | 400 | 0.34 | 1.52 | 339 | 1.18 | 135.70 | 180.00 | 338.98 | 570 | N/A | 91.35 |
| 6-3.178 | 34 | 63 | ML Curve 18 | $1111+50.00$ | 60 | 60 | 0 | C | 750 | 1.52 | -1.52 | 247 | 3.04 | 150.60 | 180.00 | 246.71 | 570 | 729.66 | 0.00 |
| 6-3.178 | 38 | 70 | ML Curve 19 | $1134+50.00$ | 60 | 60 | 0 | S | 500 | -1.52 | 1.31 | 176 | 2.83 | 135.70 | 180.00 | 176.43 | 570 | N/A | 219.41 |
| 6-3.178 | 40 | 72 | ML Curve 20 | $1153+00.00$ | 60 | 60 | 0 | C | 400 | 1.31 | 1.00 | 1274 | 0.31 | 150.60 | 180.00 | 1273.89 | 570 | 3636.31 | 0.00 |
| 6-3.178 | 43 | 75 | ML Curve 21 | 1180+23.00 | 60 | 60 | 0 | C | 800 | 1.00 | -0.40 | 571 | 1.40 | 150.60 | 180.00 | 571.43 | 570 | 1170.71 | 0.00 |
| 7.5-CD 120808 | 22 | 68 | Ramp 1 Missouri H-WB 44 Curve 1A | 03+16.67 | 40 | 40 | 0 | C | 300 | -1.00 | -4.29 | 91 | 3.29 | 43.10 | 120.00 | 91.19 | 305 | 477.96 | 0.00 |
| 7.5-CD 120808 | 22 | 68 | Ramp 1 Missouri H-WB 44 Curve 1B | 06+32.74 | 40 | 40 | 0 | S | 300 | -4.29 | -2.79 | 200 | 1.50 | 63.40 | 120.00 | 200.00 | 305 | N/A | 51.61 |
| 7.5-CD 120808 | 22 | 68 | Ramp 1 Missouri H-WB 44 Curve 1C | 09+32.74 | 40 | 40 | 0 | S | 300 | -2.79 | 0.23 | 99 | 3.02 | 63.40 | 120.00 | 99.34 | 305 | N/A | 103.91 |
| 7.5-CD 120808 | 24 | 70 | Ramp 3 EB 44-Missouri H Curve 3A | 06+78.33 | 40 | 30 | 10 | S | 100 | 1.51 | 2.82 | 76 | 1.31 | 63.40 | 120.00 | 76.34 | 305 | N/A | 45.08 |
| 7.5-CD 120808 | 24 | 70 | Ramp 3 EB 44-Missouri H Curve 3B | 08+78.33 | 40 | 40 | 0 | S | 300 | 2.82 | 4.28 | 205 | 1.46 | 63.40 | 120.00 | 205.48 | 305 | N/A | 50.24 |
| 7.5-CD 120808 | 24 | 70 | Ramp 3 EB 44-Missouri H Curve 3B | 12+21.38 | 40 | 40 | 0 | C | 300 | 4.28 | 1.00 | 91 | 3.28 | 43.10 | 120.00 | 91.46 | 305 | 478.96 | 0.00 |
| 7.5-CD 120808 | 26 | 72 | Ramp 6 WB 44-Missouri H Curve 6A | 08+78.46 | 40 | 40 | 0 | S | 300 | 2.07 | 5.37 | 91 | 3.30 | 63.40 | 120.00 | 90.91 | 305 | N/A | 113.55 |
| 7.5-CD 120808 | 26 | 72 | Ramp 6 WB 44-Missouri H Curve 6B | 12+21.48 | 40 | 40 | 0 | C | 300 | 5.37 | 2.00 | 89 | 3.37 | 43.10 | 120.00 | 89.02 | 305 | 470.18 | 0.00 |
| 7.5-CD 120808 | 28 | 74 | Ramp 8 Missouri H-EB 44 Curve 8A | 06+41.94 | 40 | 40 | 0 | C | 300 | -1.00 | -6.04 | 60 | 5.04 | 43.10 | 120.00 | 59.52 | 305 | 364.09 | 0.00 |
| 7.5-CD 120808 | 28 | 74 | Ramp 8 Missouri H-EB 44 Curve 8B | 09+46.69 | 40 | 35 | 5 | S | 250 | -6.04 | -1.92 | 61 | 4.12 | 63.40 | 120.00 | 60.68 | 305 | N/A | 141.76 |
| 6-3.178 | 46 | 83 | ML Curve 22 | 1196+02.70 | 60 | 60 | 0 | S | 300 | -0.40 | 0.30 | 429 | 0.70 | 135.70 | 180.00 | 428.57 | 570 | N/A | 54.19 |


| J8I3044: I-44 FREEWAY VERTICAL GEOMETRICS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Corridor Information |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
|  |  |  | Location | Station |  | (HdW) paəds ןeuo!̣èado | (HdW) әэиəдəみ!の pəəds |  |  |  |  | $\underline{~}$ |  |  |  |  |  | $\begin{aligned} & 0 \\ & \tilde{\sim} \\ & \frac{0}{0} \\ & \frac{0}{0} \end{aligned}$ |  |
| 8.75-3.229 | 6 | 13 | Ramp 1-Route 65 WB-NB Ramp Curve 1 | 00+85.00 | 40 | 40 | 0 | C | 170 | -0.80 | -2.20 | 121 | 1.40 | 43.10 | 120.00 | 121.43 | 305 | 855.71 | 0.00 |
| 8.75-3.229 | 6 | 13 | Ramp 1-Route 65 WB-NB Ramp Curve 2 | 04+78.00 | 40 | 40 | 0 | S | 400 | -2.20 | 0.80 | 133 | 3.00 | 63.40 | 120.00 | 133.33 | 305 | N/A | 103.23 |
| 8.75-3.229 | 6 | 13 | Ramp 1-Route 65 WB-NB Ramp Curve 3 | 16+00.00 | 40 | 40 | 0 | C | 300 | 0.80 | 0.00 | 375 | 0.80 | 43.10 | 120.00 | 375.00 | 305 | 1498.75 | 0.00 |
| 8.75-3.229 | 6 | 13 | Ramp 1-Route 65 WB-NB Ramp Curve 4 | 18+00.00 | 40 | 30 | 10 | C | 100 | 0.00 | -0.40 | 250 | 0.40 | 43.10 | 120.00 | 250.00 | 305 | 2747.50 | 0.00 |
| 9-CD 120427 | 23 | 51 | Ramp 2- Route 65 SB-WB Ramp Curve 1 | $203+60.00$ | 45 | 40 | 5 | S | 260 | 0.27 | 4.59 | 60 | 4.32 | 78.10 | 135.00 | 60.19 | 360 | N/A | 188.13 |
| 9-CD 120427 | 23 | 51 | Ramp 2- Route 65 SB-WB Ramp Curve 2 | $211+30.00$ | 45 | 45 | 0 | C | 1010 | 4.59 | -3.20 | 130 | 7.79 | 60.10 | 135.00 | 129.65 | 360 | 528.95 | 0.00 |
| 9-CD 120427 | 24 | 52 | Ramp 2-Route 65 SB-WB Ramp Curve 3 | 221+50.00 | 45 | 40 | 5 | S | 300 | -3.20 | 1.50 | 64 | 4.70 | 78.10 | 135.00 | 63.83 | 360 | N/A | 204.68 |
| 9-CD 120427 | 24 | 52 | Ramp 2- Route 65 SB-WB Ramp Curve 4 | $226+40.00$ | 45 | 45 | 0 | C | 200 | 1.50 | -0.55 | 98 | 2.05 | 60.10 | 135.00 | 97.56 | 360 | 626.34 | 0.00 |
| 9-CD 120427 | 24 | 52 | Ramp 2-Route 65 SB-WB Ramp Curve 5 | 227+90.00 | 45 | 30 | 15 | S | 100 | -0.55 | 0.62 | 85 | 1.17 | 78.10 | 135.00 | 85.47 | 360 | N/A | 50.95 |
| 9-CD 120427 | 25 | 53 | Ramp 3-Route 65 NB-WB Flyover Ramp Curve 1 | $302+80.00$ | 45 | 40 | 5 | S | 120 | 3.86 | 4.47 | 197 | 0.61 | 78.10 | 135.00 | 196.72 | 360 | N/A | 26.56 |
| 9-CD 120427 | 25 | 53 | Ramp 3-Route 65 NB-WB Flyover Ramp Curve 2 | $309+20.00$ | 45 | 45 | 0 | C | 800 | 4.47 | -3.89 | 96 | 8.36 | 60.10 | 135.00 | 95.69 | 360 | 454.43 | 0.00 |
| 8.5-3.203 | 7 | 11 | Ramp 4- Route 65 WB-SB Loop Curve 1 | 05+53.60 | 25 | 25 | 0 | S | 400 | -2.50 | 5.00 | 53 | 7.50 | 25.50 | 75.00 | 53.33 | 155 | N/A | 100.81 |
| 8.5-3.203 | 7 | 11 | Ramp 4- Route 65 WB-SB Loop Curve 2 | 10+00.00 | 25 | 25 | 0 | C | 100 | 5.00 | 3.20 | 56 | 1.80 | 11.10 | 75.00 | 55.56 | 155 | 649.44 | 0.00 |
| 8.75-3.229 | 6 | 13 | Ramp 6- Route 65 SB-EB Loop Curve 1 | 00+40.00 | 25 | 25 | 0 | C | 80 | -1.00 | -2.30 | 62 | 1.30 | 11.10 | 75.00 | 61.54 | 155 | 870.00 | 0.00 |
| 8.75-3.229 | 6 | 13 | Ramp 6- Route 65 SB-EB Loop Curve 2 | 03+00.00 | 25 | 25 | 0 | S | 300 | -2.30 | -0.80 | 200 | 1.50 | 25.50 | 75.00 | 200.00 | 155 | N/A | 20.16 |
| 8.75-3.229 | 6 | 13 | Ramp 6- Route 65 SB-EB Loop Curve 3 | 06+00.00 | 25 | 25 | 0 | C | 300 | -0.80 | -2.74 | 155 | 1.94 | 11.10 | 75.00 | 154.64 | 155 | 706.19 | 0.00 |
| 8.75-3.229 | 6 | 13 | Ramp 6- Route 65 SB-EB Loop Curve 4 | 09+37.40 | 25 | 25 | 0 | S | 300 | -2.74 | 1.00 | 80 | 3.74 | 25.50 | 75.00 | 80.21 | 155 | N/A | 50.27 |
| 8.75-3.229 | 6 | 13 | Ramp 6- Route 65 SB-EB Loop Curve 5 | 11+59.70 | 25 | 20 | 5 | C | 70 | 1.00 | -0.70 | 41 | 1.70 | 11.10 | 75.00 | 41.18 | 155 | 669.71 | 0.00 |
| 9-CD 120427 | 29 | 57 | Ramp 7- Route 65 NB-EB Ramp Curve 1 | 704+20.00 | 45 | 35 | 10 | S | 340 | -1.58 | 4.45 | 56 | 6.03 | 78.10 | 135.00 | 56.38 | 360 | N/A | 262.60 |
| 9-CD 120427 | 29 | 57 | Ramp 7- Route 65 NB-EB Ramp Curve 2 | $709+30.00$ | 45 | 45 | 0 | C | 600 | 4.45 | -2.60 | 85 | 7.05 | 60.10 | 135.00 | 85.11 | 360 | 428.56 | 0.00 |
| 9-CD 120427 | 30 | 58 | Ramp 7- Route 65 NB-EB Ramp Curve 3 | 716+50.00 | 45 | 45 | 0 | S | 290 | -2.60 | -0.77 | 158 | 1.83 | 78.10 | 135.00 | 158.47 | 360 | N/A | 79.69 |
| 9-CD 120427 | 30 | 58 | Ramp 7- Route 65 NB-EB Ramp Curve 4 | 726+00.00 | 45 | 45 | 0 | S | 220 | -0.77 | 0.99 | 125 | 1.76 | 78.10 | 135.00 | 125.00 | 360 | N/A | 76.65 |
| 8.5-3.203 | 8 | 12 | Ramp 8-Route 65 EB-SB Ramp Curve 1 | 03+30.00 | 45 | 45 | 0 | S | 300 | -2.00 | 0.85 | 105 | 2.85 | 78.10 | 135.00 | 105.26 | 360 | N/A | 124.11 |
| 8.5-3.203 | 8 | 12 | Ramp 8-Route 65 EB-SB Ramp Curve 2 | $17+45.00$ | 45 | 30 | 15 | S | 100 | 0.85 | 1.63 | 128 | 0.78 | 78.10 | 135.00 | 128.21 | 360 | N/A | 33.97 |
| 9-CD 120427 | 31 | 59 | Ramp 9- Route 65 EB-NB Loop Curve 1 | 902+60.00 | 25 | 25 | 0 | S | 250 | -1.37 | 2.98 | 57 | 4.35 | 25.50 | 75.00 | 57.47 | 155 | N/A | 58.47 |
| 8-3.157 | 9 | 13 | ML Curve 23 | 1238+00.00 | 60 | 60 | 0 | S | 400 | 0.30 | 0.80 | 794 | 0.50 | 135.70 | 180.00 | 794.44 | 570 | N/A | 38.98 |
| 8-3.157 | 11 | 15 | ML Curve 24 | 1264+00.00 | 60 | 60 | 0 | C | 400 | 0.80 | -0.72 | 263 | 1.52 | 150.60 | 180.00 | 263.07 | 570 | 909.63 | 0.00 |
| 8-3.157 | 12 | 16 | ML Curve 25 | 1286+00.00 | 60 | 60 | 0 | S | 400 | -0.72 | 0.72 | 278 | 1.44 | 135.70 | 180.00 | 278.36 | 570 | N/A | 111.25 |
| 8-3.157 | 12 | 16 | ML Curve 26 | 1306+00.00 | 60 | 60 | 0 | C | 400 | 0.72 | -0.80 | 263 | 1.52 | 150.60 | 180.00 | 263.16 | 570 | 909.87 | 0.00 |
| 8-3.157 | 13 | 17 | ML Curve 27 | 1326+00.00 | 60 | 60 | 0 | S | 800 | -0.80 | 0.80 | 500 | 1.60 | 135.70 | 180.00 | 500.00 | 570 | N/A | 123.87 |
| 9.5-3.298 | 7 | 16 | Ramp 1 WB 44-Farm Road 199 Curve 1A | 04+68.00 | 40 | 40 | 0 | S | 300 | 0.00 | 4.00 | 75 | 4.00 | 63.40 | 120.00 | 75.00 | 305 | N/A | 137.63 |


| J8I3044: I-44 FREEWAY VERTICAL GEOMETRICS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Corridor Information |  |  |  |  |  |  |  | Vertical Geometrics |  |  |  |  | Vertical Design Criteria |  |  |  |  |  |  |
|  |  |  | Location | Station |  | (HdW) pəəds ןeuo!̣eлədo | (HdW) әכиәдәц!ด pəәds |  |  |  | $\begin{aligned} & \text { oo } \\ & \stackrel{0}{0} \\ & \frac{0}{0} \\ & \stackrel{H}{x} \\ & \hline \end{aligned}$ | $\underline{\sim}$ |  |  |  |  |  | $$ |  |
| 9.5-3.298 | 7 | 16 | Ramp 1 WB 44-Farm Road 199 Curve 1B | 09+59.96 | 40 | 40 | 0 | C | 300 | 4.00 | 1.01 | 100 | 2.99 | 43.10 | 120.00 | 100.33 | 305 | 510.87 | 0.00 |
| 9.5-3.298 | 7 | 16 | Ramp 2 EB 44-Farm Road 199 Curve 2A | 05+24.09 | 40 | 35 | 5 | S | 300 | 0.24 | 5.00 | 63 | 4.76 | 63.40 | 120.00 | 63.03 | 305 | N/A | 163.78 |
| 9.5-3.298 | 7 | 16 | Ramp 2 EB 44-Farm Road 199 Curve 2B | 09+90.08 | 40 | 40 | 0 | C | 300 | 5.00 | 1.00 | 75 | 4.00 | 43.10 | 120.00 | 75.00 | 305 | 419.75 | 0.00 |
| 9.5-3.298 | 7 | 16 | Ramp 3 WB 44-Farm Road 199 Curve 3A | 01+64.00 | 40 | 40 | 0 | C | 300 | -1.67 | -3.84 | 138 | 2.17 | 43.10 | 120.00 | 138.25 | 305 | 647.24 | 0.00 |
| 9.5-3.298 | 7 | 16 | Ramp 3 WB 44-Farm Road 199 Curve 3B | 05+84.65 | 40 | 40 | 0 | S | 300 | -3.84 | 0.72 | 66 | 4.56 | 63.40 | 120.00 | 65.83 | 305 | N/A | 156.80 |
| 9.5-3.298 | 7 | 16 | Ramp 4 EB 44-Farm Road 199 Curve 4A | 02+57.79 | 40 | 40 | 0 | C | 300 | -1.00 | -2.50 | 200 | 1.50 | 43.10 | 120.00 | 200.00 | 305 | 869.33 | 0.00 |
| 9.5-3.298 | 7 | 16 | Ramp 4 EB 44-Farm Road 199 Curve 4B | 09+92.19 | 40 | 40 | 0 | S | 300 | -2.50 | 0.94 | 87 | 3.44 | 63.40 | 120.00 | 87.21 | 305 | N/A | 118.37 |
| 8-3.157 | 18 | 22 | ML Curve 28 | 1388+00.00 | 70 | 70 | 0 | C | 300 | 0.72 | 0.64 | 3750 | 0.08 | 246.90 | 210.00 | 3750.00 | 730 | 13637.50 | 0.00 |
| 8-3.157 | 19 | 23 | ML Curve 29 | 1410+00.00 | 70 | 70 | 0 | S | 400 | 0.64 | 1.66 | 392 | 1.02 | 180.30 | 210.00 | 392.16 | 730 | N/A | 107.48 |
| 12-CD 7155 | 4 | 9 | ML Curve 30 | 1431+00.00 | 70 | 70 | 0 | C | 450 | 1.70 | 0.30 | 321 | 1.40 | 246.90 | 210.00 | 321.43 | 730 | 995.71 | 0.00 |
| 11-3.337 | 10 | 19 | Ramp 1 Route 125-WB 44 Curve 1A | 01+75.00 | 40 | 35 | 5 | S | 350 | -1.32 | 4.47 | 60 | 5.79 | 63.40 | 120.00 | 60.41 | 305 | N/A | 199.36 |
| 11-3.337 | 10 | 19 | Ramp 1 Route 125-WB 44 Curve 1B | 06+93.75 | 40 | 40 | 0 | C | 400 | 4.47 | 1.56 | 137 | 2.91 | 43.10 | 120.00 | 137.46 | 305 | 570.79 | 0.00 |
| 11-3.337 | 10 | 19 | Ramp 2 EB 44-Route 125 Curve 2A | 06+00.00 | 40 | 40 | 0 | S | 650 | -1.63 | 4.96 | 99 | 6.59 | 63.40 | 120.00 | 98.63 | 305 | N/A | 226.75 |
| 11-3.337 | 10 | 19 | Ramp 2 EB 44-Route 125 Curve 2B | $11+48.18$ | 40 | 40 | 0 | C | 400 | 4.96 | 1.56 | 118 | 3.40 | 43.10 | 120.00 | 117.65 | 305 | 517.35 | 0.00 |
| 11-3.337 | 10 | 19 | Ramp 3 WB 44-Route 125 Curve 3A | 07+08.66 | 40 | 40 | 0 | S | 350 | -1.56 | -0.16 | 251 | 1.40 | 63.40 | 120.00 | 250.72 | 305 | N/A | 48.03 |
| 11-3.337 | 10 | 19 | Ramp 4 Route 125-EB 44 Curve 4A | 02+26.60 | 40 | 40 | 0 | C | 200 | -1.56 | -2.44 | 227 | 0.88 | 43.10 | 120.00 | 227.27 | 305 | 1326.14 | 0.00 |
| 11-3.337 | 10 | 19 | Ramp 4 Route 125-EB 44 Curve 4B | 05+79.35 | 40 | 40 | 0 | S | 400 | -2.44 | 0.13 | 155 | 2.57 | 63.40 | 120.00 | 155.40 | 305 | N/A | 88.57 |
| 11-3.337 | 9 | 18 | ML Curve 31 | 454+50.00 | 70 | 70 | 0 | C | 1200 | 0.90 | -1.50 | 500 | 2.40 | 246.90 | 210.00 | 500.00 | 730 | 1038.75 | 0.00 |
| 11-3.337 | 9 | 18 | ML Curve 32 | $468+23.00$ | 70 | 70 | 0 | S | 600 | -1.50 | 1.62 | 192 | 3.12 | 180.30 | 210.00 | 192.31 | 730 | N/A | 328.77 |
| 11-3.337 | 9 | 18 | ML Curve 33 | 480+73.00 | 70 | 70 | 0 | C | 1800 | 1.62 | -0.56 | 826 | 2.18 | 246.90 | 210.00 | 825.69 | 730 | 1334.85 | 0.00 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | Does not meet design criteria |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

J8I3044: I-44 FREEWAY ACCELERATION \& DECELERATION RAMP LENGTHS

| Corridor Information |  |  |  |  |  |  | Ramp Geometrics |  |  |  |  | Ramp Criteria |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location |  |  |  |  |  |  |  | do <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 10 <br> 1 |  | $\begin{aligned} & \bar{\vdots} \\ & \stackrel{U}{U} \\ & \stackrel{\rightharpoonup}{1} \\ & \stackrel{\rightharpoonup}{0} \\ & \frac{\pi}{0} \end{aligned}$ |  |
| 1-3.176 | 8 | 38 | Ramp A- WB 44-County Road MM | 70 | 20 | D | T | 14.30 | 1273.57 | 0.0\% | -0.54\% | 570 | 1.00 | 570 |
| 1-3.176 | 8 | 38 | Ramp B- County Road MM-WB 44 | 70 | 40 | A | P | 400.00 | 1273.57 | 0.0\% | -0.54\% | 1000 | 1.00 | 1000 |
| 1-3.176 | 8 | 38 | Ramp C- EB 44-County Road MM | 70 | 20 | D | T | 75.90 | 1432.69 | 0.0\% | 0.54\% | 570 | 1.00 | 570 |
| 1-3.176 | 8 | 38 | Ramp D- County Road MM-EB 44 | 70 | 40 | A | T | 400.00 | 1146.28 | 0.0\% | 0.54\% | 1000 | 1.00 | 1000 |
| 1-3.176 | 22 | 65 | Ramp 1- EB 44-Route 266 | 70 | 30 | D | P | 300.00 | 955.37 | 6.0\% | 0.80\% | 520 | 1.00 | 520 |
| 1-3.176 | 22 | 65 | Ramp 2- Loop Ramp-WB 44 | 70 | 15 | A | P | 1275.00 | 465.10 | 6.0\% | -0.32\% | 1560 | 1.00 | 1560 |
| 1-3.176 | 22 | 65 | Ramp 3- WB 44-Route 266 | 70 | 35 | D | P | 300.00 | 716.78 | 6.0\% | -0.80\% | 490 | 1.00 | 490 |
| 1-3.176 | 22 | 65 | Ramp 4- Route 266-EB 44 | 70 | 35 | A | P | 400.00 | 716.78 | 6.0\% | 0.32\% | 1230 | 1.00 | 1230 |
| 5-3.174B | 4 | 15 | Ramp 4- Rte 744-WB 44 Curve 4A | 70 | 40 | A | P | 400.00 | 716.78 | 6.0\% | 3.00\% | 1000 | 1.00 | 1000 |
| 5.5-3.247 | 27 | 34,4 | Ramp 1- Route 160- WB 44 | 70 | 40 | A | P | 400.00 | 954.93 | 8.0\% | -2.50\% | 1000 | 1.00 | 1000 |
| 5.5-3.247 | 27 | 34,4 | Ramp 2- EB 44- Route 160 | 70 | 25 | D | P | 450.00 | 954.93 | 8.0\% | -2.50\% | 550 | 1.00 | 550 |
| Current Project |  |  | Ramp 3- WB 44-Route 160 | 70 | 40 | D | P | 809.17 | 1909.86 | 5.0\% | 0.30\% | 440 | 1.00 | 440 |
| Current Project |  |  | Ramp 4- Route 160-EB 44 | 70 | 35 | A | P | 1031.16 | 1146.56 | 8.0\% | 0.30\% | 1230 | 1.00 | 1230 |
| Current Project |  |  | Ramp A- EB 44- Route 13 | 60 | 35 | D | T | 576.82 | 955.37 | 6.0\% | 0.34\% | 405 | 1.00 | 405 |
| Current Project |  |  | Ramp B- Route 13- WB 44 | 60 | 35 | A | T | 771.16 | 955.37 | 6.0\% | 0.34\% | 800 | 1.00 | 800 |
| Current Project |  |  | Ramp C- WB 44- Route 13 | 60 | 35 | D | P | 1253.28 | 955.37 | 6.0\% | 0.34\% | 405 | 1.00 | 405 |
| Current Project |  |  | Ramp D- Route 13- EB 44 | 60 | 35 | A | P | 1170.82 | 955.37 | 6.0\% | 0.34\% | 800 | 1.00 | 800 |
| Current Project |  |  | Ramp 1- Missouri H- WB 44 | 60 | 30 | A | P | 895.89 | 690.00 | 0.0\% | 0.35\% | 910 | 1.00 | 910 |
| 7.5-CD 120808 | 23 | 69 | Ramp 3- EB 44- Missouri H | 60 | 30 | D | P | 430.00 | 689.77 | 0.0\% | 0.30\% | 430 | 1.00 | 430 |
| Current Project |  |  | Ramp 6- WB 44- Missouri H | 60 | 30 | D | T | 589.51 | 467.72 | 0.0\% | 0.30\% | 430 | 1.00 | 430 |
| Current Project |  |  | Ramp 8- Missouri H- EB 44 | 70 | 35 | A | P | 764.77 | 934.83 | 0.0\% | 0.55\% | 1230 | 1.00 | 1230 |
| 8.75-3.229 | 34 | 62 | Ramp 1-WB-NB Route 65 | 70 | 40 | D | P | 365.00 | 954.93 | 8.0\% | -0.80\% | 440 | 1.00 | 440 |
| 9-CD 120427 | 34 | 62 | Ramp 2- SB-WB 44 | 70 | 30 | A | P | 350.00 | 2000.00 | 4.2\% | 0.62\% | 1350 | 1.00 | 1350 |

J8I3044: I-44 FREEWAY ACCELERATION \& DECELERATION RAMP LENGTHS

| Corridor Information |  |  |  |  |  |  | Ramp Geometrics |  |  |  |  | Ramp Criteria |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Location | ML Speed (MPH) |  |  |  |  |  | Ramp Superelevation |  | $\stackrel{5}{5}$ $\stackrel{0}{4}$ $\frac{0}{0}$ $\frac{0}{0}$ 0 $\frac{\pi}{4}$ $\frac{\pi}{4}$ |  |  |
| 9-CD 120427 | 70 | 55 | Ramp 3-EB-SB Flyover Ramp | 70 | 70 | A | NA | NA | 870.00 | 6.0\% | -3.89\% | \#N/A | 0.60 | \#N/A |
| 8.5-3.203 | 70 | 55 | Ramp 4- WB-SB Route 65 Loop Ramp Decel | 70 | 25 | D | P | 560.00 | 430.00 | 8.0\% | -2.50\% | 550 | 1.00 | 550 |
| 8.5-3.203 | 70 | 55 | Ramp 4- WB-SB Route 65 Loop Ramp Accel | 70 | 25 | A | P | 560.00 | 430.00 | 8.0\% | 3.00\% | 1420 | 1.00 | 1420 |
| 8.75-3.229 | 70 | 55 | Ramp 6- SB-EB 44 Loop Ramp Decel | 70 | 25 | D | P | 560.00 | 430.00 | 8.0\% | -1.00\% | 550 | 1.00 | 550 |
| 8.75-3.229 | 70 | 55 | Ramp 6- SB-EB 44 Loop Ramp Accel | 70 | 20 | A | P | 400.00 | 430.00 | 8.0\% | -0.70\% | 1520 | 1.00 | 1520 |
| 9-CD 120427 | 35 | 63 | Ramp 7- NB-EB 44 | 70 | 35 | A | P | 430.00 | 2850.00 | 3.4\% | 0.99\% | 1230 | 1.00 | 1230 |
| 8.5-3.203 | 35 | 63 | Ramp 8- EB-SB Route 65 | 70 | 50 | D | P | 430.00 | 955.00 | 8.0\% | -2.00\% | 340 | 1.00 | 340 |
| 9-CD 120427 | 35 | 63 | Ramp 9- EB-NB Route 65 Loop Ramp Decel | 70 | 20 | A | P | 400.00 | 400.00 | 7.9\% | -1.37\% | 1520 | 1.00 | 1520 |
| 12-CD 7155 | 4 | 9 | Ramp 1- County Road 199- WB 44 | 70 | 40 | A | P | 400.00 | 1538.64 | 5.0\% | 1.70\% | 1000 | 1.00 | 1000 |
| 12-CD 7155 | 4 | 9 | Ramp 2-EB 44-County Road 199 | 70 | 35 | D | P | 349.95 | 4583.66 | 2.0\% | 1.70\% | 490 | 1.00 | 490 |
| 12-CD 7155 | 5 | 10 | Ramp 3- WB 44- County Road 199 | 70 | 35 | D | P | 358.61 | 1272.95 | 5.0\% | 0.30\% | 490 | 1.00 | 490 |
| 12-CD 7155 | 5 | 10 | Ramp 4- County Road 199- EB 44 | 70 | 40 | A | P | 400.00 | 3104.23 | 3.0\% | 0.30\% | 1000 | 1.00 | 1000 |
| 11-3.337 | 4 | 13 | Ramp 1- Route 125- WB 44 | 70 | 35 | A | P | 400.00 | 1432.39 | 6.0\% | -1.50\% | 1230 | 1.00 | 1230 |
| 11-3.337 | 4 | 13 | Ramp 2- EB 44- Route 125 | 70 | 40 | D | P | 350.00 | 1432.39 | 6.0\% | -1.50\% | 440 | 1.00 | 440 |
| 11-3.337 | 4 | 13 | Ramp 3- WB 44- Route 125 | 70 | 40 | D | P | 1900.00 | 1145.16 | 7.0\% | -0.56\% | 440 | 1.00 | 440 |
| 11-3.337 | 4 | 13 | Ramp 4- Route 125- EB 44 | 70 | 40 | A | P | 400.00 | 1432.39 | 6.0\% | -0.56\% | 1000 | 1.00 | 1000 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Indicates posted advisory speed |  |  |  |  | Does not meet design criteria |  |  |  |  |  |  |  |
|  |  | Indicates design speed listed on plans |  |  |  |  | Current Ramp extension project |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Appendix E

## Bridge Analysis Tables

## US 360 Bridges



| Location | Bridge No. | Description | Structure Type | Structure Length ( ft ) | Bridge Width (ft) | Vert. Clr. <br> (ft) | Deck Rating | Super Rating | Sub Rating | Scope of Work | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A5905 | RP IS44W to MO360E over IS 44 | Steel Plate Girders | 296 | 30 | 17.33 | 7 | 7 | 8 | Epoxy polymer overlay or hydro \& latex | TBD |
|  | A5906 | MO 360 W over IS 44 | Steel Plate Girders | 296 | 30 | 18.33 | 7 | 7 | 8 | Epoxy polymer overlay or hydro \& latex | TBD |
| 2 | A5907 | RT MM S over MO 360 | Steel Plate Girders | 336 | 56 | 16.33 | 7 | 7 | 7 | Epoxy polymer overlay or hydro \& latex | TBD |
| 3 | A5842 | MO 360 E over CRD 156, BNSF RR | Steel Plate Girders | 368 | 40 | 20.33 | 7 | 9 | 8 | Epoxy polymer overlay or hydro \& latex | TBD |
|  | A5843 | MO 360 W over CRD 156, BNSF RR | Steel Plate Girders | 348 | 40 | 20.67 | 7 | 9 | 8 | Epoxy polymer overlay or hydro \& latex | TBD |



## US 60 Bridges (cont.)

From Route 13 to Glenstone Ave.
Date: 1/16/2018
Sheet: 2 of 3

| Location | Bridge No. | Description | Structure Type | Structure Length (ft) | Bridge Width (ft) | Vert. Clr. <br> (f) | Deck Rating | Super Rating | $\begin{aligned} & \text { Sub } \\ & \text { Rating } \end{aligned}$ | Scope of Work | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9 | A4184 | Republic Road E over US 60 | Steel Plate Girders | 409 | 83 | 16.00 | 6 | 6 | 6 | Overpass / remove asphalt overlay, replace w/ epoxy polymer or hydro \& latex / / | TBD |
| 10 | A4182 | US 60 WB over Campbell Ave, US 160 | P/S Concrete I-Girders | 225 | 41 | 16.75 | 7 | 6 | 7 | Seal or epoxy polymer or hydro \& latex / misc. subst. repairs | TBD |
| 10 | A4183 | US 60 EB over Campbell Ave, US 160 | P/S Concrete I-Girders | 238 | 41 | 17.00+ | 7 | 6 | 6 | Seal or epoxy polymer or hydro \& latex / misc. subst. repairs | TBD |
| 11 | A4181 | Republic Road W over US 60 | Steel Plate Girders | 489 | 72 | 16.00 | 7 | 8 | 6 | Overpass / seal or epoxy polymer or hydro \& latex / misc. subst. repairs / reset b | TBD |
| 12 | A4179 | US 60 EB over Ward Br. (Culvert Rating $=7$ ) | Culvert | 32 | 246 | N/A | N/A | N/A | N/A | Widen if needed | TBD |
| 13 | A4177 | National Ave S over US 60 | Steel Plate Girders | 274 | 99 | 16.92 | 7 | 8 | 6 | Overpass / misc. subst. repairs / sandblast \& paint at exp. jts. / coat abut. caps, | TBD |
| 14 | A4176 | Fremont Ave S over US 60 | P/S Concrete I-Girders | 259 | 52 | 17.00+ | 7 | 5 | 7 | Overpass / seal or epoxy polymer or hydro \& latex / misc. subst. repairs / sandbl | TBD |
| 15 | A4175 | BU 60 S over US 60 | Steel Plate Girders | 268 | 88 | 16.58 | 7 | 7 | 6 | Overpass / seal or epoxy polymer or hydro \& latex / misc. subst. repairs / sandbl | TBD |

## US 60 Bridges (cont.) <br> From Glenstone Ave. to Route 247

Date: 1/16/2018
Sheet: 3 of 3


| Location | $\begin{aligned} & \text { Bridge } \\ & \text { No. } \end{aligned}$ | Description |
| :---: | :---: | :---: |
| 16 | $\begin{aligned} & \text { A7537 } \\ & \text { A7538 } \\ & \text { A7539 } \\ & \text { A7540 } \end{aligned}$ | US 65 NB to US 60 WB Ramp over Galloway Creek, BNSF RR US 60 WB over Galloway Creek, BNSF RR US 60 EB over Galloway Creek, BNSF RR US 60 EB to US 65 NB Ramp over Galloway Creek, BNSF RR |
| 17 | $\begin{aligned} & \text { A2072 } \\ & \text { A7541 } \\ & \text { A7542 } \\ & \text { A7543 } \end{aligned}$ | US 65 SB over US 60 US 60 EB to US 65 NB Ramp over US 65 SB to US 60 EB US 65 NB to US 60 WB Ramp over US 65 NB to US 60 EB US 65 NB over US 60 |
| 18 | $\begin{aligned} & \text { A1218 } \\ & \text { A7550 } \end{aligned}$ | US 60 EB over James River US 60 WB over James River |
| 19 | A8303 | Rte J N over US 60 |
| 20 | A8343 | Rte 247 S over US 60 |


| Structure Type | Structure <br> Length (ft) | Bridge <br> Width (ft) | Vert. Clr. <br> (ft) | Deck <br> Rating | Super <br> Rating | Sub <br> Rating |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| P/S Concrete I-Girders | 361 | 29 | 23.00 | 8 | 9 | 9 |
| P/S Concrete I-Girders | 353 | 21 | 23.08 | 8 | 8 | 9 |
| P/S Concrete I-Girders | 353 | 41 | 23.50 | 7 | 9 | 9 |
| Steel Plate Girders \& P/S I-Gdr | 410 | 31 | 23.00 | 7 | 9 | 9 |
| Rolled Steel I-Beams | 184 | 44 | 16.50 | 7 | 9 | 6 |
| Steel Plate Girders \& P/S I-Gdr | 2018 | 32 | 16.75 | 7 | 9 | 9 |
| Steel Plate Girders | 1646 | 34 | 16.50 | 6 | 9 | 6 |
| P/S Concrete I-Girders | 223 | 60 | 17.17 | 7 | 9 | 9 |
| Steel Plate Girders | 395 | 32 | N/A | 7 | 7 | 6 |
| Steel Plate Girders | 416 | 51 | N/A | 6 | 8 | 8 |
| P/S Concrete I-Girders | 139 | 63 | 16.67 | 8 | 9 | 9 |
| P/S Concrete NU-Girders | 208 | 35 | 16.50 | 8 | 7 | 7 |


| No work needed (built in 2009) | TBD |
| :--- | :---: |
| No work needed (built in 2009) | TBD |
| No work needed (built in 2009) | TBD |
| No work needed (built in 2009) | TBD |
| Overpass / 2008 superstructure replacment fixed any issues | TBD |
| No work needed (built in 2009) | TBD |
| No work needed (built in 2009, epoxy polymer overlay applied in 2010) | TBD |
| Overpass / No work needed (built in 2009) | TBD |
| No work needed (2008 rehab was extensive) | TBD |
| No work needed (built in 2009) | TBD |
| Overpass / No work needed (built in 2015) | TBD |
| Oyerpass / Noworkneeded (built in 2015) | TBD |

## 1-44 Bridges <br> From Route 360 to Route 125

Date: 1/16/2018


| Location | $\begin{aligned} & \text { Bridge } \\ & \text { No. } \end{aligned}$ | Description | Structure Type | $\begin{aligned} & \text { Structure } \\ & \text { Length (ft) } \end{aligned}$ | Bridge Width ( ft ) | Vert. CIr. <br> (tt) | Deck Rating | $\begin{aligned} & \text { Super } \\ & \text { Rating } \end{aligned}$ | $\begin{gathered} \text { Sub } \\ \text { Rating } \end{gathered}$ | Scope of Work | Cost |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A0177 | IS $44 \mathrm{E} \mathrm{over} \mathrm{SAC} \mathrm{RVR} \mathrm{(Culvert} \mathrm{Rating}=7$ ) | Culvert | 31 | 193 | N/A | N/A | N/A | N/A | Extend existing culvert if neccesary | TBD |
| 2 | A8086 | RT B S over IS 44 | P/S Concrete NU Girders | 171 | 49 | 17.08 | 9 | 9 | 9 | New overpass-new interchange / no work needed | TBD |
| 3 | A0598 | MO 266 E ( W Chestnut Expy) over IS 44 | Rolled Steel I-Beam | 274 | 63 | 16.17 | 7 | 7 | 6 | Overpass / redecked in 2007 / no work needed | TBD |
| 4 | A0712E | IS 44 E over BNSF RR | Rolled Steel I-Beam | 158 | 34 | 23.25 | 7 | 7 | 7 | Remove existing overlay / hydro \& latex / if widened keep bridge and rehab | TBD |
|  | A0712W | IS 44 W over BNSF RR | Rolled Steel I-Beam | 158 | 34 | 23.25 | 7 | 7 | 7 | Remove existing overlay / hydro \& latex / if widened keep bridge and rehab | TBD |
| 5 | A0713 | RT EE E over IS 44 | Rolled Steel I-Beam | 280 | 32 | 16.00 | 5 | 7 | 6 | Overpass / hydro \& latex / replace expansion devices / other misc. repairs | TBD |
| 6 | A0714 | IS 44 W over MO 744, ABANDONED RR | Rolled Steel I-Beam | 407 | 35 | 24.92 | 7 | 7 | 7 | Rehab Programed 2018 = exp. jts. \& brngs; Needs hydro \& latex / sandblast \& paint / if widened keep bridge | TBD |
|  | A0715 | IS 44 E over MO 744, ABANDONED RR | Rolled Steel I-Beam | 443 | 35 | 24.33 | 7 | 6 | 7 | Rehab Programed 2018 = exp. jts. \& brngs; Needs hydro \& latex / sandblast \& paint/ if widened keep bridge | tBd |
| 7 | A7953 | US 160 E over IS 44 | Steel Plate Girder | 164 | 89 | 17.08 | 8 | 9 | 9 | New overpass-new interchange / no work needed | TBD |
| 8 | A0441 | 127 E (W Melville Rd) over IS 44 | Voided Slab | 234 | 31 | 16.00 | 5 | 5 | 7 | Remove exist. bridge | TBD |
| 9 | A0442 | IS 44 E over SPRING CR (Culvert Rating $=6$ ) | Culvert | 25 | 315 | N/A | N/A | N/A | N/A | Extend exist. culvert if neccesary | TBD |
| 10 | A0443 | MO 13 S over Is 44 | Voided Slab | 203 | 73 | 16.17 | 6 | 7 | 6 | Overpass / rehabilitated in 2008 / no work needed | TBD |
| 11 | A0444E | IS 44 E over CST BROADWAY AVE | Voided Slab | 134 | 44 | 15.50 | 7 | 7 | 7 | No work needed / replace if widened | TBD |
|  | A0444W | IS 44 W over CST BROADWAY AVE | Voided Slab | 134 | 44 | 15.50 | 7 | 7 | 7 | No work needed / replace if widened | TBD |
| 12 | A0445E | IS 44 E over CST GRANT AVE (N Farm Road 151) | Voided Slab | 139 | 44 | 15.08 | 7 | 7 | 7 | No work needed / replace if widened | TBD |
|  | A0445W | IS 44 W over CST GRANT AVE ( N Farm Road 151) | Voided Slab | 139 | 44 | 15.08 | 7 | 7 | 7 | No work needed / replace if widened | TBD |
| 13 | A0446 | IS 44 E over PEA RIDGE CR (Culvert Rating $=6$ ) | Culvert | 33 | 310 | N/A | N/A | N/A | N/A | No work needed / may need to replace if grade is raised due to extra load | TBD |
| 14 | A0447E | IS 44 E over CST National ave | Voided Slab | 134 | 44 | 15.08 | 7 | 7 | 7 | No work needed / replace if widened | TBD |
|  | A0447W | IS 44 W over CST National ave | Voided Slab | 134 | 44 | 15.08 | 7 | 7 | 7 | No work needed / replace if widened | TBD |
| 15 | A7501 | RTH S over IS 44 | P/S Concrete 1-Girders | 178 | 89 | 16.58 | 7 | 8 | 8 | Overpass / no work needed | TBD |
| 16 | A7024 | RP US65N to IS44W over RP IS44E to US65N, IS44 | Steel Plate Girder | 1383 | 41 | 16.42 | 6 | 9 | 7 | Overpass / no work needed | TBD |
|  | A2071 | US 65 S over IS 44 | Voided Slab | 216 | 44 | 15.42 | 5 | 5 | 7 | Overpass / if widened replace / if not widened hyrdo \& latex | TBD |
|  | A7300 | US 65 N over IS 44 | Rolled Steel I-Beam | 132 | 55 | 16.67 | 8 | 9 | 8 | New overpass-new interchange / no work needed | TBD |
| 17 | A4721 | MO 744 E ( N Farm Road 199) over IS 44 | Steel Plate Girder | 254 | 41 | 16.42 | 6 | 7 | , | Overpass / hydro \& latex / Replace exp. Jts. / overcoat paint / misc. subst. repairs | TBD |
| 18 | A5400 | MO 125 S over IS 44 | Voided Slab | 226 | 72 | 16.92 | 7 | 7 | 7 | Overpass / hydro \& latex by 2026 according to District Bridge Engineer | TBD |

## Appendix F

 Project Exhibits
# US 60 West Corridor Project Exhibits 












## US 60 East Corridor Project Exhibits





















## I-44 Corridor

## Project Exhibits












## Appendix G

## Detailed Cost Estimates

|  | FY 2018 |  | 60W-1 |  | 60W-2 |  | 60W-3* |  | 60W-4* |  | 60W-5 |  | 60W-6 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | J8P3032 <br> US 60/Glenstone Interchange |  | J8P3032 <br> US 60/MM Signals |  | J8P3032 <br> US 60/Sunshine DDI |  | J8P3032 <br> US 60/West Bypass DDI |  | $\begin{aligned} & \text { J8P3032 } \\ & \text { US 60/US } 65 \end{aligned}$ |  | J8P3032 <br> US 60/ National Ave |  |
| Item Description | Unit | Unit Cost | Qty | Total Cost | Qty | Total Cost | Qty | Total Cost | Qty | Total Cost | Qty | Total Cost | Qty | Total Cost |
| Interchange | LS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Fill | CY | \$8 | 30,963 | \$247,703 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Linear Grading | Mile | \$350,000 | 3.0 | \$1,057,027 | 0.2 | \$70,000 | 0.5 | \$175,000 | 0.7 | \$245,000 | 0.4 | \$147,159 | 0.3 | \$88,163 |
| Unclassified Excavation | CY | \$85 | 3,000 | \$255,000 |  | \$0 | 250 | \$21,250 | 500 | \$42,500 | 100 | \$8,500 | 100 | \$15,385 |
| Drainage Improvements | Mile | \$350,000 | 4.0 | \$1,397,614 | 0.2 | \$70,000 | 1.0 | \$350,000 | 1.4 | \$490,000 | 0.4 | \$140,000 | 0.3 | \$88,163 |
| GRADING/DRAINAGE SUBTOTAL |  |  |  | \$2,957,000 |  | \$140,000 |  | \$546,000 |  | \$778,000 |  | \$296,000 |  | \$192,000 |
| Interchange | LS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Mainline Pavement and Base | SY | \$75 | 64,113 | \$4,808,458 | 1,168 | \$87,617 | 6,730 | \$504,750 | 4,544 | \$340,813 | 1,494 | \$112,070 | 3,800 | \$285,000 |
| Outer Roads, Shoulders (Full Depth), and Base | SY | \$50 | 1,418 | \$70,922 | 600 | \$29,983 | 11,068 | \$553,384 | 12,740 | \$636,980 | 1,055 | \$52,767 | 1,489 | \$74,433 |
| Low Type Surface and Base | SY | \$35 | 3,359 | \$117,553 |  | \$0 | 4,797 | \$167,893 | 3,779 | \$132,278 |  | \$0 |  | \$0 |
| Pavement Overlay | SY | \$15 | 533 | \$8,000 |  | \$0 | 13,242 | \$198,624 | 7,189 | \$107,834 | 3,575 | \$53,625 |  | \$0 |
| Pavement Removal | SY | \$10 | 39,578 | \$395,776 | 535 | \$5,351 | 2,000 | \$20,000 | 4,000 | \$40,000 | 1,495 | \$14,950 | 2,687 | \$26,872 |
| PAVEMENT BASE/SURFACE SUBTOTAL |  |  |  | \$5,401,000 |  | \$123,000 |  | \$1,445,000 |  | \$1,258,000 |  | \$233,000 |  | \$386,000 |
| Interchange | LS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Bridge (Includes Costs of MSE Walls for Bridges) | LS |  |  | \$1,428,000 |  | \$0 |  | \$650,000 |  | \$525,000 |  | \$0 |  | \$0 |
| Retaining Walls | SF | \$80 | 1,850 | \$148,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 | 780 | \$62,400 |
| Noise Walls | SF | \$40 | 0 | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 | 0 | 0 |
| BRIDGE ITEMS SUBTOTAL |  |  |  | \$1,576,000 |  | \$0 |  | \$650,000 |  | \$525,000 |  | \$0 |  | \$62,000 |
| Concrete Safety Barrier | LF | \$50 | 15,738 | \$786,900 |  | \$0 | 850 | \$42,500 | 326 | \$16,275 |  | \$0 |  | \$0 |
| Guardrail | LF | \$30 | 470 | \$14,100 | 350 | \$10,500 | 1,400 | \$42,000 | 1,400 | \$42,000 |  | \$0 | 1,125 | \$33,750 |
| Guardrail End Terminal | EA | \$3,000 | 5 | \$15,000 | 2 | \$6,000 | 8 | \$24,000 | 8 | \$24,000 |  | \$0 | 2 | \$6,000 |
| Curb/Gutter | LF | \$35 | 4,927 | \$172,445 |  | \$0 |  | \$0 |  | \$0 |  | \$0 | 260 | \$9,100 |
| Traffic Signals | LS |  |  | \$525,000 |  | \$350,000 |  | \$450,000 |  | \$450,000 |  | \$35,000 |  | \$25,000 |
| Lighting | LS |  |  | \$202,000 |  | \$0 |  | \$67,500 |  | \$67,500 |  | \$0 |  | \$5,000 |
| Sign Structures (Overhead) | EA | \$100,000 | 7 | \$700,000 |  | \$0 | 2 | \$200,000 | 2 | \$200,000 |  | \$0 | 1 | \$100,000 |
| Sign Structures (Cantilever) | EA | \$50,000 | 1 | \$50,000 |  | \$0 | 2 | \$100,000 | 2 | \$100,000 |  | \$0 |  | \$0 |
| Sign Structures (Mast Arm) | EA | \$25,000 | 3 | \$75,000 |  | \$0 | 2 | \$50,000 | 2 | \$50,000 |  | \$0 | 2 | \$50,000 |
| Signing and Pavement Marking ( $2 \%$ Grading \& Pvmt) | 2\% |  |  | \$167,000 |  | \$5,000 |  | \$40,000 |  | \$41,000 |  | \$11,000 |  | \$12,000 |
| Erosion Control (1\% Grading \& Pvmt) | 1.0\% |  |  | \$84,000 |  | \$3,000 |  | \$20,000 |  | \$20,000 |  | \$5,000 |  | \$6,000 |
| Traffic Control | 4\% |  |  | \$509,000 | LS | \$100,000 |  | \$147,000 |  | \$143,000 | LS | \$100,000 | LS | \$100,000 |
| Mobilization (5\% Total Const Cost) | 5\% |  |  | \$662,000 |  | \$37,000 |  | \$191,000 |  | \$186,000 |  | \$34,000 |  | \$49,000 |
| MISCELLANEOUS ITEMS SUBTOTAL |  |  |  | \$3,962,000 |  | \$512,000 |  | \$1,374,000 |  | \$1,340,000 |  | \$185,000 |  | \$396,000 |
| Subtotal Construction Cost Estimate |  |  |  | \$13,896,000 |  | \$775,000 |  | \$4,015,000 |  | \$3,901,000 |  | \$714,000 |  | \$1,036,000 |
| Contingency | 5\% |  |  | \$695,000 |  | \$39,000 |  | \$201,000 |  | \$195,000 |  | \$36,000 |  | \$52,000 |
| Total Construction Cost Estimate |  |  |  | \$14,591,000 |  | \$814,000 |  | \$4,216,000 |  | \$4,096,000 |  | \$750,000 |  | \$1,088,000 |
| Design \& Survey | 10\% |  |  | \$1,460,000 |  | \$80,000 |  | \$420,000 |  | \$410,000 |  | \$80,000 |  | \$110,000 |
| Construction Engineering | 5\% |  |  | \$730,000 |  | \$40,000 |  | \$210,000 |  | \$200,000 |  | \$40,000 |  | \$50,000 |
| Utility Relocation (5\% Grading and Pavement) | 5\% |  | LS | \$0 | LS | \$0 | LS | \$0 |  | \$100,000 | LS | \$0 | LS | \$0 |
| Right of Way (rural) | Acre | \$30,000 |  | \$0 |  | \$0 |  | \$0 | 2.6 | \$80,000 |  | \$0 |  | \$0 |
| Right of Way (urban) | Acre | \$100,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Right of Way Incidentals | Each | \$15,000 |  | \$0 |  | \$0 |  | \$0 | 3 | \$50,000 |  | \$0 |  | \$0 |
|  |  |  |  | \$16,781,000 |  | \$934,000 |  | \$4,846,000 |  | \$4,936,000 |  | \$870,000 |  | \$1,248,000 |

* Projects 60W-3 and 60W-4 were not carried forward after refined operational analysis did not indicate a need.
hdrinc.com

|  | FY 2018 |  | 60E-1 |  | 60E-2 |  | 60E-3 |  | 60E-4 |  | 60E-5 |  | 60E-6 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | J8P0683G |  |  |  | J8P0683G |  | J8P0683G |  | J8P0683E |  | J8P0683E |  |
|  |  |  | J8P0683E <br> US 60/125 Interchange |  | US 60 Fwy-Highland Springs to NN/J |  | US 60/FR 189 Intchg + Frontage Rds |  | US 60 Freeway-NN/J to elo FR213 |  | US 60 Freeway-e/o FR 213 to Rte 125 |  | US 60 Freeway Rte 125 to FR 247 |  |
| Item Description | Unit | Unit Cost | Qty | Total Cost | Qty | Total Cost | Qty | Total Cost | Qty | Total Cost | Qty | Total Cost | Qty | Total Cost |
| Interchange | LS |  |  |  |  |  |  | \$2,250,000 |  |  |  |  |  |  |
| Fill | CY | \$8 | 146,658 | \$1,173,261 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Linear Grading | Mile | \$350,000 | 2.57 | \$898,658 | 3.6 | \$1,263,500 | 3.6 | \$1,263,500 | 4.8 | \$1,682,850 | 3.6 | \$1,266,297 | 3.9 | \$1,380,246 |
| Unclassified Excavation | CY | \$85 | 1,666 | \$141,610 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Drainage Improvements | Mile | \$350,000 | 1.50 | \$525,000 | 3.6 | \$1,263,500 | 3.6 | \$1,263,500 | 4.8 | \$1,682,850 | 3.6 | \$1,266,297 | 3.9 | \$1,380,246 |
| GRADING/DRAINAGE SUBTOTAL |  |  |  | \$2,739,000 |  | \$2,527,000 |  | \$4,777,000 |  | \$3,366,000 |  | \$2,533,000 |  | \$2,760,000 |
| Interchange | LS |  |  |  |  |  |  | \$4,402,000 |  |  |  |  |  |  |
| Mainline Pavement and Base | SY | \$75 | 41,453 | \$3,108,983 | 31,596 | \$2,369,675 | 31,596 | \$2,369,675 | 50,355 | \$3,776,650 | 37,401 | \$2,805,067 | 21,293 | \$1,596,983 |
| Outer Roads, Shoulders (Full Depth), and Base | SY | \$50 | 19,220 | \$960,989 | 62,310 | \$3,115,481 | 62,310 | \$3,115,481 | 56,266 | \$2,813,308 | 48,665 | \$2,433,233 | 64,534 | \$3,226,689 |
| Low Type Surface and Base | SY | \$35 | 11,276 | \$394,664 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Pavement Overlay | SY | \$15 | 0 | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Pavement Removal | SY | \$10 | 46,908 | \$469,084 | 17,428 | \$174,282 |  | \$0 |  | \$0 | 5,273 | \$52,732 | 875 | \$8,748 |
| PAVEMENT BASE/SURFACE SUBTOTAL |  |  |  | \$4,934,000 |  | \$5,659,000 |  | \$9,887,000 |  | \$6,590,000 |  | \$5,291,000 |  | \$4,832,000 |
| Interchange | LS |  |  |  |  |  |  | \$2,050,000 |  |  |  |  |  |  |
| Bridge (Includes Costs of MSE Walls for Bridges) | LS |  |  | \$2,080,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Retaining Walls | SF | \$80 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Noise Walls | SF | \$40 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| BRIDGE ITEMS SUBTOTAL |  |  |  | \$2,080,000 |  | \$0 |  | \$2,050,000 |  | \$0 |  | \$0 |  | \$0 |
| Concrete Safety Barrier | LF | \$50 | 1,331 | \$66,550 | 11,225 | \$561,250 | 11,225 | \$561,250 | 15,946 | \$797,300 | 16,665 | \$833,250 | 4,744 | \$237,200 |
| Guardrail | LF | \$30 | 3,104 | \$93,120 | 300 | \$9,000 | 300 | \$9,000 | 500 | \$15,000 |  | \$0 |  | \$0 |
| Guardrail End Terminal | EA | \$3,000 | 2.0 | \$6,000 | 2 | \$6,000 | 2 | \$6,000 | 2 | \$6,000 |  | \$0 |  | \$0 |
| Curb/Gutter | LF | \$35 | 2,761 | \$96,646 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Traffic Signals | LS |  |  | \$0 |  | \$200,000 |  | \$200,000 |  | \$0 |  | \$0 |  | \$0 |
| Lighting | LS |  |  | \$117,500 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Sign Structures (Overhead) | EA | \$100,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Sign Structures (Cantilever) | EA | \$50,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Sign Structures (Mast Arm) | EA | \$25,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Signing and Pavement Marking ( $2 \%$ Grading \& Pvmt) | 2\% |  |  | \$153,000 |  | \$164,000 |  | \$293,000 |  | \$199,000 |  | \$156,000 |  | \$152,000 |
| Erosion Control (1\% Grading \& Pvmt) | 1.0\% |  |  | \$77,000 |  | \$82,000 |  | \$147,000 |  | \$100,000 |  | \$78,000 |  | \$76,000 |
| Traffic Control | 4\% |  |  | \$415,000 |  | \$368,000 |  | \$717,000 |  | \$443,000 |  | \$356,000 |  | \$322,000 |
| Mobilization (5\% Total Const Cost) | 5\% |  |  | \$539,000 |  | \$479,000 |  | \$932,000 |  | \$576,000 |  | \$462,000 |  | \$419,000 |
| MISCELLANEOUS ITEMS SUBTOTAL |  |  |  | \$1,564,000 |  | \$1,869,000 |  | \$2,865,000 |  | \$2,136,000 |  | \$1,885,000 |  | \$1,206,000 |
| Subtotal Construction Cost Estimate |  |  |  | \$11,317,000 |  | \$10,055,000 |  | \$19,579,000 |  | \$12,092,000 |  | \$9,709,000 |  | \$8,798,000 |
| Contingency | 5\% |  |  | \$566,000 |  | \$503,000 |  | \$979,000 |  | \$605,000 |  | \$485,000 |  | \$440,000 |
| Total Construction Cost Estimate |  |  |  | \$11,883,000 |  | \$10,558,000 |  | \$20,558,000 |  | \$12,697,000 |  | \$10,194,000 |  | \$9,238,000 |
| Design \& Survey | 10\% |  |  | \$1,190,000 |  | \$1,060,000 |  | \$2,060,000 |  | \$1,270,000 |  | \$1,020,000 |  | \$920,000 |
| Construction Engineering | 5\% |  |  | \$590,000 |  | \$530,000 |  | \$1,030,000 |  | \$630,000 |  | \$510,000 |  | \$460,000 |
| Utility Relocation (5\% Grading and Pavement) | 5\% |  |  | \$380,000 |  | \$410,000 | LS | \$610,000 |  | \$500,000 |  | \$390,000 |  | \$380,000 |
| Right of Way (rural) | Acre | \$30,000 | 3.6 | \$110,000 | 3.78 | \$110,000 | 6.78 | \$200,000 | 4.4 | \$130,000 | 4.81 | \$140,000 | 10.88 | \$330,000 |
| Right of Way (urban) | Acre | \$100,000 |  | \$0 |  | \$0 | 3 | \$300,000 |  | \$0 |  | \$0 |  | \$0 |
| Right of Way Incidentals | Each | \$15,000 | 7 | \$110,000 | 4 | \$60,000 | 10 | \$150,000 | 3 | \$50,000 | 4 | \$60,000 | 12 | \$180,000 |
|  |  |  |  | \$14,263,000 |  | \$12,728,000 |  | \$24,908,000 |  | \$15,277,000 |  | \$12,314,000 |  | \$11,508,000 |

I-44 Corridor Detailed Cost Estimate

|  | FY 2018 |  | 44-1 |  | 44-2 |  | 44-3 |  | 44-4 |  | 44-5 |  | 44-6 |  | 44-7 |  | 44-8 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | J813044 |  | J813044 |  | J813044 |  | J813044 |  | J813044 |  | J813044 |  | J813044 |  | J813044 |  |
|  |  |  | 1-44 Aux Lanes |  | 1-44/MM RAB |  | 1-44/Chestnut |  |  |  | 1-44/West Bypass |  | 1-44/US 65 SB-EB |  | 1-44/FR199 RAB |  | 1-44/125 |  |
|  |  |  | Rte 13 to US 65 |  | Accel/Decel |  | Loop |  | 1-44/744 Accel Lane |  | Accel/Decel |  | Flyover |  | Accel/Decel |  | Accel/Decel |  |
| Item Description | Unit | Unit | Qty | Total Cost | Qty | Total Cost | Qty | Total | Qty | Total Cost | Qty | Total Cost | Qty | Total Cost | Qty | Total Cost | Qty | Total Cost |
| Interchange | LS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Fill | CY | \$8 | 40,300 | \$322,400 |  | \$0 |  | \$0 |  | \$0 | 12,452 | \$99,616 |  | \$0 | 13,202 | \$105,616 |  | \$0 |
| Linear Grading | Mile | \$350,000 | 5.0 | \$1,760,500 | 1.39 | \$487,216 | 0.15 | \$53,030 | 0.35 | \$122,500 |  | \$0 | 0.7 | \$255,208 | 1.4 | \$497,027 | 0.4 | \$145,436 |
| Unclassified Excavation | CY | \$85 | 8,980 | \$763,300 | 250 | \$21,250 |  | \$0 | 100 | \$8,500 | 250 | \$21,250 | 250 | \$21,250 | 250 | \$21,250 | 250 | \$21,250 |
| Drainage Improvements | Mile | \$350,000 | 5.0 | \$1,760,500 | 1.39 | \$487,216 | 0.15 | \$53,030 | 0.35 | \$122,500 | 0.15 | \$52,500 | 0.7 | \$255,208 | 1.4 | \$490,000 | 0.4 | \$140,000 |
| GRADING/DRAINAGE SUBTOTAL |  |  |  | \$4,607,000 |  | \$996,000 |  | \$106,000 |  | \$254,000 |  | \$173,000 |  | \$532,000 |  | \$1,114,000 |  | \$307,000 |
| Interchange | LS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Mainline Pavement and Base | SY | \$75 | 93,848 | \$7,038,600 | 17,724 | \$1,329,325 | 1,050 | \$78,750 | 3,616 | \$271,200 | 1,667 | \$125,002 | 6,543 | \$490,750 | 11,734 | \$880,064 | 2,295 | \$172,129 |
| Outer Roads, Shoulders (Full Depth), and Base | SY | \$50 | 36,667 | \$1,833,350 | 6,550 | \$327,478 | 543 | \$27,133 | 1,764 | \$88,200 | 947 | \$47,367 | 3,266 | \$163,322 | 5,029 | \$251,474 | 1,429 | \$71,433 |
| Low Type Surface and Base | SY | \$35 | 845 | \$29,575 | 2,179 | \$76,273 |  | \$0 |  | \$0 |  | \$0 |  | \$0 | 233 | \$8,160 |  | \$0 |
| Pavement Overlay | SY | \$15 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Pavement Removal | SY | \$10 | 59,200 | \$592,000 | 22,240 | \$222,397 | 532 | \$5,320 | 3,904 | \$39,044 | 751 | \$7,508 | 3,213 | \$32,127 | 2,139 | \$21,390 | 9,408 | \$94,081 |
| PAVEMENT BASE/SURFACE SUBTOTAL |  |  |  | \$9,494,000 |  | \$1,955,000 |  | \$111,000 |  | \$398,000 |  | \$180,000 |  | \$686,000 |  | \$1,161,000 |  | \$338,000 |
| Interchange | LS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Bridge (Includes Costs of MSE Walls for Bridges) | LS |  |  | \$6,600,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$10,000,000 |  | \$0 |  | \$0 |
| Retaining Walls | SF | \$80 | 2,600 | \$208,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Noise Walls | SF | \$40 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| BRIDGE ITEMS SUBTOTAL |  |  |  | \$6,808,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$10,000,000 |  | \$0 |  | \$0 |
| Concrete Safety Barrier | LF | \$50 | 2,550 | \$127,500 |  | \$0 |  | \$0 | 433 | \$21,650 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Guardrail | LF | \$30 | 11,935 | \$358,050 | 575 | \$17,250 |  | \$0 | 125 | \$3,750 | 800 | \$24,000 | 50 | \$1,500 | 750 | \$22,500 |  | \$0 |
| Guardrail End Terminal | EA | \$3,000 | 17 | \$51,000 | 2.0 | \$6,000 |  | \$0 | 1.0 | \$3,000 | 1 | \$3,000 | 1 | \$3,000 | 2 | \$6,000 |  | \$0 |
| Curb/Gutter | LF | \$35 | 2,000 | \$70,000 | 1,350 | \$47,250 |  | \$0 |  | \$0 |  | \$0 |  | \$0 | 1,705 | \$59,675 |  | \$0 |
| Traffic Signals | LS |  |  | \$25,000 |  | \$0 |  | \$0 |  | \$0 |  | \$30,000 |  | \$0 |  | \$0 |  | \$175,000 |
| Lighting | LS |  |  | \$50,000 |  | \$113,000 |  | \$0 |  | \$32,500 |  | \$12,000 |  | \$18,000 |  | \$93,500 |  | \$12,000 |
| Sign Structures (Overhead) | EA | \$100,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 | 1 | \$100,000 |  | \$0 |  | \$0 |
| Sign Structures (Cantilever) | EA | \$50,000 | 8 | \$400,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 | 1 | \$50,000 |  | \$0 |  | \$0 |
| Sign Structures (Mast Arm) | EA | \$25,000 | 2 | \$50,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Signing and Pavement Marking (2\% Grade \& Pvmt) | 2\% |  |  | \$282,000 |  | \$59,000 |  | \$4,000 |  | \$13,000 |  | \$7,000 |  | \$24,000 |  | \$46,000 |  | \$13,000 |
| Erosion Control ( $1 \%$ Grading \& Pvmt) | 1.0\% |  |  | \$141,000 |  | \$30,000 |  | \$2,000 |  | \$7,000 |  | \$4,000 |  | \$12,000 |  | \$23,000 |  | \$6,000 |
| Traffic Control | 4\% |  |  | \$899,000 |  | \$129,000 | LS | \$100,000 | LS | \$100,000 | LS | \$100,000 |  | \$457,000 | LS | \$100,000 | LS | \$100,000 |
| Mobilization (5\% Total Const Cost) | 5\% |  |  | \$1,168,000 |  | \$168,000 |  | \$16,000 |  | \$42,000 |  | \$27,000 |  | \$594,000 |  | \$131,000 |  | \$48,000 |
| MISCELLANEOUS ITEMS SUBTOTAL |  |  |  | \$3,622,000 |  | \$570,000 |  | \$122,000 |  | \$223,000 |  | \$207,000 |  | \$1,260,000 |  | \$482,000 |  | \$354,000 |
| Subtotal Construction Cost Estimate |  |  |  | \$24,531,00 |  | \$3,521,000 |  | \$339,000 |  | \$875,000 |  | \$560,000 |  | \$12,478,000 |  | \$2,757,000 |  | \$999,000 |
| Contingency | 5\% |  |  | \$1,227,000 |  | \$176,000 |  | \$17,000 |  | \$44,000 |  | \$28,000 |  | \$624,000 |  | \$138,000 |  | \$50,000 |
| Total Construction Cost Estimate |  |  |  | \$25,758,00 |  | \$3,697,000 |  | \$356,000 |  | \$919,000 |  | \$588,000 |  | \$13,102,000 |  | \$2,895,000 |  | \$1,049,000 |
| Design \& Survey | 10\% |  |  | \$2,580,000 |  | \$370,000 |  | \$40,000 |  | \$90,000 |  | \$60,000 |  | \$1,310,000 |  | \$290,000 |  | \$100,000 |
| Construction Engineering | 5\% |  |  | \$1,290,000 |  | \$180,000 |  | \$20,000 |  | \$50,000 |  | \$30,000 |  | \$660,000 |  | \$140,000 |  | \$50,000 |
| Utility Relocation (5\% Grading and Pavement) | 5\% |  | LS | \$0 |  | \$150,000 | LS | \$0 |  | \$30,000 | LS | \$0 | LS | \$0 |  | \$110,000 | LS | \$0 |
| Right of Way (rural) | Acre | \$30,000 |  | \$0 | 1.3 | \$40,000 |  | \$0 | 0.3 | \$10,000 |  | \$0 |  | \$0 | 0.41 | \$10,000 |  | \$0 |
| Right of Way (urban) | Acre | \$100,000 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Right of Way Incidentals | Each | \$15,000 |  | \$0 | 3 | \$50,000 |  | \$0 | 1 | \$20,000 |  | \$0 |  | \$0 | 1 | \$20,000 |  | \$0 |
|  |  |  |  | \$29,628,00 |  | \$4,487,000 |  | \$416,000 |  | \$1,119,000 |  | \$678,000 |  | \$15,072,000 |  | \$3,465,000 |  | \$1,199,000 |

Appendix H Crash Modification Factors

## Crash Modification Factors

| Type | Description | Value | Applicable Projects | Quality | Crash Type | Crash Severity | Assumptions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mainline Lanes | Add continuous auxiliary lane for weaving between entrance ramp and exit ramp | 0.79 | 44-1 | *** | All | All |  |
|  | (Estimated) Add braided ramp roadway | 0.5 | 60W-1 | na | na | na | No similar CMF available. The project will eliminate weaving collisions that currently exist east of Glenstone. The braided ramp roadway may introduce typical sideswipes, but at a lower rate. This is the basis for the estimation. |
| Interchange Type | Convert at-grade intersection into gradeseparated interchange | 0.43 | 60E-1, 60E-2, 60E-3, 60E-4, 60E-5, 60E-6 | ***** | All | A,B,C | This CMF was applied to all crash severities. The CMF for all severities is slightly higher at 0.58 . Due to the fact that in many locations the at-grade is removed without being replaced by an interchange, the lower CMF was assumed due to the lower number of conflicts. |
|  | Convert diamond interchange to DDI | 0.67 | 60W-1, 60W-3, 60W-4 | **** | All | All |  |
|  | Provide straight ramp instead of cloverleaf | 0.55 | 44-6 | *** | All | All |  |
| Ramp Design | Convert a Type I exit ramp to a Type III exit ramp | 0.79 | 44-1 | *** | Truck related | All | This CMF was applied to truck and non-truck related crashes. Truck data was unavailable, and this CMF was closest in applicability. |
|  | Extend acceleration lane by approx. 98 ft | 0.89 | $\begin{gathered} 44-2,44-3,44-4,44-5, \\ 44-7,44-8,60 W-5 \\ \hline \end{gathered}$ | ***** | All | All | Acceleration length extensions varied on each project and were generally longer than 98 ft ., but this CMF has the closest applicability. |
|  | Change length of deceleration lane from 101 200 ft to 601 - 700 ft . | 0.064 | 44-2 | *** | All | All | Deceleration length changes in actual projects may not match exactly as stated in the CMF, but the CMF with the closest total increase was chosen. |
|  | Change length of deceleration lane from 401 500 ft to $601-700 \mathrm{ft}$. | 0.59 | 44-5, 60W-5 | ** | All | All | Deceleration length changes in actual projects may not match exactly as stated in the CMF, but the CMF with the closest total increase was chosen. |
|  | Extend deceleration lane by approx. 100ft | 0.93 | 44-7, 44-8 | *** | All | All |  |
|  | Change number of lanes on freeway exit ramp from $X$ to $Y$ | 0.31 | 60W-6 | *** | All | All |  |
|  | (Estimated) Provide positive separation for acceleration lane | 0.9 | 44-3, 44-4 | na | na | na | No exact CMF available. Estimate based on various CMFs applicable to delineators, wide pavement markings, and channelization. |
|  | (Estimated) Remove ramp access to/from truck parking | 0.58 | 44-8 | na | na | na | No exact CMF available. Estimate based on a combination of factors, but ultimately using the value for converting an at-grade intersection to a gradeseparated interchange. |
| Intersection Design | Convert intersection with minor-road stop control to modern roundabout | 0.56 | 44-2, 44-7 | ***** | All | All |  |
|  | Increase the number of left-turn lanes on major road | 0.75 | 60W-1, 44-1, 44-5 | *** | Sideswipe | All | CMF was applied to all crash types. The CMF for installing a left-turn lane had a similar CMF value ( 0.748 ) and was stated to be applicable to all crash types. In the case of project 44-1, the CMF is applied due to addition of a right turn lane. |
|  | Install a traffic signal and left turn lanes | 0.54 | 60W-2 | **** | All | All |  |
|  | Install a traffic signal | 0.56 | 44-8 | ***** | All | All |  |

Notes: Projects where dual left-turn lanes were converted to triple left-turn lanes were given a CMF of 1.0 (no crash reduction). A Texas study found that triple lefts did not raise any major safety issues. For projects 60E-2 and 60E-3, the CMF for installing a traffic signal, as shown in the table above, was not used. Adequate crash data did not exist at this location because the signal was installed during the last month of the crash data time period. A CMF of 1.0 was used in this case.
Source: Crash Modification Factors Clearinghouse, http://www.cmfclearinghouse.org/index.cfm

## Appendix I

Mid-Project Preliminary Prioritization Results

The following page was transmitted to MoDOT on February 28, 2018 for assistance in formulating STIP inputs, with the understanding that the data was preliminary and based on the best information at that time. Between that time and the completion of this report, several refinements have been made that have resulted in adjustments to the prioritization tables. Key among these refinements were the following:

- The construction cost estimates were thoroughly reviewed, and adjustments were made to several unit costs. These changes caused variations in all the estimates, with some increasing and some decreasing.
- The traffic operational analysis was refined, adjusting signal timing, segmentation of the US60 East corridor, ramp merge / diverge calculations, and driver behavior at the two-stage unsignalized intersections along US-60 East.
- The safety analysis was refined, including further adjustments of Crash Modification Factors (CMFs) and improvement influence areas.

Although these changes caused projects to move to various places on the prioritization list, the general order of the large ( $>\$ 9 \mathrm{~m}$ ) projects was preserved, as was the general order of the small projects.


| Ranking | Study Project \# | Location | Project Description | Construction Costs | Total Costs | Rounded Costs | High Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 60E-1 | US-60, at Route 125 | Convert at-grade signaized intersection to a grade separated interchange with double "peanut" roundabouts | \$11,888,000 | \$14,238,000 | \$14,240,000 | \$16,380,000 |
| 2 | 60E-2 | US-60, Highland Spring to J/ $/ \mathrm{NN}$ | Close at-grade intersections and construct new outer roads and new freeway roadways, and signaize the WB offramp at $\mathrm{J} / \mathrm{NN}$ | \$10,043,000 | \$12,173,000 | \$12,170,000 | \$14,000,000 |
| 3 | 60E-4 | US-60, J/NN to East of fr 213 | Close at-grade intersections and construct new outer roads and new freeway roadways | \$11,720,000 | \$14,120,000 | \$14,120,000 | \$16,240,000 |
| 4 | 60E-3 | US-60, at FR 189 | Convert to a grade separated interchange, close at-grade intersections, and construct new outer roads and new freeway roadways, and signalize the WB offramp at J/ NN | \$20,04, 000 | \$24,35,000 | \$24,350,000 | \$28,000,000 |
| 5 | 44.8 | 1-44, at Route 125 | Signalize the WB offrramp terminal, extend the EB acceldecel and WB accel ramps, and close old weigh staion | \$744,000 | \$877,000 | \$870,000 | \$1,000,000 |
| 6 | 60W-6 | US.60, at National | Add a 3rd left-turn lane at the EB offr-ramp taffic signal and add a third dight-turn lane at the WB offramp | \$1,020,000 | \$1,190,000 | \$1,190,000 | \$1,370,000 |
| 7 | 44-2 | 1.44, at MM/B | Construct roundabouts at both ramp terminals (tei-i. frontage road on notth-side) and extend all accelldeceel ramps | \$3,36,000 | \$3,986,000 | \$3,90,000 | \$4,590,000 |
| 8 | 44.5 | 1-44, at lighway 160 (West Bypass) | Add a 2nd left-um lane at the WB offr-ramp trafic signal and extend the EB decel and WB accel ramps | \$452,000 | \$532,000 | \$530,000 | \$610,000 |
| 9 | 60W-5 | Us-60, at US-65 | Extend the WB to SB deeel ramp and the SB to EB accel ramp | \$398,00 | \$468,000 | \$470,000 | \$540,000 |
| 10 | 44.3 | 1-44, a Chestrut Expwy | Exend and provide positive separation for WB accel lane | \$242,000 | \$282,000 | \$280,000 | \$320,000 |
| 11 | 44.7 | 1.44, at Muroy | Construct roundabouts at both ramp terminals (tie-in frontage road on south-side) and extend all accel/decel ramps | \$2,38,000 | \$2,848,000 | \$2,85,000 | \$3,28,000 |
| 12 | 60W-2 | Us-601360, at MM | Signalize both ramp terminals and include left-um lanes at both ramps | \$590,000 | \$690,000 | \$690,000 | \$790,000 |
| 13 | 44.4 | 1-4, West of Route 744 (Kearney) | Extend and provide positive separation for WB accel lane | \$747,00 | \$887,000 | \$890,000 | \$1,20,000 |
| 14 | 60-5 5 | US-60, East of FR 213 to Rte. 125 | Close at-grade intersections and construct new outer roads and nee freeway roadways | \$9,551,000 | \$11,481,000 | \$11,480,000 | \$13,200,000 |
| 15 | 60W-4 | Us-60, at Route FF / US 160 (West Bypass) | Convert to interchange to a DD and relocate nearby divive access | \$3,69,000 | \$4,229,000 | \$4,230,00 | \$4,80,000 |
| 16 | 60W-3 | Us-60/360, at Route 413 (Sunssine) | Convert to interchange to a DOl and relocate nearby dive access | \$4,351,000 | \$5,101,000 | \$5,10,000 | 55,870,000 |
| 17 | 60W-1 | US.60, National to US.65 | Provide an EB braided ramp roadway and provide a DD a Glenstone to reconfigure access to US 60 | \$14,415,00 | \$16,925,000 | \$16,930,000 | \$19,470,000 |
| 18 | 60-6 | US-60, Route 125 to FR 247 | Close at-grade intersections and construct new outer roads and new freeway roadways | 98,467,000 | \$10,707,000 | \$10,710,000 | \$12,320,000 |
| 19 | 44.6 | 1-44, at US-65 | Construct a SB-to-EB flyover ramp and eiminiate the exising cloverleaf | \$13,006,000 | \$15,690,000 | \$15,700,000 | \$18,000,000 |
| 20 | 44.1 | 1-44, Route 13 (KS Expwy to US-65 | Provide axxiliary lanes bewwen interchanges and provide an added 2nd right-um lane for the WB offramp at Route 13 , including minor shoulder improvements at the Glenstone interchange | \$25,396,000 | \$29,816,000 | \$29,820,000 | \$34,290,000 |

- Existing MODOT project is addressing some of the issues addressed by this project


[^0]:    1
    https://www.transportation.gov/sites/dot.gov/files/docs/2016\%20Revised\%20Value\%20of\%20Travel\%20Time\%20Gui dance.pdf

[^1]:    Red text indicates projects with a construction cost of greater than \$9M.

[^2]:    Red text indicates projects with a construction cost of greater than \$9M.

